



**TOWN OF DIGHTON**  
**PLANNING BOARD**  
**979 SOMERSET AVENUE**  
**DIGHTON, MA 02715**  
**Tel: (508) 669-6431, Ext. 114**  
**Fax: (508) 669-4509**

Jeff Carvalho, Chairman  
Daniel Higgins, Vice Chairman  
Christopher Cunha, Clerk  
Joseph Figueiredo, Member  
Robert J. Woods, Member

LEGAL NOTICE  
DIGHTON PLANNING BOARD  
June 5, 2024 at 7:00 PM  
Old Town Hall  
1111 Somerset Avenue  
Dighton, MA 02715

Notice is hereby given the Dighton Planning Board will conduct a Public Hearing on the Modification of a Special Permit and Site Plan Review by GHTJA03, LLC (Grasshopper Energy) for a redesign of stormwater Basin 1 and submit maintenance items for stormwater Basin 3, for property located at 893 Brook Street being shown as Assessors Map 16, Lot 28, pursuant to Sections 4600, 5300 and 5400 of the Town of Dighton Zoning Bylaws.

Copies of the application and plan may be viewed in the Planning Board office during normal business hours or requested by email at [keasterday@dighton-ma.gov](mailto:keasterday@dighton-ma.gov). Any person wishing to be heard on the above application should appear at the time and place designated for the public hearing.

DIGHTON PLANNING BOARD  
Jeff Carvalho, Chairman

**RECEIVED**

Town Clerk-Dighton, MA

MAY 07 2024

Time: 9:29 AM

By: SC

05-24



PETITIONER  
NAME &  
ADDRESS

GHTJAO3

**TOWN OF DIGHTON**  
**PLANNING BOARD**

LOCATION (from Assessors' Office)  
PLAT AND  
LOT NOS.

MAP 16 Parcel 28

PRESENT  
ZONING

R

First Record Date  
Planning Board Use only

DATE OF THIS  
DOCUMENT

5/16/28

FILE:  
TITLE:

**APPLICATION FOR SPECIAL PERMIT**

File two (2) completed copies of this application. One (1) copy with the Planning Board and one (1) copy with the Town Clerk in accordance with the Zoning Bylaws. The filing fee as calculated by Appendix A, made payable to the Town of Dighton.

To the Dighton Planning Board:

PROJECT NAME: Brook Street Solar

SUBJECT PROPERTY ADDRESS: 893 Brook Street

ASSESSOR'S MAP/LOT(s): Map 16 - Parcel 28

ALL APPLICABLE ZONING DISTRICT: Residence & Agricultural (RA)

TITLE OF PLAN: Brook Street Solar; Basin 1 & 3 Repair

PLAN DATED: May 3, 2024

DESCRIBE WHAT IS PROPOSED FOR THIS PROPERTY:

Construct and maintain a 2.7 +/- MWac Groundmounted Solar Photovoltaic Systems. The site is currently under construction under a Special Permit issued by the Dighton Planning Board on January 16, 2019.

STATE THE EXACT NATURE OF ACTION OR RELIEF REQUESTED BY THIS APPLICATION AND CITE THE APPLICABLE BYLAW(s) AND/OR BYLAW SECTION(s):

The Applicant is seeking a major modification to the Special Permit issued by the Dighton Planning Board on January 16, 2019. The requested modification is to install a 4" subdrain and outlet to the infiltration basin which has been installed at the site. Currently, the installed infiltration basin is not fully draining within 72-hours as required and the installation of the 4" drain will allow for the basin to slowly drain the stormwater runoff which cannot be infiltrated by the basin.

DESCRIBE HOW THIS APPLICATION MEETS THE CRITERIA FOR A SPECIAL PERMIT AS DESCRIBED IN THE APPLICABLE SECTION(S) OF THE DIGHTON ZONING BYLAWS:

The Application is for a minor change to the infiltration basin configuration and will not change the current approved use of the site.

THE UNDERSIGNED HEREBY CERTIFIES THAT THE INFORMATION ON THIS APPLICATION AND PLANS SUBMITTED HERewith IS CORRECT, AND THAT THE APPLICATION COMPLIES WITH ALL APPLICABLE PROVISIONS OF STATUTES, REGULATIONS AND BYLAWS TO THE BEST OF HIS/HER KNOWLEDGE.

THE ABOVE IS SUBSCRIBED TO AN EXECUTED BY THE UNDERSIGNED UNDER THE PENALTIES OF PERJURY IN ACCORDANCE WITH M.G.L. Ch. 268, §1-A.

RECEIVED

Received by Town Clerk: Town Clerk-Dighton, MA

Date: MAY 07 2024  
Time: \_\_\_\_\_

Time: 9:28 AM

By: se

Received by Board of Health

Date: \_\_\_\_\_  
Time: \_\_\_\_\_  
Signature: \_\_\_\_\_

Applicant's Name GHTJA03 LLC  
Applicant's Address 4 Bobbie Ct Manalapan  
NJ 07726  
Applicant's Phone # 416-477-0726  
Signature: \_\_\_\_\_

Owner's name, address and signature for authorization (if other than applicant)

Owner's Name Mil~ Andrews  
Owner's Address 135 Sherman Lane  
Raynham MA 02767  
Owner's Phone# 774 501 7899  
Signature: Mil

Checklist of items to be submitted with application.

- 1.  Application Form (x2)
- 2.  Application Fee (please refer to Fee Schedule)
- 3.  Project Review Fee & Completed W-9 (please refer to Fee Schedule)
- 4.  Tax Status Application Form
- 5.  Plans (See applicable Zoning Bylaws for Specific Requirements)
- 6.  Certified Abutters List

RECEIVED

MAY - 6 2024

By: Dighton Planning Board



May 6, 2024

Town of Dighton Planning Board  
979 Somerset Avenue  
Dighton, MA 02715

Re: Brook Street Solar-Commercial Solar Facility  
Special Permit Modification  
893 Brook Street, Dighton, MA  
Assessor Map 16; Parcel 28

Members of the Planning Board,

Level Design Group, L.L.C. (LDG), on behalf of the project developer, GHTJA03, LLC (Grasshopper Energy), is submitting a request for a major modification to the current issued special permit for the above-referenced parcel. The Town of Dighton Planning Board originally issued a special permit on January 16, 2019 for the development of a ground-mounted solar photovoltaic installation with a subsequent major modification for the installation of a Battery Energy Storage System (BESS) approved by the Board on March 2, 2022. The Board reviewed and approved an additional minor modification to reconfiguration of the site entrance driveway on January 6, 2021. Copies of all record-issued permits and plans are included with the application package.

The current request for a major modification to the issued special permit is for a redesign of stormwater Basin 1 which is currently retaining stormwater for a prolonged period. The original approved basin design was for a fully infiltrating stormwater basin with no pipe outlets which was intended to fully drain within 72 hours as required by current Massachusetts Stormwater Management Standards. The Applicant has been working with the Town of Dighton Stormwater Committee over the past three years on addressing issues with Basin 1 regarding its construction. The original site contractor installed the basin without the required inspections from the Stormwater Agent or the site engineer and chose to mine material from the floor of the basin and backfill that area with unsuitable materials (organic material, stumps, wood chips, etc.) to a depth ranging between 4'-12'. Since that time basin has been reconstructed to reflect the approved basin geometry and configuration along with removing all unsuitable material from the basin floor and backfilling it with clean sand.

Despite the corrective measures that have been implemented the basin is still retaining stormwater for a prolonged period and is not fully draining within 72 hours as required. The Dighton Stormwater Committee has recently enlisted the services of Weston & Sampson to review the basin and provide recommendations on how to repair the basin so that it will fully drain within 72 hours. Weston & Sampson have provided two review letters dated December 11, 2023, & March 15, 2024, addressed to the Town of Dighton Stormwater Committee with their findings and recommendations which are included with the application package. Based on a review of the findings and recommendations by Weston & Sampson, LDG has prepared an updated basin design with, supporting calculations, for the install the installation of a new 4" basin subdrain. The subdrain consists of a network of 4" perforated pipes set into the crushed stone basin floor which discharge via a 4" solid PVC pipe to be located within the existing rip-rap spillway. The 4" perforated subdrain will allow to basin to continue to function as an infiltrating basin with water being able to drain through the perforated pipes and basin floor. When the subsoil becomes saturated and can no longer infiltrate, stormwater will then drain slowly through the 4" pipe draining the basin down within 72 hours.

The requested major modification is to allow for the reconfiguration of stormwater Basin 1 as shown on the provided plan for the installation of the new subdrain and 4" piped discharge. The recommendations and calculations included are based on a drainage as-built survey prepared by LDG dated November 17, 2022. The drainage as-built survey

Special Permit Modification  
Brook Street Solar  
Dighton, MA  
May 6, 2024



details existing as-built site grades within the basin footprints, installed outlets, and installed solar panel racking within the basin areas to provide an accurate representation of the stormwater basins as currently installed.

In addition to the requested modification of Basin 1, the design plan prepared by LDG also includes maintenance items recommended by Weston and Sampson to be completed for stormwater Basin 3. These items are not part of the request for the major permit modification as there is no proposed design change to Basin 3. The recommended maintenance includes some minor re-grading of the basin floor and adjusting the currently installed outlet pipe to match the regraded basin floor.

Enclosed please find the following:

- Five (5) copies of the Basin Repair Plan dated April 15, 2024
- Five (5) copies of supporting information
- Two (2) copies of the Application form
- Municipal Lien Certificate
- Certified Abutter List
- Filing Fee - \$500.00 for Special Permit Modification
- Consultant Fee Deposit - The Applicant currently has a 53G Account with the Town for ongoing reviews with Weston and Sampson. Additional funds will be provided, if necessary, for any review work requested by the Planning Board.

If there are any questions before the hearing please do not hesitate to contact me.

Truly yours,  
LEVEL DESIGN GROUP, LLC

*Nicola Facendola*

Nicola Facendola, P.E.  
Principal

CC: Grasshopper Energy, Town of Dighton Fire Department, Building Department, Conservation Commission, Board of Health, and Highway Department

**REQUEST TO MODIFY SPECIAL PERMIT**

*for*

**BROOK STREET SOLAR  
COMMERCIAL PHOTOVOLTAIC SYSTEM  
0 BROOK STREET  
(AM 16, PARCEL 28)  
DIGHTON, MASSACHUSETTS**

MAY 6, 2024

Prepared By:  
**Level Design Group, L.L.C.**  
**249 South Street, Unit 1**  
**Plainville, MA 02762**

Prepared For:  
GJTJA03, LLC  
1209 ORANGE STREET  
WILMINGTON, DELAWARE 19801

***LDG Project No.:***  
***1817.00***

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7. Copy of Current Approve Site Plans (reduced) –September 28, 2021
8. Copy of Minor Modification Approval for Driveway Modification – Approved January 6, 2021
9. Copy of Driveway Modification Site Plan - Approved January 6, 2021
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May 6, 2024

Town of Dighton Planning Board  
979 Somerset Avenue  
Dighton, MA 02715

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Special Permit Modification  
893 Brook Street, Dighton, MA  
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Special Permit Modification  
Brook Street Solar  
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Truly yours,  
LEVEL DESIGN GROUP, LLC

*Nicola Facendola*

Nicola Facendola, P.E.  
Principal

CC: Grasshopper Energy, Town of Dighton Fire Department, Building Department, Conservation Commission, Board of Health, and Highway Department



PETITIONER  
NAME &  
ADDRESS

**TOWN OF DIGHTON**

**PLANNING BOARD**

LOCATION (from Assessors' Office)  
PLAT AND  
LOT NOS.

PRESENT  
ZONING

First Record Date  
Planning Board Use only

DATE OF THIS  
DOCUMENT

FILE:  
TITLE:

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December 11, 2023

Dighton Stormwater Committee  
C/O Nancy Goulart, Chairwoman  
1111 Somerset Avenue  
Dighton, MA 02715

Re: **893 Brook Street Solar Field – Stormwater Basin Review**

Dear Stormwater Committee:

In accordance with your request, Weston & Sampson has conducted its initial review of the stormwater basins that were constructed as part of the solar energy project located at 893 Brook Street. Our review has been conducted in response to concerns about long-term standing water in the basins, and especially with regard to the stormwater basin located at the northern end of the site that was intended to function as a stormwater infiltration basin. With this letter we are providing you with our findings from our review and recommendations for next steps.

Weston & Sampson received numerous documents that were produced through the life of the project going back to 2018. While all documents were reviewed, certain documents stood out due to their relevance to the issue at hand; these are listed as follows:

- A report entitled “Stormwater Report for Brook Street Solar Project” by Atlantic Design Engineers, Inc., 80 pages, dated 7/16/2018
- A report entitled “Stormwater Report Addendum 1 for Brook Street Solar Project” by Atlantic Design Engineers, Inc., 52 pages, dated 11/19/2018
- A report entitled “Stormwater Report Addendum 2 for Brook Street Solar Project” by Atlantic Design Engineers, Inc., 14 pages, dated 12/5/2018
- Plans entitled “Brook Street Solar Commercial Photovoltaic System” by Level Design Group, annotated “for construction,” 10 sheets, dated 1/29/2021
- Plans entitled “Brook Street Solar Stormwater Basin Repair Plan” by Level Design Group, 3 sheets, dated 9/16/2022
- A plan entitled “Drainage As-Built, Brook Street Solar” by Level Design Group, 1 sheet, dated 11/17/2022
- A letter report from Level Design Group (LDG) to the Dighton Stormwater Committee, 50 pages, dated 2/27/2023
- A review letter prepared by Green International Affiliates, 3 pages, dated 6/22/2023

In general, a review of the documents listed above and others within the file indicate a history of various approvals, modifications of approvals, plan revisions and technical reviews leading up to present. Without listing a complete history, a timeline of certain key events is as follows:

7/16/2018	Date of Special Permit Application
11/1/2018	Test pits conducted onsite
11/19/2018	Stormwater Report Addendum #1 issued
12/5/2018	Stormwater Report Addendum #2 issued
1/16/2019	Site Plan Approval and Special Permit issued
2/10/2021	Stormwater Permit issued by the Board of Health
3/30/2022	Additional test pits were performed identifying unsuitable materials beneath the basins
9/16/2022	Plans issued for required basin repairs
10-11/2022	Basin repair construction activities were performed over October and November of 2022
11/17/2022	Stormwater as-built drawing was issued
12/21/2022	A site visit occurred to look at existing conditions, areas of basins were requested to be re-graded
2/22/2023	A site visit was conducted by LDG after 0.18-inches of rainfall
2/27/2023	LDG issued an as-built summary letter with stormwater calculations
6/7/2023	A site visit was conducted by Green International Affiliates

## Findings

Based upon our review of the project documentation, we offer the following findings and comments. In the context of these findings, it should be noted that the site has two stormwater basins. The northern basin, located closest to Brook Street, is identified as "Basin 1" and the southerly basin is identified as "Basin 3," which is consistent with the nomenclature used for these basins throughout the project documentation.

1. The project documents indicate that the stormwater basins as currently constructed differ from the approved design. Some of these differences include the elevations of the basin bottoms, basin embankments, and spillway elevations. Additionally, Basin 3 had pipe outlets with differences between design and as-built elevations. The differences are reported below based on a review of the as-built drawings vs. two versions of the design drawings:

<b>Basin 1</b>	<b>Bottom Elev.</b>	<b>Embankment Elev.</b>	<b>Spillway Elev.</b>	
Design 1/29/2021	77	79.7	78	
Design 9/16/2022	77	79.7	78	
As-Built	76	79.2	78.7	
<b>Basin 3</b>	<b>Bottom Elev.</b>	<b>Embankment Elev.</b>	<b>Spillway Elev.</b>	<b>Outlet</b>
Design 1/29/2021	77	79.1	78	77.00/77.00 6" vertical pipe openings
Design 9/16/2022	77	79.1	78.05	77.00/77.00 6" vertical pipe openings
As-Built	76.5	78.8	78.5	77.60/77.55 6" horizontal elbow openings

*Data above based on WSE observations of applicant materials*

2. According to the as-built analysis (2/27/2023) Basin 1 is intended to perform as an infiltration basin with the intent that runoff entering the basin should infiltrate into underlying soil and infiltrate within 72 hours of entering the basin for storms. Storms that exceed the 25-year storm would result in some overflow at the spillway. The as-built analysis indicates that if this basin were performing as intended, it would perform somewhat better than the original design which allowed some overflow to occur at the 25-year event.
3. According to the as-built analysis (2/27/2023) Basin 3 is intended to perform as a detention basin with the runoff entering the basin slowly draining via pipe outlets until the basin is fully drained and left in a dry state. Under conditions wherein the basin performs as intended, no overflow should be expected over the spillway even in the 100-year storm event. This reflects better performance than the original design in which some overflow was allowed in the original design. That being said, the performance that is being reported in the as-built analysis may differ due to an issue noted in the following comment.
4. In performing a review of the Basin 3 outlet pipe elevations shown on the as-built plans as compared with the as-built analysis, a discrepancy was noted. The plans indicate that there are two 6-inch horizontal elbow openings at elevations of 77.6 and 77.55, whereas calculations in the analysis indicate that both are at elevations of 77.10. This means that Basin 3 would have less available storage than what is reflected in the as-built analysis and may discharge during smaller storms than indicated in applicant materials.
5. In reviewing various project documentation, as-built drawings and photographs, it appears that Basin 3 has an area in its northern half that was constructed at a lower elevation than the pipe elbow outlets. This seems to have resulted in standing water in the basin. Generally, a detention basin is required to be graded such that all runoff will drain into its outlets so that the basin can fully drain to a dry state. The as-built letter (2/27/2023) reports that basin floors were "re-worked," but the review letter by Green International Affiliates indicates that both basins still had standing water during a site visit on June 7, 2023, which suggests that Basin 3 may still need to be properly re-graded to drain to its outlets.
6. The designs of both basins were reviewed relative to test pits presented in Stormwater Report Addendum #1. The as-built conditions of both stormwater basins appear to be such that the floors of both basins are higher in elevation than the reported seasonal high groundwater from the test pits, and there appears

to be at least two feet of separation between the reported seasonal high groundwater elevations and Basin 1, meets the Massachusetts requirements for infiltration basins.

7. Project documentation indicates what appears to have been a thoroughly inspected construction activity in fall 2022 involving the removal of unsuitable material that had been placed beneath the floor of each basin. This material was reportedly replaced with free-draining material (Title V sand), and the basins are presently topped off with a geotextile filter fabric and processed stone.
8. In its as-built letter, LDG indicates that a site visit was conducted on 2/22/2023 after a rain event of 0.18-inches from the previous day and no standing water was observed.

### ***Conclusions and Recommendations***

1. Basin 3 should be re-graded further to eliminate the presence of standing water. Additionally, the basin should be re-analyzed due to the inconsistency between as-built surveyed outlet elevations and the elevations reported in LDG's analysis to confirm that it will perform as required.
2. Based upon the performance issues associated with Basin 1, further site investigation may be warranted to verify the cause of the problem. In general, an infiltration basin that remains inundated for an extended period could be experiencing one or more of the following issues:
  - a. The materials at the bottom of the basin could be clogged with fine sediment, creating a restrictive layer at or near the surface that slows or stops flow from occurring.
  - b. The bottom of the basin could have been installed below the elevation of seasonal high groundwater.
  - c. The material at or beneath the bottom of the basin could have been compacted during construction, reducing the hydraulic conductivity rate of the soil.
  - d. The material at or beneath the bottom of the basin could be too fine-grained and could have a very low hydraulic conductivity rate.

The potential issues listed above are ranked in order starting from the potential cause that we see as being most likely and ending with that which seems least likely based upon our review and the information that we have at this time. The issue of sediment clogging could be a likely factor given that the site has seen construction activity within the past year and may not be fully stabilized. The basin was reported to have performed acceptably in February 2023 but by June 2023 issues of standing water were observed; fine sediment could have accumulated within that intervening period. It is worth noting that LDG indicates that a layer of stone and filter fabric were used in the upper layer of the basin floor; filter fabric can sometimes act as a sediment trap, collecting fine sediment and creating a restrictive layer. Consequently, though no fine sediment may be visible on the surface, our first recommendation would be to remove material down to the filter fabric to see if the fabric has become clogged.

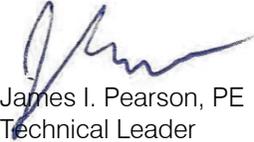
If fabric clogging has not occurred, the need for additional excavation and/or testing should be discussed, or it may be necessary to consider the possibility that elevated groundwater could be a concern. It is acknowledged that the basin appears to have been built correctly relative to seasonal high groundwater estimates, and that those estimates were obtained using accepted practices, but if other possible causes are exhausted it may become necessary to review this issue further in which case we may recommend the installation of a monitoring well.

Soil compaction and the presence of fine-grained soils were low on the list above due to several factors, such as original test pit data, the apparent level of care taken to remove and replace unsuitable materials in the basin, and the acceptable performance that was found to occur in February 2023. If further test pitting were to be conducted as discussed above, then these factors could be investigated further if warranted.

Weston & Sampson appreciates the opportunity to present our findings, and we look forward to discussing the next steps toward resolving the issues related to stormwater management at this project site. Please contact Jim Riordan if you have any questions. Jim Riordan may be reached at (401) 497-6705 or riordanj@wseinc.com.

Sincerely,

WESTON & SAMPSON ENGINEERS, INC.



James I. Pearson, PE  
Technical Leader



M. James Riordan, LEED AP  
Team Leader

March 15, 2024

Dighton Stormwater Committee  
C/O Nancy Goulart, Chairwoman  
1111 Somerset Avenue  
Dighton, MA 02715

Re: **893 Brook Street Solar Field – Findings from Site Visit and Soil Testing**

Dear Stormwater Committee:

In accordance with your request, Weston & Sampson has performed follow-up work subsequent to the initial document review that was presented in our letter dated December 11, 2023. This work has consisted of a visit to the site on February 6, 2024 and a review of the testing results that were performed on February 22, 2024 for materials sampled from that site. The test results were received by us on March 1, 2024 and consisted of nine separate soil grain size distribution reports, one for each sample taken.

### ***Findings***

In our initial review of the project documentation, it had appeared that a geotextile fabric layer had been installed in the bottom of the basin beneath a layer of stone. Upon visiting the site on the morning of February 6, we learned that there was no geotextile fabric or stone present at the surface of the basin. Surficial materials appeared to have a sandy consistency. Standing water at a depth of 2 to 4-inches was observed at the lower end of the basin. General reconnaissance was conducted around the periphery of the site to the north and east of the basin and no standing water was observed in those areas. The areas to the east of the basin slope steeply downward to elevations 5 to 7 feet below the basin floor elevation based on record drawings.

Two test pits were excavated onsite to depths of approximately 10 to 12 feet in depth. Test Pit #1 was excavated in the eastern end of the basin and Test Pit #2 was excavated in the western end of the basin. Both test pits encountered similar conditions. In both cases, a tan-colored sand material was encountered for nearly the entire depth. The upper 4 to 5 feet of material was loose and moist, with minimal cohesion and caving occurring throughout the excavation. From 4 to 5 feet and lower, the sand was heavily saturated, with heavy weeping occurring in the sides of the pit as excavation progressed. Both test pits were advanced to find material below the sand layer. At the bottom of each pit, a material that appeared to be a blue-gray clay with an organic odor was encountered. Samples were taken in each pit at the top, middle, and bottom of the test pits. In addition, a sample of the blue-gray clay material at the bottom of the test pits was taken at the base of each test pit. Finally, Test Pit #2 was expanded laterally to sample material approximately 4 to 5 feet down at the edge of the sand-fill area of the basin to characterize what seemed to be native material outside of the footprint of the basin.

Laboratory testing confirms that the sand material taken at the top, middle, and bottom of each test pit is of a very similar gradation of sand. The testing results for the “blue-gray clay” material at the base of each test pit indicates that it could fall either in the sandy loam or sandy clay loam classification; however, due to sampling methods it is believed that some of the overlying sand material may have been mixed in with the clay sample. Visual observation at the time of the site visit suggests that the underlying material is likely a clay loam or finer.

The laboratory results for the sample taken at the lateral edge of Test Pit #2 likewise also indicate a material that is either a sandy loam or sandy clay loam. Visual observations of the material onsite suggest that the material likely falls closer to the finer-grained end of that spectrum (i.e. sandy clay loam).

### ***Conclusions and Recommendations***

Based on the findings presented above as well as the findings presented in our previous initial document review letter, it appears that the material within the bottom of the stormwater basin is a very free-draining sand material that should be expected to allow stormwater infiltration to occur at a rapid rate; however, material 10 to 12 feet

below the basin as well as material around the periphery of the basin appears to be a finer grained material with a low hydraulic conductivity, meaning that stormwater would be expected to pass through these materials at a very slow rate. We believe that the problems with standing water in the basin that has been present for periods greater than 72 hours can likely be attributed to the low hydraulic conductivity of the materials below and surrounding the basin. During recent periods of significant rainfall events, we believe that the sand material became saturated with stormwater, at which point the hydraulic conductivity of the materials surrounding and beneath the basin became the controlling factor in how quickly the basin was able to infiltrate. Since these soils have a low hydraulic conductivity, the basin was unable to drain within the 72-hour period prescribed under the MA Stormwater Handbook.

It is anticipated that the conditions described above will likely recur during periods of frequent heavy rainfall. Site conditions do not appear to be favorable for the stormwater basin to function as an infiltration basin if it is expected to drain within 72 hours. Under the standards of the MA Stormwater Handbook, sites that are not adequate to support the installation of infiltration basins are generally allowed to seek waivers to allow infiltration only to the "maximum extent practicable." As such, we recommend that the Stormwater Committee allow the owner of the site to consider potential modifications to the stormwater management to the site that take into account a possible waiver request of this nature. It is the responsibility of the owner's engineer to determine what that modification would consist of, but one potential solution may include the conversion of the infiltration basin into a detention basin that allows for infiltration to the maximum extent practicable while also preventing standing water from occurring for periods greater than 72 hours. In considering any modifications to the basin, we believe the site owner's engineer should seek to ensure that all other standards that were met as part of the original design should continue to be met.

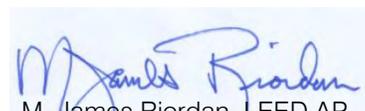
Weston & Sampson appreciates the opportunity to present our findings, and we look forward to discussing the next steps toward resolving the issues related to stormwater management at this project site. Please contact Jim Riordan if you have any questions. Jim Riordan may be reached at (401) 497-6705 or [riordanj@wseinc.com](mailto:riordanj@wseinc.com).

Sincerely,

WESTON & SAMPSON ENGINEERS, INC.



James I. Pearson, PE  
Technical Leader



M. James Riordan, LEED AP  
Team Leader

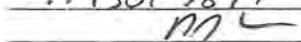
DESCRIBE HOW THIS APPLICATION MEETS THE CRITERIA FOR A SPECIAL PERMIT AS DESCRIBED IN THE APPLICABLE SECTION(S) OF THE DIGHTON ZONING BYLAWS:

The Application is for a minor change to the infiltration basin configuration and will not change the current approved use of the site.

THE UNDERSIGNED HEREBY CERTIFIES THAT THE INFORMATION ON THIS APPLICATION AND PLANS SUBMITTED HERewith IS CORRECT, AND THAT THE APPLICATION COMPLIES WITH ALL APPLICABLE PROVISIONS OF STATUTES, REGULATIONS AND BYLAWS TO THE BEST OF HIS/HER KNOWLEDGE.

THE ABOVE IS SUBSCRIBED TO AN EXECUTED BY THE UNDERSIGNED UNDER THE PENALTIES OF PERJURY IN ACCORDANCE WITH M.G.L. Ch. 268, §1-A.

Received by Town Clerk:	Applicant's Name	GHTJA03 LLC
Date: _____	Applicant's Address	4 Bobbie Ct Manalapan
Time: _____		NJ 07726
	Applicant's Phone #	416-477-0726
	Signature:	

Received by Board of Health	Owner's name, address and signature for authorization (if other than applicant)	
Date: _____	Owner's Name	Mil- Andrews
Time: _____	Owner's Address	135 Sherwood Lane
Signature: _____		Royalton MA 02767
	Owner's Phone#	774 501 7888
	Signature:	

- Checklist of items to be submitted with application.
1.  Application Form (x2)
  2.  Application Fee (please refer to Fee Schedule)
  3.  Project Review Fee & Completed W-9 (please refer to Fee Schedule)
  4.  Tax Status Application Form
  5.  Plans (See applicable Zoning Bylaws for Specific Requirements)
  6.  Certified Abutters List



## TOWN OF DIGHTON

PLANNING BOARD  
979 SOMERSET AVENUE  
DIGHTON, MA 02715  
TEL: (508) 669-6636  
FAX: (508) 669-4509

20 Day  
Appeal  
expires on  
2-6-2019

### FINDINGS AND DECISION

RE: SPECIAL PERMIT & SITE PLAN REVIEW FOR GROUND-MOUNTED SOLAR PHOTOVOLTAIC INSTALLATION

APPLICANT: TJA SOLAR

DATE: JANUARY 16, 2019

1. On or about July 16, 2018, the TJA Solar (the "Applicant") submitted an application for a special permit with a site plan review for ground-mounted solar photovoltaic installation at property comprised of about  $\pm 8$  acres of a  $\pm 19.6$  acre tract of land at 0 Brook Street in Dighton, Massachusetts (the "Locus"), identified in the Assessor's records as Map 16, Lot 28. The owner-of-record of the Locus is Estates of Louise a Andrews.
2. On September 5, 2018, the Planning Board commenced a public hearing on the Application. Said public hearing was continued to October 3, 2018, October 26, 2018, November 28, 2018, December 5, 2018 and closed on December 19, 2018.
3. The proposal is to allow the installation and operation of a  $\pm 3$  MW Ground-Mounted Solar Photovoltaic Array in a Residential District in accordance with Section 4600 and 5400 of the Town of Dighton Zoning Bylaws.
4. Special Permit applications are accompanied by and augmented by Site Development Plans, entitled Site Development Plans for Brook Street Solar Project ("Plans"), Dighton, Massachusetts, dated July 16, 2018, last revised December 19, 2018, prepared by Atlantic Design Engineers, Inc., PO Box 1051, Sandwich, MA 02563.

### FINDINGS

#### General

The Applicant proposes to construct a  $3.4\pm$  MW Ground-Mounted Solar Photovoltaic Array Installation as shown on the Plans and described in the Special Permit Application. In accordance with Section 4600 of the Bylaw, where the Ground Mounted Solar

Photovoltaic Installation Array is located in a Residential District, a Special Permit is required, in addition to Site Plan Review.

### Special Permit Criteria

The determination of the Planning Board shall include consideration of each of the following:

1. Social, economic or community needs which are served by the proposal;
2. Traffic flow and safety, including parking and loading;
3. Adequacy of utilities and other public services;
4. Neighborhood character and social structures;
5. Impacts on the natural environment; and
6. Potential fiscal impact, including impact on town services, tax base, and employment.

Specifically, as to the Special Permit request, the Board found as follows:

1. The project will have a positive impact on the general social, economic and community needs by providing a renewable energy source in town with added economic benefits to both the property owner and other employed by the work of the installation. Generally, an overall community benefit is realized with the addition of renewable energy sources.
2. There will be no adverse effect to the community or neighborhood from increased traffic flow or safety. Any such impact will be negligible over the long run.
3. There are adequate utilities and other public services.
4. There will be no impact to the neighborhood character and social structures. Indeed, the location of the facility will have little to no impact.
5. The installation will not have any meaningful negative impacts on the natural environment. However, the result of the use of the solar facility will have far reaching positive impacts; and
6. The Town will receive increased personal property tax revenue and there will be positive fiscal impacts to the tax base, and employment.

The Applicant meets the criteria of the Special Permit as set forth above, provided that the Applicant comply with the conditions hereof.

### **DECISION**

The Planning Board, at its meeting of December 19, 2018, voted to Approve the Site Plan application and Special Permit for the proposed solar facility as shown on the Plans.

In view of the foregoing, the Planning Board hereby decides that the aforesaid proposed Ground Mounted Solar Photovoltaic Installation Array is proposed, as set forth on the Plans, in a manner consistent with the requirements of Section 4600 and 5400 of the Town of Dighton Zoning Bylaws in that it meets all requisite criteria. It is therefore

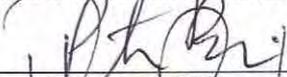
further determined, that subject to satisfaction of the conditions as set forth below that any perceived adverse effects of the proposed use will not outweigh its beneficial impacts to the Town of the neighborhood, in view of the particular characteristics of the site and of the proposal. Therefore, the Planning Board hereby grants a Special Permit for the installation and operation of a 3.4± MW Ground Mounted Solar Photovoltaic Installation Array in a Residential District subject to the Conditions:

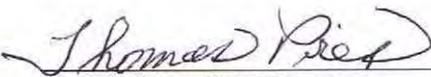
### CONDITIONS

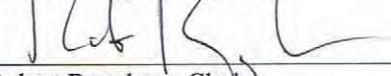
1. The Applicant has agreed to obtain approval of the revised plan (dated December 19, 2018 relocating the entrance) from The Town's engineer, the Fire Chief and the Conservation Commission. No construction of the project may commence and no building permit may issued unless and until such approvals are provided.
2. The Applicant shall obtain approval of the Stormwater Report from the Board of Health prior to the issuance of a building permit.
3. The Applicant shall submit detail of electrical equipment pads and spill prevention measures to the Planning Board prior to the issuance of a building permit.
4. The Applicant shall submit the names and address of the system installer to the Planning Board prior to the issuance of a building permit.
5. The Applicant will work with the Building Department and comply with all requirements regarding signage and lighting in accordance with the Zoning Bylaws Section 3300 prior to the issuance of a building permit.
6. The Applicant is hereby granted a waiver of underground utilities in the area of the wetland crossing, provided that the Conservation Commission approves above-ground wires.
7. The Applicant further agrees to an additional \$10,000 in landscape screening for the front of the property. The Applicant has agreed to a Landscape Performance Security Agreement prior to the issuance of a building permit. Such agreement shall be in the amount of \$10,000.00, and shall be in a form approvable by the Board's counsel.
8. The Applicant has prepared and presented an Emergency Response Plan and the layout of the access drive to the Fire Chief. The Fire Chief's approval of said plan is required prior to the issuance of a building permit.
9. The Applicant has agreed to posting Decommissioning Security with the Town of Dighton in the estimated amount of \$139,300.00 prior to the issuance of a building permit. The form of such security agreement is subject to the prior approval of the Board's counsel and final confirmation of the amount of such security.

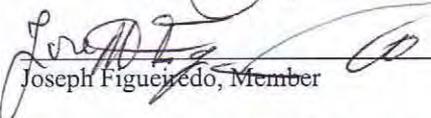
10. The Applicant has agreed to install additional traffic signs on Pine and Brook Street in accordance with requirements and standards of the Highway Superintendent. Such signs shall be installed prior to the commencement of operation of the solar facility
11. The Applicant has agreed to submit a Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan for the Board's approval prior to the issuance of a building permit. The Board utilize the services of an engineer to review such plan, and the Applicant shall bear all costs for such review, pursuant to G.L. c. 44, s. 53G.
12. The Applicant has agreed to posting Security for the drainage system construction prior to the issuance of a building permit. The security agreement shall be in the amount of \$30,000.00, and shall be in a form approvable by the Board's counsel.

**DIGHTON PLANNING BOARD**

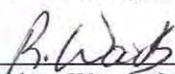
  
 \_\_\_\_\_  
 Peter Bouvie, Jr., Chairman

  
 \_\_\_\_\_  
 Thomas Pires, Vice Chairman

  
 \_\_\_\_\_  
 Robert Boughner, Clerk

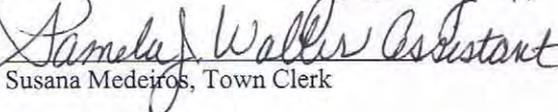
  
 \_\_\_\_\_  
 Joseph Figueiredo, Member

The following members of the Planning Board are in opposition to the grant of the special permit:

  
 \_\_\_\_\_  
 Robert Woods, Member

\_\_\_\_\_

Filed with the Town Clerk on January 17, 2019.

  
 \_\_\_\_\_  
 Susana Medeiros, Town Clerk

**RECEIVED**  
 2019 JAN 17 AM 10:16  
 TOWN CLERK  
 DIGHTON, MA

# SITE DEVELOPMENT PLANS FOR BROOK STREET SOLAR PROJECT

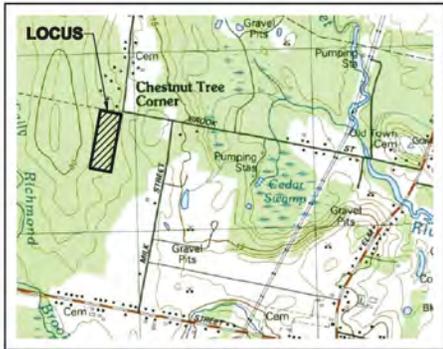
DIGHTON, MASSACHUSETTS

DATE: JULY 16, 2018

REVISED: NOVEMBER 19, 2018

REVISED: DECEMBER 5, 2018

REVISED: DECEMBER 19, 2018



VICINITY MAP  
1" = 1,500'



LOCUS MAP  
1" = 1,200'



OVERALL LOCATION PLAN  
SCALE: 1" = 200'

INDEX OF PLANS		
SHEET NO.	TITLE	SCALE
1	COVER SHEET	1" = 200'
2	OVERALL SITE DEVELOPMENT PLAN	1" = 80'
3	SITE DEVELOPMENT PLAN	1" = 40'
4	DETAILS PLAN	AS SHOWN
5	DETAILS PLAN	AS SHOWN

**OWNER:**

THE MANUAL & LOUISE TRUST  
12 CYPRESS DR,  
DARTMOUTH, MASSACHUSETTS 02747  
PHONE NUMBER: 505-967-7905

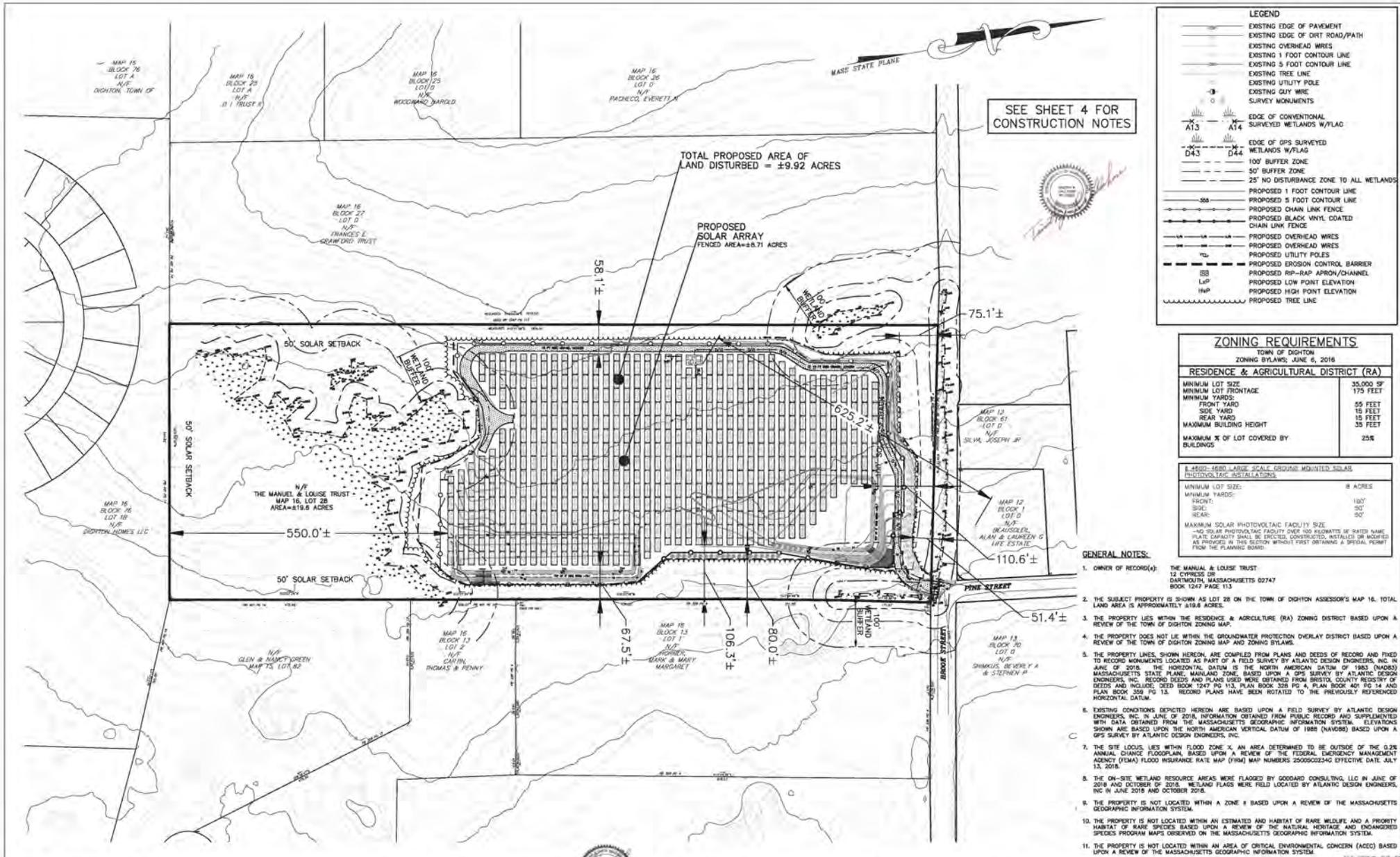
**APPLICANT:**

TJA SOLAR  
150 JOHN VERTENTE BOULEVARD  
NEW BEDFORD, MASSACHUSETTS 02745  
PHONE NUMBER: (774) 573-5726

**ENGINEER:**

**Atlantic**<sup>®</sup>  
DESIGN ENGINEERS, INC.  
P.O. Box 1051, Sandwich, MA 02563  
PHONE NUMBER: (508) 888-9282





**LEGEND**

- EXISTING EDGE OF PAVEMENT
- EXISTING EDGE OF DIRT ROAD/PATH
- EXISTING OVERHEAD WIRES
- EXISTING 1 FOOT CONTOUR LINE
- EXISTING 5 FOOT CONTOUR LINE
- EXISTING TREE LINE
- EXISTING UTILITY POLE
- EXISTING GUY WIRE
- SURVEY MONUMENTS
- EDGE OF CONVENTIONAL SURVEYED WETLANDS W/FLAG
- EDGE OF GPS SURVEYED WETLANDS W/FLAG
- 100' BUFFER ZONE
- 50' BUFFER ZONE
- 25' NO DISTURBANCE ZONE TO ALL WETLANDS
- PROPOSED 1 FOOT CONTOUR LINE
- PROPOSED 5 FOOT CONTOUR LINE
- PROPOSED CHAIN LINK FENCE
- PROPOSED BLACK VINYL COATED CHAIN LINK FENCE
- PROPOSED OVERHEAD WIRES
- PROPOSED UTILITY POLES
- PROPOSED EROSION CONTROL BARRIER
- PROPOSED RIP-RAP APRON/CHANNEL
- PROPOSED LOW POINT ELEVATION
- PROPOSED HIGH POINT ELEVATION
- PROPOSED TREE LINE

**ZONING REQUIREMENTS**  
TOWN OF DIGHTON  
ZONING BY-LAWS, JUNE 6, 2016

**RESIDENCE & AGRICULTURAL DISTRICT (RA)**

MINIMUM LOT SIZE	35,000 SF
MINIMUM LOT FRONTAGE	175 FEET
MINIMUM YARDS:	
FRONT YARD	55 FEET
SIDE YARD	15 FEET
REAR YARD	15 FEET
MAXIMUM BUILDING HEIGHT	35 FEET
MAXIMUM % OF LOT COVERED BY BUILDINGS	25%

**4-4600-4600 LARGE SCALE (GROUND MOUNTED) SOLAR PHOTOVOLTAIC INSTALLATIONS**

MINIMUM LOT SIZE:	8 ACRES
MINIMUM YARDS:	
FRONT:	100'
SIDE:	50'
REAR:	50'

**MAXIMUM SOLAR PHOTOVOLTAIC FACILITY SIZE**  
—NO SOLAR PHOTOVOLTAIC FACILITY OVER 100 KILOWATTS OR 5000 KW-HR PER YEAR SHALL BE RECORDED, CONVEYERED, MORTGAGED OR MODIFIED AS PROVIDED IN THIS SECTION WITHOUT FIRST OBTAINING A SPECIAL PERMIT FROM THE PLANNING BOARD.

- GENERAL NOTES:**
- OWNER OF RECORD(S): THE MANUAL & LOUISE TRUST  
12 CYPRESS DR  
DARTMOUTH, MASSACHUSETTS 02747  
BOOK 1247 PAGE 113
  - THE SUBJECT PROPERTY IS SHOWN AS LOT 28 ON THE TOWN OF DIGHTON ASSESSOR'S MAP 16. TOTAL LAND AREA IS APPROXIMATELY ±19.6 ACRES.
  - THE PROPERTY LIES WITHIN THE RESIDENCE & AGRICULTURE (RA) ZONING DISTRICT BASED UPON A REVIEW OF THE TOWN OF DIGHTON ZONING MAP.
  - THE PROPERTY DOES NOT LIE WITHIN THE GROUNDWATER PROTECTION OVERLAY DISTRICT BASED UPON A REVIEW OF THE TOWN OF DIGHTON ZONING MAP AND ZONING BYLAWS.
  - THE PROPERTY LINES, SHOWN HEREON, ARE COMPILED FROM PLANS AND DEEDS OF RECORD AND FIXED TO RECORD MONUMENTS LOCATED AS PART OF A FIELD SURVEY BY ATLANTIC DESIGN ENGINEERS, INC. IN JUNE OF 2018. THE HORIZONTAL DATUM IS THE NORTH AMERICAN DATUM OF 1983 (NAD83) MASSACHUSETTS STATE PLANE, MARLBOROUGH ZONE. BASED UPON A GPS SURVEY BY ATLANTIC DESIGN ENGINEERS, INC. RECORD DEEDS AND PLANS WERE OBTAINED FROM BRISTOL COUNTY RECORDS OF DEEDS AND INCLUDE: DEED BOOK 1247 PG 113, PLAN BOOK 328 PG 4, PLAN BOOK 401 PG 14 AND PLAN BOOK 358 PG 13. RECORD PLANS HAVE BEEN ROTATED TO THE PREVIOUSLY REFERENCED HORIZONTAL DATUM.
  - EXISTING CONDITIONS DEPICTED HEREON ARE BASED UPON A FIELD SURVEY BY ATLANTIC DESIGN ENGINEERS, INC. IN JUNE OF 2018. INFORMATION OBTAINED FROM PUBLIC RECORDS AND SUPPLEMENTED WITH DATA OBTAINED FROM THE MASSACHUSETTS GEOGRAPHIC INFORMATION SYSTEM. ELEVATIONS SHOWN ARE BASED UPON THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88) BASED UPON A GPS SURVEY BY ATLANTIC DESIGN ENGINEERS, INC.
  - THE SITE LOCUS LIES WITHIN FLOOD ZONE-X AN AREA DETERMINED TO BE OUTSIDE OF THE 0.2% ANNUAL CHANCE FLOODPLAIN, BASED UPON A REVIEW OF THE FEDERAL EMERGENCY MANAGEMENT AGENCY (FEMA) FLOOD INSURANCE RATE MAP (FIRM) MAP NUMBER 2505050224C EFFECTIVE DATE JULY 13, 2016.
  - THE ON-SITE WETLAND RESOURCE AREAS WERE FLAGGED BY GOODARD CONSULTING, LLC IN JUNE OF 2018 AND OCTOBER OF 2018. WETLAND FLAGS WERE FIELD LOCATED BY ATLANTIC DESIGN ENGINEERS, INC. IN JUNE 2018 AND OCTOBER 2018.
  - THE PROPERTY IS NOT LOCATED WITHIN A ZONE I BASED UPON A REVIEW OF THE MASSACHUSETTS GEOGRAPHIC INFORMATION SYSTEM.
  - THE PROPERTY IS NOT LOCATED WITHIN AN ESTIMATED HABITAT OF RARE WILDLIFE AND A PRIORITY HABITAT OF RARE SPECIES BASED UPON A REVIEW OF THE NATURAL HERITAGE AND ENDANGERED SPECIES PROGRAM MAPS OBSERVED ON THE MASSACHUSETTS GEOGRAPHIC INFORMATION SYSTEM.
  - THE PROPERTY IS NOT LOCATED WITHIN AN AREA OF CRITICAL ENVIRONMENTAL CONCERN (ACEC) BASED UPON A REVIEW OF THE MASSACHUSETTS GEOGRAPHIC INFORMATION SYSTEM.

**Atlantic** DESIGN ENGINEERS, INC.  
P.O. Box 1051, Sandwich, MA 02563 (508) 888 - 9282

Designed by: \_\_\_\_\_  
Drawn by: \_\_\_\_\_  
Checked by: \_\_\_\_\_  
Survey chk. by: \_\_\_\_\_  
Approved by: \_\_\_\_\_

**SCALE**  
SCALE 1" = 80'  
0' 40' 80' 160'



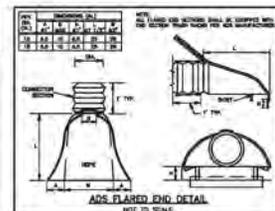
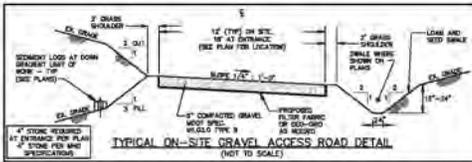
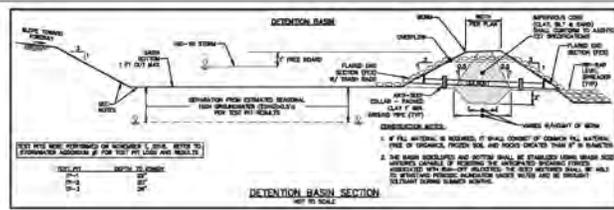
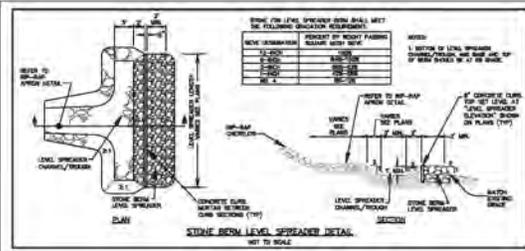
NO.	BY	DATE	REVISION
1	CMK	12-19-18	REVISED W/ ALTERNATIVE ACCESS
2	CMK	12-5-18	REVISED PER REVIEW COMMENTS
3	FMA	11-19-18	REVISED PER REVIEW COMMENTS

PREPARED FOR:  
**TJA SOLAR**  
150 JOHN VERTENTE BOULEVARD  
NEW BEDFORD, MASSACHUSETTS 02745

**OVERALL SITE DEVELOPMENT PLAN**  
FOR  
**BROOK STREET SOLAR PROJECT**  
DIGHTON, MASSACHUSETTS  
JULY 16, 2018

11.6 2992.01-910-40  
Sheet of **2** of **5**  
JOB NUMBER **2992.01**





**EROSION CONTROL NOTES:**

1. NEED TO CONSIDER EROSION CONTROL MEASURES OPERATIONAL, INSTALL EROSION CONTROL MEASURES AND MAINTAIN EROSION CONTROL MEASURES.
2. ALL EROSION CONTROL MEASURES SHALL BE INSTALLED AND MAINTAINED THROUGHOUT CONSTRUCTION. EROSION CONTROL MEASURES SHALL BE INSTALLED AND MAINTAINED THROUGHOUT CONSTRUCTION. EROSION CONTROL MEASURES SHALL BE INSTALLED AND MAINTAINED THROUGHOUT CONSTRUCTION.
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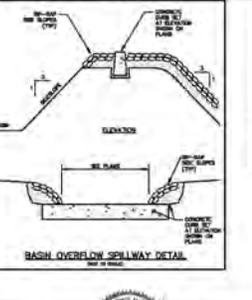
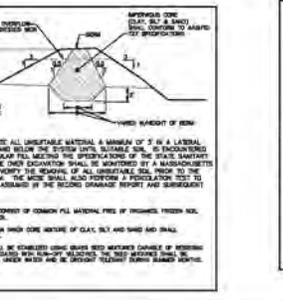
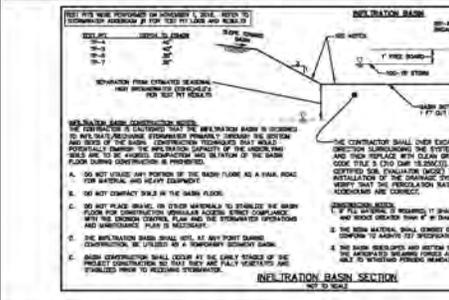
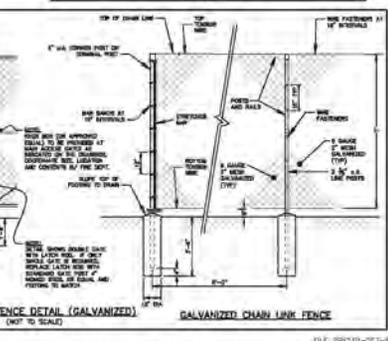
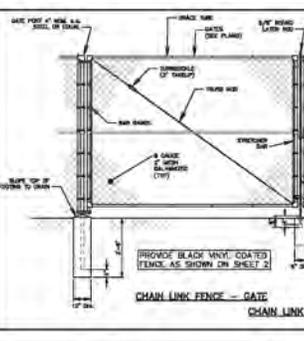
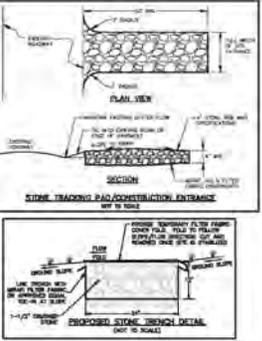
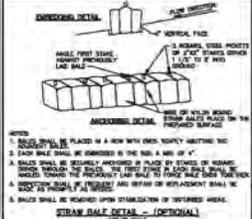
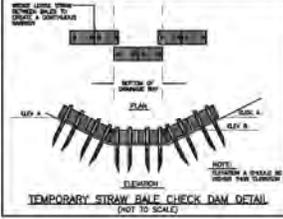
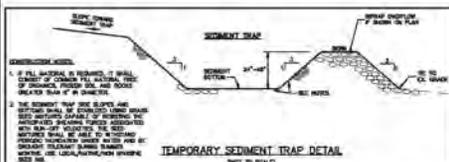
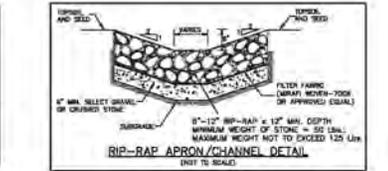
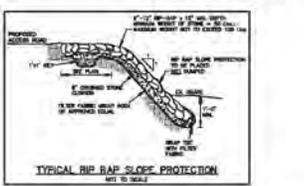
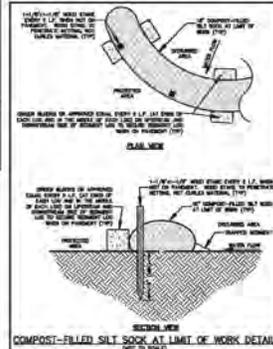
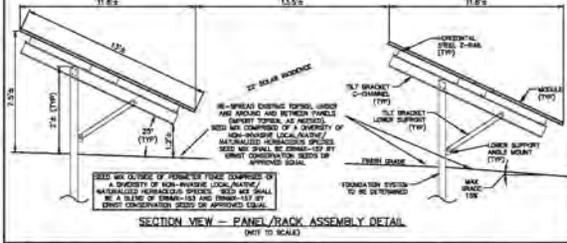
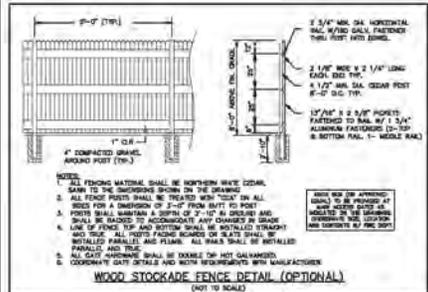
**CONSTRUCTION PERIOD SUSTAINMENT OPERATION AND MAINTENANCE:**

**GENERAL:**

1. THE CONTRACTOR SHALL MAINTAIN ALL EXISTING UTILITIES AND STRUCTURES AND SHALL BE RESPONSIBLE FOR ANY DAMAGE TO EXISTING UTILITIES AND STRUCTURES.
2. THE CONTRACTOR SHALL MAINTAIN ALL EXISTING UTILITIES AND STRUCTURES AND SHALL BE RESPONSIBLE FOR ANY DAMAGE TO EXISTING UTILITIES AND STRUCTURES.
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**CONSTRUCTION NOTES:**

1. THE CONTRACTOR SHALL MAINTAIN ALL EXISTING UTILITIES AND STRUCTURES AND SHALL BE RESPONSIBLE FOR ANY DAMAGE TO EXISTING UTILITIES AND STRUCTURES.
2. THE CONTRACTOR SHALL MAINTAIN ALL EXISTING UTILITIES AND STRUCTURES AND SHALL BE RESPONSIBLE FOR ANY DAMAGE TO EXISTING UTILITIES AND STRUCTURES.
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**Atlantic** DESIGN ENGINEERS, INC.  
 P.O. Box 1051, Sandwich, MA 02563 (508) 888 - 9282

Designed by: \_\_\_\_\_  
 Drawn by: \_\_\_\_\_  
 Checked by: \_\_\_\_\_  
 Survey data by: \_\_\_\_\_  
 Approved by: \_\_\_\_\_

SCALE: AS NOTED

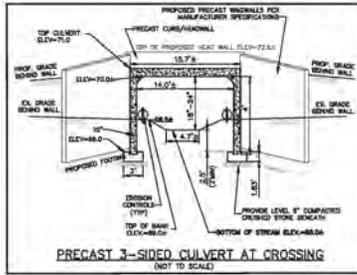
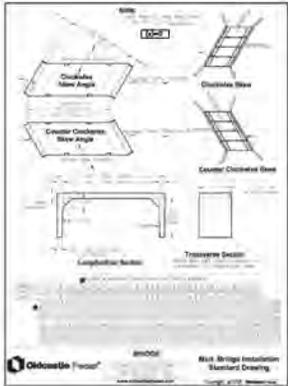


NO.	BY	DATE	REVISION
1	JMP	12-19-18	REVISED BY ALTERNATIVE ADDRESS
2	JMP	12-5-18	REVISED FROM REVIEW COMMENTS
3	JMP	11-19-18	REVISED FROM REVIEW COMMENTS

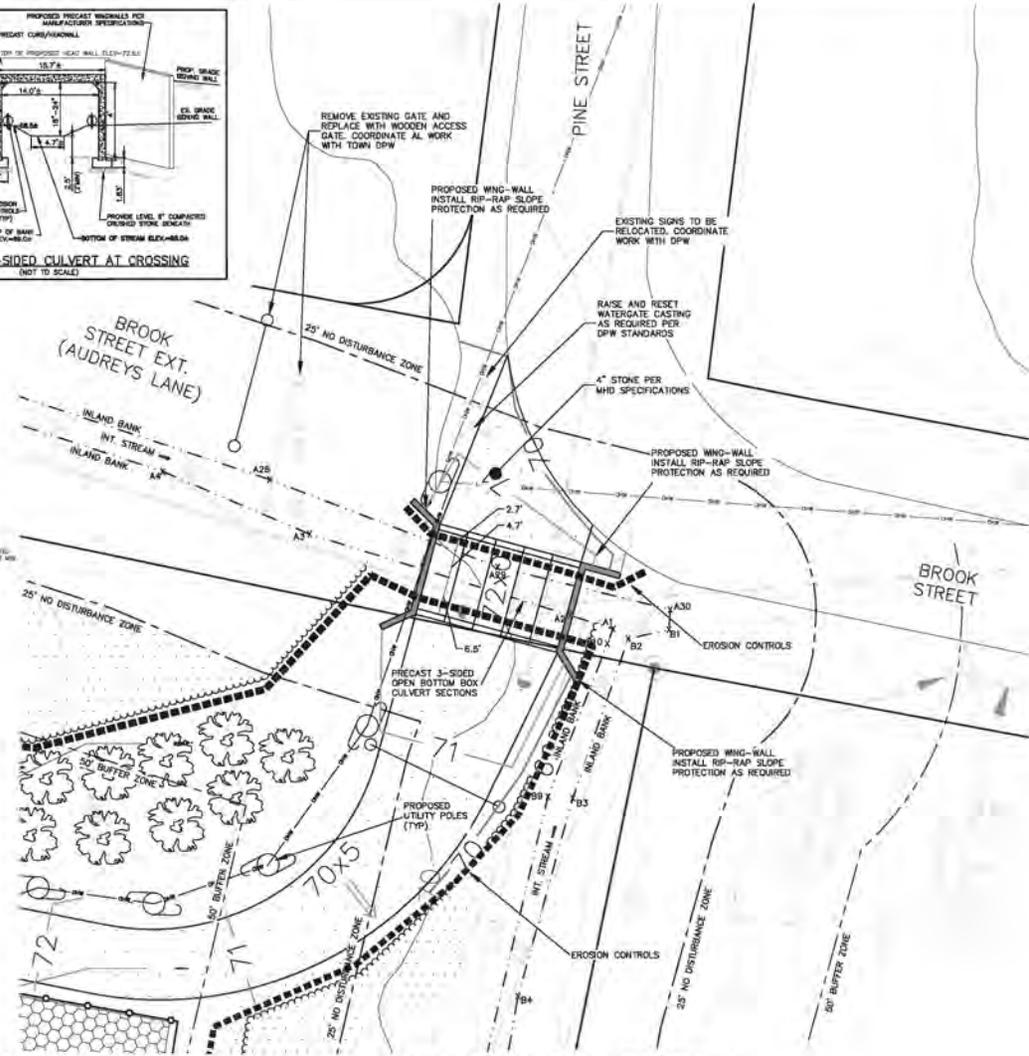
PREPARED FOR:  
 TJA SOLAR  
 150 JOHN VERTENTE BOULEVARD  
 NEW BEDFORD, MASSACHUSETTS 02745

FOR:  
 STREET SOLAR PROJECT  
 DIGHTON, MASSACHUSETTS  
 JULY 16, 2018

Sheet of 5  
 JOB NUMBER 2992.01



PRECAST 3-SIDED CULVERT AT CROSSING (NOT TO SCALE)



PLAN VIEW - PRECAST 3-SIDED CULVERT AT CROSSING (SCALE: 1"=10')

**LANDSCAPE SCREENING PLANT LIST (OUTSIDE OF 100-FOOT BUFFER)**

NUMBER	SPECIES	SIZE	SPACING
20	GREEN GRANT ARBORESCENS	7-8FT	8-10FT O.C.

- NOTES:
- NUMBER AND SIZE ARE APPROXIMATE AND BASED ON ASSUMED SOIL AND REQUIREMENTS OF SCREENING AREA. SPECIFIC NUMBER MAY VARY AND IS CONTINGENT ON THE LOCATION OF NEARBY VISUAL BARRIERS. PLANTING SIZES MAY BE MODIFIED/REMOVED DEPENDENT ON SITE CONDITIONS AS REQUIRED BY MANUAL SCREENING EFFECTIVENESS.
  - SPECIFIC PLACEMENT OF SCREENING PLANTING WILL BE DETERMINED BY A QUALIFIED LANDSCAPE DESIGNER TO MANAGE SCREENING EFFECTIVENESS AND ENSURE SUCCESSFUL ESTABLISHMENT OF PLANTING.
  - THE EFFECTIVENESS OF THE SCREENING INSTALLATION WILL BE EVALUATED DURING THE 100' BUFFER PERIOD BY A QUALIFIED WEED SCIENTIST OR LANDSCAPE DESIGNER. AREAS WHERE ADDITIONAL SCREENING IS REQUIRED WILL BE IDENTIFIED AND SCREENING WILL BE INSTALLED IN THE IDENTIFIED AREAS.

**LANDSCAPE SCREENING PLANT LIST (WITHIN 100-FOOT BUFFER)**

NUMBER	SPECIES	SIZE	SPACING
21	ARBORESCENS	7-8FT	8-10FT O.C.
22	WET PINE	10-15FT	8-10FT O.C.
23	HEAVY OAK	6-8FT	8-10FT O.C.

- NOTES:
- NUMBER AND SIZE ARE APPROXIMATE AND BASED ON ASSUMED SOIL AND REQUIREMENTS OF SCREENING AREA. SPECIFIC NUMBER MAY VARY AND IS CONTINGENT ON THE LOCATION OF NEARBY VISUAL BARRIERS. PLANTING SIZES MAY BE MODIFIED/REMOVED DEPENDENT ON SITE CONDITIONS AS REQUIRED BY MANUAL SCREENING EFFECTIVENESS.
  - SPECIFIC PLACEMENT OF SCREENING PLANTING WILL BE DETERMINED BY A QUALIFIED LANDSCAPE DESIGNER/PROFESSIONAL PERSONNEL IN THE COMPANY'S OFFICE OR AS MANAGED SCREENING.
  - SPECIFIC PLACEMENT OF SCREENING PLANTING WILL BE DETERMINED BY A QUALIFIED LANDSCAPE DESIGNER/PROFESSIONAL PERSONNEL TO MANAGE SCREENING EFFECTIVENESS AND ENSURE SUCCESSFUL ESTABLISHMENT OF PLANTING.
  - THE EFFECTIVENESS OF THE SCREENING INSTALLATION WILL BE EVALUATED DURING THE 100' BUFFER PERIOD BY A QUALIFIED WEED SCIENTIST OR LANDSCAPE DESIGNER. AREAS WHERE ADDITIONAL SCREENING IS REQUIRED WILL BE IDENTIFIED AND SCREENING WILL BE INSTALLED IN THE IDENTIFIED AREAS.
  - SPECIES MAY BE SUBSTITUTED WITH CONSENTATION COMMISSION APPROVAL.

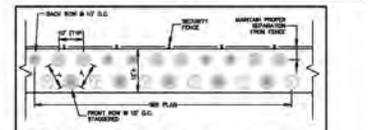
**FOREST ENHANCEMENT AREAS (1,000 SPS)**

NUMBER	SPECIES	SIZE	SPACING
24	WITCH HAZEL	2-3FT	1'-2' O.C.
25	WAXY ARAL	4-5FT	6-20' O.C.
26	RED MAPLE	4-5FT	8-20' O.C.
27	COMMON SWEETSHERRY	6-8FT	6-10' O.C.

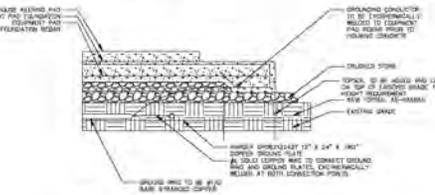
- NOTES:
- SPECIES NUMBER AND SIZE ARE APPROXIMATE AND BASED ON ASSUMED SOIL AND REQUIREMENTS OF SCREENING AREA. SPECIFIC NUMBER MAY VARY AND IS CONTINGENT ON THE LOCATION OF NEARBY VISUAL BARRIERS. PLANTING SIZES MAY BE MODIFIED/REMOVED DEPENDENT ON SITE CONDITIONS AS REQUIRED BY MANUAL SCREENING EFFECTIVENESS.
  - SPECIFIC PLACEMENT OF SCREENING PLANTING WILL BE DETERMINED BY A QUALIFIED LANDSCAPE DESIGNER/PROFESSIONAL PERSONNEL TO MANAGE SCREENING EFFECTIVENESS AND ENSURE SUCCESSFUL ESTABLISHMENT OF PLANTING.
  - THE EFFECTIVENESS OF THE SCREENING INSTALLATION WILL BE EVALUATED DURING THE 100' BUFFER PERIOD BY A QUALIFIED WEED SCIENTIST OR LANDSCAPE DESIGNER. AREAS WHERE ADDITIONAL SCREENING IS REQUIRED WILL BE IDENTIFIED AND SCREENING WILL BE INSTALLED IN THE IDENTIFIED AREAS.



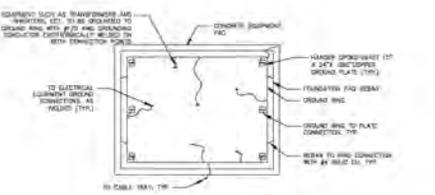
EVERGREEN TREE PLANTING DETAIL (NOT TO SCALE)



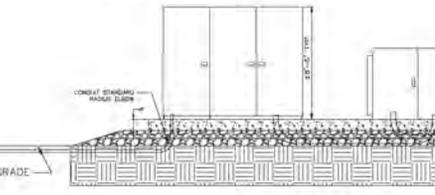
GENERAL PLANTING DETAIL (NOT TO SCALE)



TYPICAL EQUIPMENT PAD DETAIL



TYPICAL EQUIPMENT PAD PLAN VIEW



TYPICAL EQUIPMENT PAD ELEVATION

**Atlantic** DESIGN ENGINEERS, INC.  
 P.O. Box 1051, Sandwich, MA 02563 (508) 888 - 9282

Designed by: \_\_\_\_\_  
 Drawn by: \_\_\_\_\_  
 Checked by: \_\_\_\_\_  
 Surveyed by: \_\_\_\_\_  
 Approved by: \_\_\_\_\_

SCALE  
 AS NOTED



NO.	BY	DATE	REVISION
1	CMK	12-19-18	REVISED W/ ALTERNATIVE ADDRESS
2	CMK	12-5-18	REVISED PER REVIEW COMMENTS
3	BMH	11-19-18	REVISED PER REVIEW COMMENTS

PREPARED FOR:  
**TJA SOLAR**  
 150 JOHN VERTENTE BOULEVARD  
 NEW BEDFORD, MASSACHUSETTS 02745

DETAIL SHEET FOR  
**BROOK STREET SOLAR PROJECT**  
 DIGHTON, MASSACHUSETTS  
 JULY 16, 2018

Sheet of 5 5  
 JOB NUMBER 2992.01



**TOWN OF DIGHTON**  
**PLANNING BOARD**  
**979 SOMERSET AVENUE**  
**DIGHTON, MA 02715**  
**Tel: (508) 669-6431, Ext. 114**  
**Fax: (508) 669-4509**

Timothy Rhines, Chairman  
Robert J. Woods, Vice Chairman  
Joseph Figueiredo, Clerk  
Jeff Carvalho, Member  
Christopher Cunha, Member

**FINDINGS AND DECISION**

RE: MODIFICATION OF A SPECIAL PERMIT & SITE PLAN REVIEW

APPLICANT: GHTJA03, LLC  
d/b/a GRASSHOPPER ENERGY, CORP.  
4 BOBBIE CT  
MANALAPAN, NJ 07726

LOCATION: 0 BROOK STREET  
ASSESSORS MAP 16, LOT 28

DATE:

TOWN CLERK  
BY  
DIGHTON, MA

2022 MAR 17 AM 8:39

RECEIVED

1. On or about September 28, 2021, GHTJA03, LLC (the "Applicant") submitted an application for a modification of a special permit and a site plan review to include the addition of Sungrow BESS Energy Storage System, reconfiguration of the array racking layout, addition of two new utility poles and adjustment of the pole configuration, and as-built modification to the installed box culvert at 0 Brook Street in Dighton, Massachusetts (the "Locus"), identified in the Assessor's records as Map 16, Lot 28. The owner-of-record of the Locus is The Manuel & Louise Andrews Trust.
2. On October 20, 2021, the Planning Board commenced a public hearing on the Application. Said public hearing was continued to November 17, 2021, December 1, 2021, December 15, 2021, January 19, 2022, February 2, 2022, March 2, 2022 and closed on March 2, 2022.
3. The proposal is to allow the installation of seven (7) 19.87'W x 8.00'D x 9.5'H containers on a 32' x 20' crushed stone equipment pad and operation of Sungrow BESS Energy Storage System, a modification of the panel and racking configuration to provide adequate space and clearance for the Sungrow BESS Energy Storage System, a modification of the utility pole configuration for a total of six (6) new utility poles to be installed at the site and a modification to the installed three-sided box culvert in a Residential District in accordance with Section 4600, 5300 and 5400 of the Town of Dighton Zoning Bylaws.
4. Special Permit and Site Plan applications are accompanied by and augmented by Site Development Plans, entitled Brook Street Solar Commercial Photovoltaic System, 0 Brook Street Dighton, Massachusetts ("Plans"), dated January 29, 2021

and revised on September 28, 2021, prepared by Level Design Group, 249 South Street, Unit 1, Plainville, MA 02762.

## FINDINGS

### General

The Applicant proposes to modify the original Special Permit and Site Plan approved on January 16, 2019 to install seven (7) 19.87'W x 8.00'D x 9.5'H containers on a 32' x 20' crushed stone equipment pad and operate Sungrow BESS Energy Storage System, modify the panel and racking configuration to provide adequate space and clearance for the Sungrow BESS Energy Storage System, modify the utility pole configuration for a total of six (6) new utility poles to be installed at the site and modify the installed three-sided box culvert in a Residential District in accordance with Section 4600, 5300 and 5400 where the Ground Mounted Solar Photovoltaic Installation Array is located in a Residential District, a Special Permit is required, in addition to Site Plan Review.

### Special Permit Criteria

The determination of the Planning Board shall include consideration of each of the following:

1. Social, economic or community needs which are served by the proposal;
2. Traffic flow and safety, including parking and loading;
3. Adequacy of utilities and other public services;
4. Neighborhood character and social structures;
5. Impacts on the natural environment; and
6. Potential fiscal impact, including impact on town services, tax base, and employment.

Specifically, as to the Special Permit request, the Board found as follows:

1. The project will have a positive impact on the general social, economic and community needs by providing a renewable energy source in town with added economic benefits to both the property owner and other employed by the work of the installation. Generally, an overall community benefit is realized with the addition of renewable energy sources.
2. There will be no adverse effect to the community or neighborhood from increased traffic flow or safety. Any such impact will be negligible over the long run.
3. There are adequate utilities and other public services.
4. There will be no impact to the neighborhood character and social structures. Indeed, the location of the facility will have little to no impact.
5. The installation will not have any meaningful negative impacts on the natural environment. However, the result of the use of the solar facility will have far reaching positive impacts; and

6. The Town will receive increased personal property tax revenue and there will be positive fiscal impacts to the tax base, and employment.

The Applicant meets the criteria of the Special Permit as set forth above, provided that the Applicant comply with the conditions hereof.

### **DECISION**

The Planning Board, at its meeting of March 2, 2022, voted to Approve the Modification to the Special Permit and Site Plan for the solar facility as shown on the Plans.

In view of the foregoing, the Planning Board hereby decides that the aforesaid proposed modification proposed, as set forth on the Plans, in a manner consistent with the requirements of Section 4600, 5300 and 5400 of the Town of Dighton Zoning Bylaws in that it meets all requisite criteria. It is therefore further determined, that subject to satisfaction of the conditions as set forth below that any perceived adverse effects of the proposed use will not outweigh its beneficial impacts to the Town of the neighborhood, in view of the particular characteristics of the site and of the proposal. Therefore, the Planning Board hereby grants a modification to the Special Permit and a Site Plan to include the addition of a Sungrows BESS Energy Storage System, reconfiguration of the array racking layout, addition of two new utility poles and adjustment of the pole configuration, and as-built modification to the installed box culvert in a Residential District subject to the Conditions:

### **CONDITIONS**

1. The Applicant shall obtain approval of the revised panel and racking configuration extending into a portion of Stormwater Basin 1A from the Stormwater Committee prior to the issuance of Grid Interconnection.
2. The Applicant shall obtain approval of the Sungrow BESS Energy Storage System from the Stormwater Committee prior to the issuance of Certificate of Completion.
3. The Applicant shall supply the Fire Department access to municipal maintained public water supply within 800 feet of the center point of the Sungrow BESS Energy Storage System modules, but at no time should be located any closer than 100 feet from nearest Sungrow BESS Energy Storage System. Adequate water supply shall be determined by the applicable public water supplier and the Dighton Fire Chief.
4. The Applicant shall provide the following setbacks in order to secure public safety concerns from the Sungrow BESS Energy Storage System:
  - a. No less than 200 feet from any property line
  - b. No less than 100 feet from the tree line/vegetative buffer

5. The Applicant shall adhere to the following relative to Hazardous Materials:
- a. Before work begins on the Sungrow BESS Energy Storage System, the Applicant/Owner will advise the Planning Board, Building Commissioner and Dighton Fire Chief in writing of all toxic substances used in relation to the Sungrow BESS Energy Storage System. The Sungrow BESS Energy Storage System must include secondary containment and other safety features satisfactory to the Planning Board, Building Commissioner and Dighton Fire Chief, who whereby are authorized to approve (or deny) administratively the design of the Sungrow BESS Energy Storage System, such approval shall not to be unreasonably denied if the Sungrow BESS Energy Storage System conforms to industry best practices, including without limitation applicable National Fire Protection Association standards, for ensuring safety of the public and the environment. The Planning Board may retain the services of a consultant to aid in such review, with the costs thereof to be borne by the Applicant/Owner in accordance with MGL Ch. 44, Sec. 53G. Said features must be adequate to prevent the release of any toxic substances from the Sungrow BESS Energy Storage System from any cause, including without limitation fire or explosion, to the extent that such release would, or could reasonably be expected to, adversely affect the health, property, drinking water, or inhalable air of any person or property surrounding the site of the Solar or Sungrow BESS Energy Storage System. The height of the Sungrow BESS Energy Storage System unit should not exceed ten-feet (10') in height above the surrounding grade level. The plans for the Sungrow BESS Energy Storage System shall be presented and approved prior to the commencement of any site work to verify compliance with this condition.
  - b. In order to protect water supplies and preserve public safety associated Sungrow BESS Energy Storage System should not be located in the Zone 1 of any public water supply and should be located above the 100-year flood plain. The Sungrow BESS Energy Storage System must be located within a structure with the following features: an acid resistant membrane floor for potential leaks of hazardous materials; a temperature and humidity-maintained environment; a smoke/fire detection system, UL approved monitoring system, fire alarm fire suppression system, a thermal runaway system, and a local disconnect point or emergency shutdown feature.

The building and systems must be approved by the Dighton Fire Chief and must be designed and installed in accordance with all applicable State codes and safety requirements, as well as, safety measures recommended by the National Fire Protection Association. Applicant/Owner will provide specialized emergency response funding for training of Dighton Fire Department staff prior to grid inter connection. Periodic inspections

to ensure the integrity of the batteries, other equipment, and the containment systems, be required as conditions of the special permit and the site plan review.

Sungrow BESS Energy Storage System must number only those needed to support the solar installation at the site. Spent, expired or damaged Battery Energy Storage System must be immediately removed from the site.

6. The Applicant shall submit an Emergency Response Plan for the Sungrow BESS Energy Storage System. Specialized emergency response personnel will be retained or employed for technical assistance by the Applicant/Owner to respond to certain kinds of incidents, including but not limited to, electrical and chemical fires, as well as, include remote monitoring systems which alert the facility owner and local emergency personnel to any problems or unusual conditions occurring on-site. The Applicant/Owner will cooperate with local emergency services to develop an Emergency Response Plan for the construction period and operations period. Such Plan must be approved by the Dighton Fire Chief prior to the commencement of work on the Property.
7. The Applicant shall submit a Battery Energy Storage System Operation & Maintenance Plan for the Sungrow BESS Energy Storage System. The Applicant shall submit a complete Operation and Maintenance Plan, including but not limited to, inspection schedules, warranties for all monitoring and protection equipment, warranties, service life and operational life, to the Planning Board and Dighton Fire Chief prior to the commencement of construction.
8. The Applicant shall submit Annual Reporting which certifies compliance with the requirements of this bylaw, the Sungrow BESS Energy Storage System, and the approved site plan including control of vegetation, noise standards, and adequacy of road access. The Annual Report shall also provide information on the maintenance completed during the course of the year and the amount of electricity generated and stored by the facility. The Annual Report shall be submitted to the Board of Selectmen, Planning Board, Dighton Fire Chief, Emergency Management Director, Building Commissioner, Board of Health, Stormwater Committee and the Conservation Commission no later than 45 days after the end of each calendar year.
9. The Applicant shall provide a form of surety for the Sungrow BESS Energy Storage System, either through a cash deposit, passbook agreement, lender's agreement, bond or other form of surety approved by the Planning Board to cover the cost of removal in the event the Town must remove the installation and remediate the landscape, said surety to be secured by an agreement in an amount and form determined to be reasonable by the Planning Board. The Applicant shall submit a fully inclusive estimate of the costs associated with removal, prepared by

a qualified engineer, said amount to be subject to peer review. The amount shall include contingency as well as a mechanism for calculating increased removal costs due to inflation.

**DIGHTON PLANNING BOARD**

Timothy F. Rhines  
Timothy Rhines, Chairman

R. Woods  
Robert J. Woods, Vice Chairman

Joseph Figueiredo  
Joseph Figueiredo, Clerk

Jeff Carvalho  
Jeff Carvalho, Member

Christopher Cunha  
Christopher Cunha, Member

The following members of the Planning Board are in opposition to the grant of the special permit:

\_\_\_\_\_  
\_\_\_\_\_

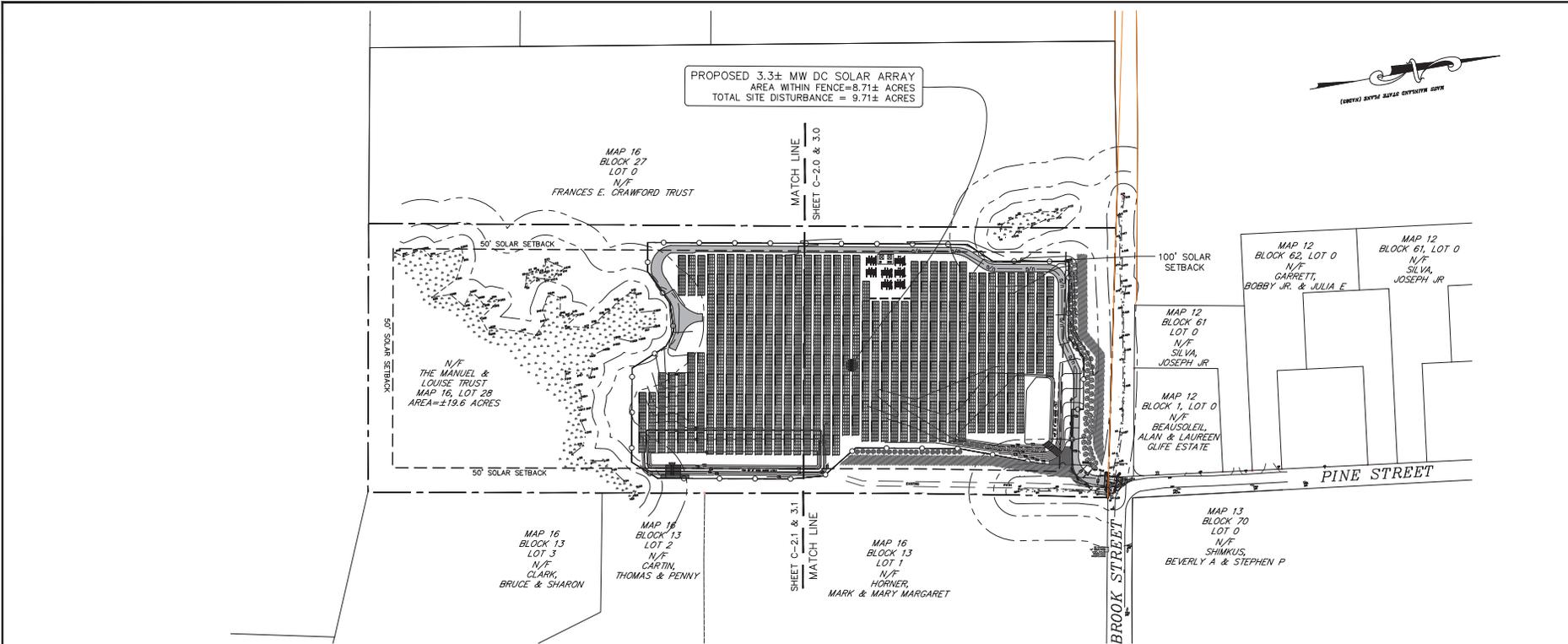
Filed with the Town Clerk on \_\_\_\_\_, 20\_\_.

\_\_\_\_\_  
Mark Pacheco, Town Clerk

TOWN CLERK  
DIGHTON, MA  
BY MP

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2022 MAR 17 AM 8:39





PROPOSED 3.3± MW DC SOLAR ARRAY  
 AREA WITHIN FENCE=8.71± ACRES  
 TOTAL SITE DISTURBANCE = 9.71± ACRES

**REFERENCE NOTES:**

- EXISTING SITE CONDITIONS WERE OBTAINED FROM THE APPROVED PROJECT PLAN SET ENTITLED "SITE DEVELOPMENT PLANS FOR BROOK STREET SOLAR PROJECT DIGHTON, MASSACHUSETTS", DATED JULY 16, 2018 AND REVISED THROUGH DECEMBER 19, 2018. PREPARED BY ATLANTIC DESIGN ENGINEERS, INC.
- ON-SITE WETLANDS RESOURCE AREA DELINEATION BY GODDARD CONSULTING, INC. IN JUNE, 2018. ADDITIONAL DELINEATION WAS PERFORMED IN OCTOBER, 2018. RESOURCE AREA DELINEATION FLAGS WERE FIELD LOCATED BY ATLANTIC DESIGN ENGINEERS, INC. IN JUNE, 2018 AND ADDITIONALLY IN OCTOBER, 2018.
- THIS CONSTRUCTION PLAN SET IS BASED ON THE APPROVE PROJECT SITE PLAN SET ENTITLED "SITE DEVELOPMENT PLANS FOR BROOK STREET SOLAR PROJECT DIGHTON, MASSACHUSETTS", DATED JULY 16, 2018 AND REVISED THROUGH DECEMBER 19, 2018. PREPARED BY ATLANTIC DESIGN ENGINEER, INC. AS APPROVED BY THE TOWN OF DIGHTON PLANNING BOARD FOR SPECIAL PERMIT DATED JANUARY 17, 2018 AND IN ACCORDANCE WITH AN ORDER OF CONDITIONS (MADEP FILE # 017-0401 ISSUED BY THE TOWN OF DIGHTON CONSERVATION COMMISSION ISSUED DECEMBER 19, 2018.
- LEVEL DESIGN GROUP, LLC HAS MADE NO CHANGES TO APPROVED SITE DRAINAGE, CLEARING LIMITS, EROSION CONTROLS AND CONSTRUCTION REQUIREMENTS AS DETAILED IN THE APPROVED SITE PLAN. CHANGES TO THE ABOVE REFERENCE SITE PLAN INCLUDE FINAL STING AND ORIENTATION OF THE PROPOSED SOLAR PANEL RACKING AND PLACEMENT REQUIRED GROUND EQUIPMENT AND BATTERY STORAGE PADS BASED ON FINAL ELECTRICAL DESIGN REQUIREMENTS OF THE PROPOSED GROUND MOUNTED SOLAR ARRAY.
- THE HORIZONTAL DATUM OF THIS PLAN SET IS BASED ON MASS GRID SYSTEM, NAD83, ELEVATIONS ON THIS PLAN REFER TO NAVD83.

**GENERAL NOTES:**

- THE LOCATION OF EXISTING UTILITIES IS APPROXIMATE. THE CONTRACTOR SHALL VERIFY THE LOCATION OF ALL UTILITIES IN THE FIELD PRIOR TO THE START OF CONSTRUCTION. NOTIFY "DIG-SAFE" AT 1-888-344-7233 AT LEAST 72 HOURS PRIOR TO ANY SITE DEMOLITION OR EXCAVATION.
- CONTRACTOR SHALL NOTIFY ENGINEER OF ANY DISCREPANCIES IN THE DESIGN PLANS PRIOR TO THE START OF CONSTRUCTION AND SHALL VERIFY EXISTING GROUND ELEVATIONS THROUGHOUT THE SITE AND IN THE AREA OF PROPOSED STORMWATER MANAGEMENT SITE FEATURES TO ENSURE PROPER WORKING CONDITION OF THE INSTALLED STORMWATER MANAGEMENT SYSTEM AS RELATED TO SURROUNDING SITE GRADES.
- CONTRACTOR IS REQUIRED TO MANAGE STORMWATER RUNOFF DURING THE CONSTRUCTION PROCESS IN ACCORDANCE WITH THE EROSION CONTROL NOTES AND PROCEDURES DETAILED WITHIN THIS SITE PLAN AND THE CORRESPONDING STORMWATER POLLUTION PREVENTION PLAN. ALL COSTS ASSOCIATED WITH REPAIRS AND CORRECTIVE ACTIONS REQUIRED TO PROPERLY MANAGE STORMWATER RUNOFF SHALL BE THE RESPONSIBILITY OF THE SITE CONTRACTOR.
- ALL EXISTING PAVEMENT SHALL BE SAWCUT PRIOR TO REMOVAL.
- ALL EXISTING PAVEMENT, CURB, WALKS, UTILITIES, LIGHT POLES, TREES, SHRUBS, ETC., SHALL BE REMOVED FROM THE AREAS TO BE DEVELOPED. ALL SUCH ITEMS NOT WITHIN THE WORK AREA SHALL BE PROTECTED AND UNDISTURBED.
- ALL DISTURBED AREAS NOT RECEIVING IMPROVEMENTS SHALL BE LOAMED AND SEEDED.
- ALL CONSTRUCTION AND CONSTRUCTION ACTIVITIES SHALL CONFORM TO STATE AND LOCAL REQUIREMENTS AND ALL PROJECT PERMITS ISSUED, INCLUDING BUT NOT LIMITED TO THE TOWN OF DIGHTON, THE COMMONWEALTH OF MASSACHUSETTS AND ANY OTHER AGENCIES HAVING JURISDICTION.
- THE LOCATION AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE AND UTILITY OWNED ELECTRIC SERVICES SHALL BE INSTALLED ACCORDANCE WITH CURRENT UTILITY COMPANY REQUIREMENT.
- SUBSURFACE AND ENVIRONMENTAL CONDITIONS WERE NOT EXAMINED OR CONSIDERED AS PART OF THIS SURVEY. NO STATEMENT IS MADE CONCERNING THE EXISTENCE OF UNDERGROUND CONTAINERS OR FACILITIES THAT MAY AFFECT THE USE OR DEVELOPMENT OF THE SITE.
- CONTRACTOR IS RESPONSIBLE TO ENSURE THAT ALL REQUIRED INSPECTIONS AND/OR CERTIFICATIONS REQUIRED BY CODES AND/OR UTILITY COMPANIES ARE COMPLETED PRIOR TO THE INSTALLATION, BACKFILLING, AND FINAL CONNECTION OF THE SERVICES.
- CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ALL SURVEY CONTROL POINTS AND BENCHMARKS NECESSARY FOR THE PROPOSED WORK.
- CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ADEQUATE RECORDS OF THE LOCATIONS AND ELEVATION OF ALL STRUCTURES INSTALLED AND/OR WORK COMPLETED.

**CONSTRUCTION NOTES:**

- ALL DAILY VEHICLE PARKING SHALL OCCUR WITHIN THE LIMIT OF SITE CLEARING AND WITHIN EROSION CONTROL BARRIERS. NO ADDITIONAL SOIL DISTURBANCE OR SITE CLEARING SHALL OCCUR TO ACCOMMODATE DAILY PARKING. NO PARKING OF PERSONAL VEHICLES BY DAILY WORKFORCE SHALL OCCUR ALONG THE PUBLIC ROAD RIGHT OF WAY OR SHARED RESIDENTIAL SEGMENT OF THE ACCESS DRIVE.
- SOLAR ARRAY DEVELOPMENT AREA WITHIN SECURITY FENCE:
  - ALL TREES AND SHRUBS TO BE CLEARED AND STUMPS TO BE REMOVED
  - ANY RE-GRADING TO BE MINIMAL AS FOLLOWS:
    - EXISTING GRASSY VEGETATION WITHIN AREA OF CONSTRUCTION TO REMAIN DURING SOLAR ARRAY INSTALLATION.
    - AREA TO BE SCARIFIED AND SEEDED AFTER MAJOR SITE WORK IS COMPLETE.
- MAINTENANCE AND PEDESTRIAN CORRIDOR:
  - AREA AROUND SECURITY FENCE-- WIDTH VARIES
  - ALL TREES AND SHRUBS TO BE CLEARED AND STUMPS REMOVED
  - ANY RE-GRADING TO ADHERE TO NOTE 1A
- SHADE MANAGEMENT:
  - SHADE MANAGEMENT SHALL BE ALLOWED ONLY WITHIN THE DEFINED AREAS DETAILED ON THE SITE PLAN. ADDITIONAL PERIMETER EROSION CONTROLS WILL BE INSTALLED WHERE WORK WITHIN THE SHADE MANAGEMENT FALLS OUTSIDE OF THE EROSION CONTROL LINE DETAILED ON THE SITE PLANS.
- THE CONTRACTOR SHALL NOTIFY THE PLANNING BOARD OR ITS DESIGNATED AGENT AND THE DESIGN ENGINEER AND REQUEST AND INSPECTION AT LEAST TWO WORKING DAYS BEFORE EACH OF THE FOLLOWING EVENT:
  - EROSION AND SEDIMENT CONTROL MEASURES ARE IN PLACE AND STABILIZED;
  - SITE CLEARING HAS BEEN SUBSTANTIALLY COMPLETED;
  - ROUGH GRADING HAS BEEN SUBSTANTIALLY COMPLETED;
  - FINAL GRADING BEEN HAS SUBSTANTIALLY COMPLETED;
  - CLOSE OF THE CONSTRUCTION SEASON;
  - FINAL LANDSCAPING (PERMANENT STABILIZATION) AND PROJECT FINAL COMPLETION.

**ZONING REQUIREMENTS:**

ZONING DISTRICT: RESIDENCE & AGRICULTURAL (RA)  
 OVERLAY DISTRICT: GROUNDWATER PROTECTION OVERLAY

**REQUIREMENT**

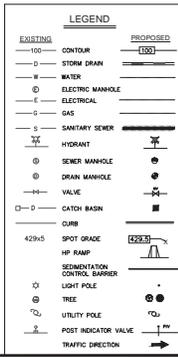
*MINIMUM LOT AREA	35,000 SQUARE FEET
*FRONTAGE	175 FEET
*MINIMUM FRONT YARD	55 FEET
*MINIMUM SIDE YARD	15 FEET
*MINIMUM REAR YARD	15 FEET

\*NOTE: PROPERTY LINE SETBACK FOR GROUND-MOUNTED SOLAR FACILITIES AS REQUIRED BY THE TOWN OF DIGHTON ZONING BYLAW SECTION 4600-4680 LARGE SCALE GROUND MOUNTED SOLAR PHOTOVOLTAIC INSTALLATIONS:

MINIMUM LOT SIZE	8 ACRES
MINIMUM FRONT YARD	100 FEET
MINIMUM SIDE YARD	50 FEET
MINIMUM REAR YARD	50 FEET

**PROPERTY / PROJECT INFORMATION:**

SUBJECT PARCEL AREA = 19.6 ACRES AND IS IDENTIFIED AS LOT 28, MAP 16 BY CURRENT TOWN OFFICE OF DIGHTON ASSESSOR RECORDS  
 OWNER OF RECORD: THE MANUAL & LOUISE ANDREWS TRUST, 12 CYPRESS DRIVE, DARTMOUTH, MASSACHUSETTS 02747  
 PROPERTY DEED REFERENCE: DEED BOOK 1247, PAGE 113  
 DEVELOPER / APPLICANT: GHJIAQ3, 1209 ORANGE STREET, WILMINGTON, DELAWARE 19801  
 THE SITE IS LOCATED WITH ZONE X FLOOD PLAN, AN AREA DETERMINED TO BE OUTSIDE OF THE 0.2% ANNUAL CHANCE OF FLOODING BASED ON A REVIEW OF FEMA FLOOD INSURANCE RATE MAP NUMBER 25050C0234G EFFECTIVE DATE, JULY 13, 2018.  
 BASED ON A REVIEW OF CURRENT MASSACHUSETTS GEOGRAPHIC INFORMATION SYSTEM (MASS GIS) INFORMATION THE SITE IS NOT LOCATED WITHIN A ZONE II AQUIFER PROTECTION DISTRICT, AN AREA OF CRITICAL ENVIRONMENTAL CONCERN (ACEC) OR WITHIN A PRIORITY OR ESTIMATED HABITAT OF ANY RARE OR ENDANGERED SPECIES.



NO.	DATE	REVISIONS
1.	01/26/2021	ISSUE FOR CONSTRUCTION
2.	03/08/2021	PERMITS PERMITS MODIFIED

SEAL

DATE: AUGUST 31, 2020  
 DRAWN: NP/ERIC  
 SCALE: 1" = 100'

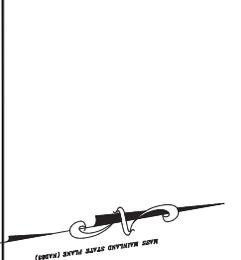
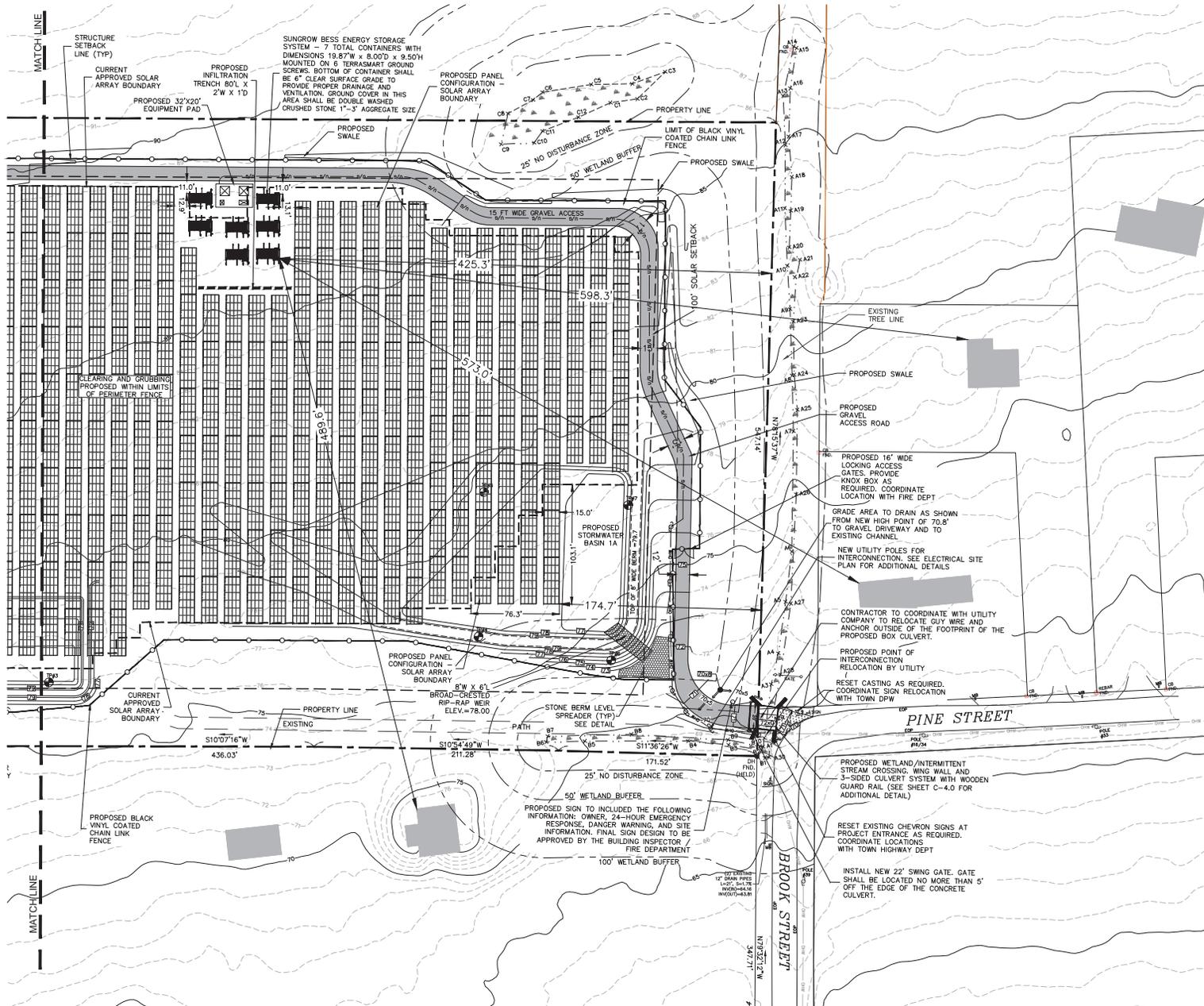
**BROOK STREET SOLAR  
 COMMERCIAL SOLAR FACILITY**  
 ASSESSOR PARCEL - MAP 16; PARCEL 28  
 BROOK STREET  
 DIGHTON, MASSACHUSETTS

**LEVEL**  
 CIVIL ENGINEERING / LAND SURVEYING  
 240 SOUTH STREET  
 PLAINVILLE, MA 02762  
 TEL: (508) 695-2221 FAX: (508) 695-2219

**KEY SHEET  
 & NOTES**

**C-1.0**  
 SHEET 2 OF 10  
 0' 50' 100' 200'  
 1817.00





- PLAN NOTES:**
- SEE SHEETS C-1.0 & 1.1 FOR PLAN LEGEND, REFERENCE NOTES, CONSTRUCTION NOTES, EROSION AND SEDIMENT CONTROL NOTES, AND TOWN OF DIGHTON SITE PLAN / SPECIAL PERMIT APPROVAL CONDITIONS AND ORDER OF CONDITIONS GENERAL AND SPECIAL CONDITIONS.

NO.	DATE	REVISIONS
1	01/26/2021	ISSUE FOR CONSTRUCTION
2	03/26/2021	PERMIT REVISIONS

SEAL: DATE: AUGUST 31, 2020 DRAWN: NP/ERIC SCALE: 1" = 40'

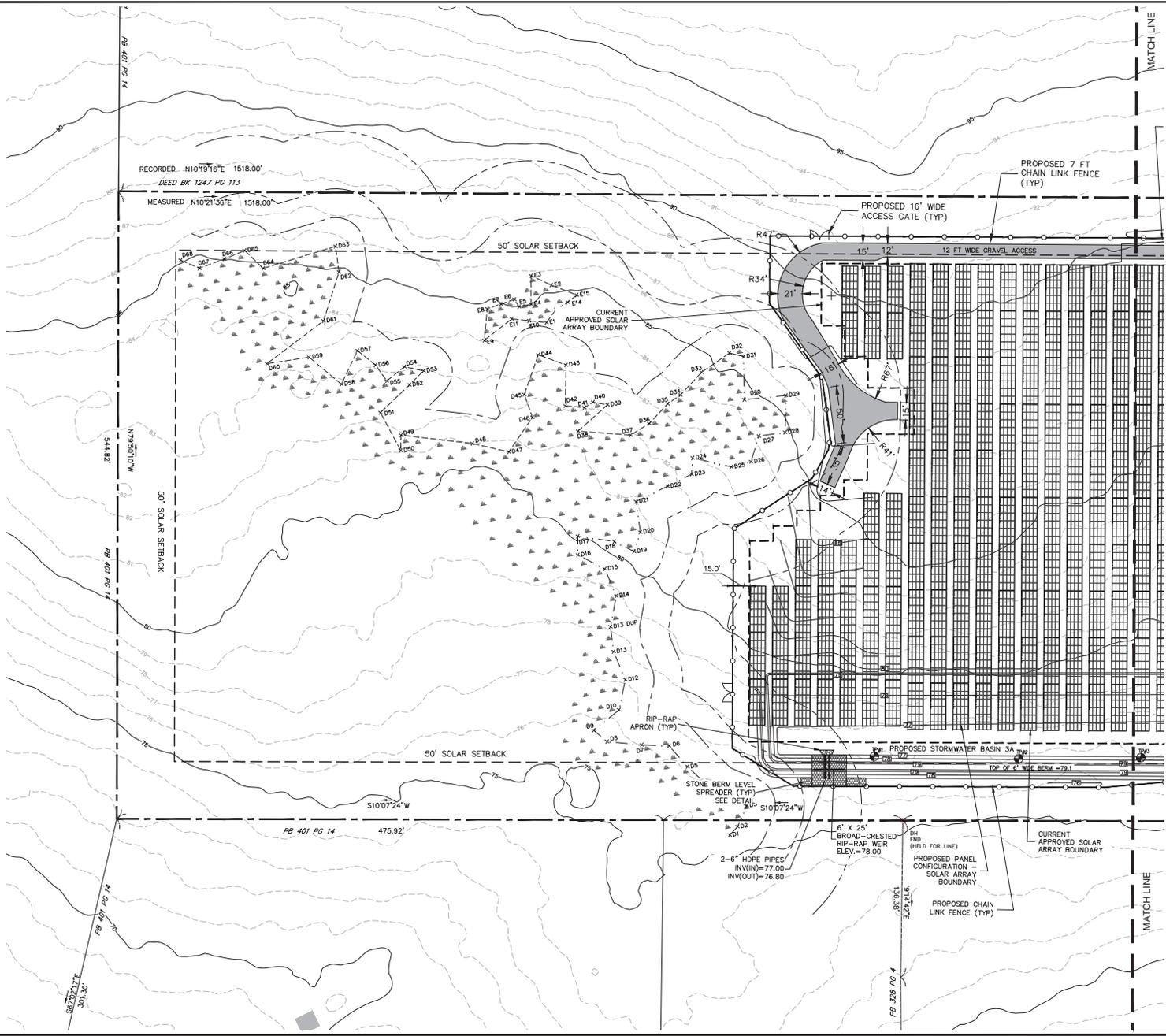
**BROOK STREET SOLAR COMMERCIAL SOLAR FACILITY**  
 ASSESSOR PARCEL - MAP 16; PARCEL 28  
 BROOK STREET  
 DIGHTON, MASSACHUSETTS

**LEVEL**  
 DESIGNER  
 CIVIL ENGINEERING / LAND SURVEYING  
 240 SOUTH STREET  
 SUITE 1  
 PLAINVILLE, MA 02762  
 TEL: (508) 695-2221 FAX: (508) 695-2219

**SITE PLAN**

**C-2.0**  
 SHEET 4 OF 10

0 20 40 80  
 1817.00



**PLAN NOTES:**

1. SEE SHEETS C-1.0 & 1.1 FOR PLAN LEGEND, REFERENCE NOTES, CONSTRUCTION NOTES, EROSION AND SEDIMENT CONTROL NOTES, AND TOWN OF DIGHTON SITE PLAN / SPECIAL PERMIT APPROVAL CONDITIONS AND ORDER OF CONDITIONS GENERAL AND SPECIAL CONDITIONS.

NO.	DATE	REVISIONS
1	01/26/2021	ISSUE FOR CONSTRUCTION
2	03/05/2021	SPECIAL PERMIT SUBMITTAL

SEAL

DATE: AUGUST 31, 2020  
 DRAWN: NP/ERIC  
 SCALE: 1" = 40'

**BROOK STREET SOLAR  
 COMMERCIAL SOLAR FACILITY**  
 ASSESSOR PARCEL - MAP 16; PARCEL 28  
 BROOK STREET  
 DIGHTON, MASSACHUSETTS

**LEVEL**  
 ENGINEERING  
 CIVIL ENGINEERING / LAND SURVEYING  
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 SUITE 1  
 PLAINVILLE, MA 02762  
 TEL: (508) 695-2221 FAX: (508) 695-2219

**SITE  
 PLAN**

**C-2.1**  
 SHEET 5 OF 10

1817.00



**EROSION CONTROL GENERAL NOTES:**

EROSION AND SEDIMENT CONTROL METHODS FOR THE SITE INCLUDE STRUCTURAL AND STABILIZATION PRACTICES. STABILIZATION PRACTICES WILL BE IMPLEMENTED TO COVER EXPOSED SOIL SO THAT DISCHARGE OF SEDIMENT IS MINIMIZED. STABILIZATION PRACTICES REDUCE THE TIME SOIL IS EXPOSED TO THE ELEMENTS THEREFORE REDUCING THE POSSIBILITY OF EROSION. AN ADEQUATE STOCKPILE OF EROSION CONTROL MATERIALS WILL BE MAINTAINED AT THE CONSTRUCTION SITE IN THE EVENT OF AN EMERGENCY OR ROUTINE REPAIRS.

STRUCTURAL PRACTICES INVOLVE THE CONSTRUCTION OF DEVICES TO DIVERT AND LIMIT RUNOFF. THESE PRACTICES LIMIT THE AMOUNT OF STORM WATER ENTERING A DISTURBED AREA OR TRAP SEDIMENT PRIOR TO STORM WATER LEAVING A SITE. THE FOLLOWING ARE THE PROCEDURES TO BE FOLLOWED:

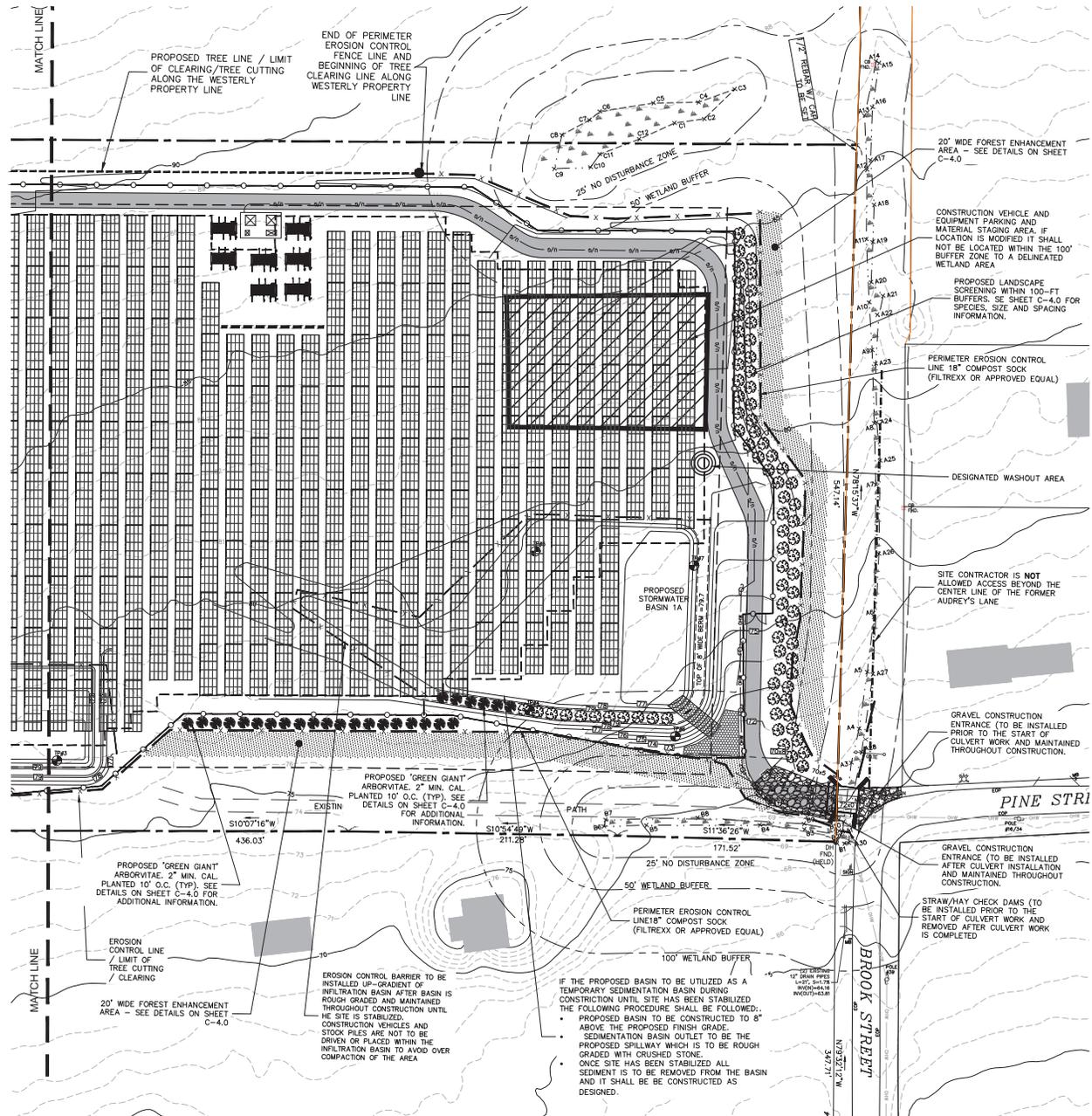
1. THE SITE CONSTRUCTION FOREMAN SHALL BE DESIGNATED AS THE ON-SITE INDIVIDUAL WHO WILL BE RESPONSIBLE FOR THE DAILY MAINTENANCE OF ALL SEDIMENT AND EROSION CONTROLS, AND SHALL IMPLEMENT ALL MEASURES NECESSARY TO CONTROL EROSION AND TO PREVENT SEDIMENT FROM LEAVING THE SITE.
2. PRIOR TO ANY SITE GRADING OR SITE WORK, THE CONTRACTOR SHALL INSTALL ALL SPECIFIED SEDIMENT AND EROSION CONTROLS, WHICH WILL ALSO SERVE AS THE LIMIT OF CONSTRUCTION. THE SEDIMENT CONTROLS WILL BE AS SPECIFIED ON THE APPROVED PLANS.
3. ANY WORK UP TO 100' OF WETLAND RESOURCE AREA (NOT DETAILED IN THE SITE PLAN) IS TO HAVE A SECONDARY ROW OF SILT/STOCK & EROSION CONTROL BARRIERS. EROSION CONTROL TYPE AS SHOWN ON THE PLANS TO BE FIELD VERIFIED BASED ON CONSTRUCTION TIMING, PHASING AND SITE CONDITIONS.
4. A CONSTRUCTION VEHICLE SHALL BE CONSTRUCTED TO SHED DIRT FROM CONSTRUCTION VEHICLE TIRES. THE CRUSHED STONE PAD WILL BE REPLACED/CLEANED AS NEEDED TO MAINTAIN ITS EFFECTIVENESS.
5. CONSTRUCTION DEBRIS AND SEDIMENT SHALL BE KEPT ON SITE AND SHALL NOT BE PERMITTED TO MIGRATE BEYOND THE PROJECT BOUNDARIES.
6. ONCE THE SITE IS STABLE, THE SEDIMENT AND EROSION CONTROLS MAY BE REMOVED UNDER THE DIRECTION OF THE EROSION CONTROL SPECIALIST.

**SITE CONTROLS**

THE FOLLOWING ADDITIONAL CONTROLS SHALL BE IMPLEMENTED DURING CONSTRUCTION IN ORDER TO MINIMIZE EROSION AND RUNOFF FROM THE PROJECT LOCATION:

1. CONTRACTOR SHALL TAKE APPROPRIATE MEASURES TO CONTROL DUST ON PROJECT SITE, INCLUDING BUT NOT LIMITED TO THE ADDITION OF DRY CALCIUM ON THE ACCESS ROAD TOWARDS ENTRANCE AT Brook ROAD.
2. CONTRACTOR SHALL TAKE APPROPRIATE MEASURES TO KEEP Dighton ROAD CLEAR OF MUD, EXCESS GRAVEL, AND OTHER CONSTRUCTION DEBRIS.
3. NO CHEMICALS (CEMENT, MORTAR, ETC.) SHALL BE MIXED OR POURED WITHIN ANY WETLANDS OR BUFFER ZONE.
4. SOLID WASTE WILL BE COLLECTED AND STORED IN A SECURE DUMPSTER. THE DUMPSTER SHALL MEET ALL LOCAL AND STATE SOLID WASTE MANAGEMENT REGULATIONS.
5. CONSTRUCTION DEBRIS MAY INCLUDE LUMBER, CONCRETE, STEEL, OR OTHER DEBRIS AND SITE MATERIALS REQUIRING REMOVAL. THESE MATERIALS WILL BE DISPOSED OF ACCORDING TO STATE AND FEDERAL LAW AND WILL NOT BE DISPOSED OF ON SITE. EXCESS SOIL GENERATED FROM THIS SITE REQUIRES CHARACTERIZATION PRIOR TO REMOVAL. RATHER THAN EXPORT MATERIAL, IT IS PREFERRED THAT MINOR EXCAVATIONS ARE REUSED ON SITE AS BACKFILL IN THE SAME GENERAL AREA IT ORIGINATED.
6. THE LIMITS OF ALL GRADING AND DISTURBANCE SHALL BE KEPT TO A MINIMUM WITHIN THE PROPOSED AREA OF CONSTRUCTION. ALL AREAS OUTSIDE THE LIMITS OF DISTURBANCE SHALL REMAIN UNDISTURBED.
7. CONTINUOUS LINES OF EROSION CONTROLS SHALL ENCLOSE THE DOWNSTREAM SIDES OF THE WORK AREA, THESE COMBINED WITH UP-SLOPE MARKERS (CONS. FENCE AND/OR FLAGGING) WILL SERVE AS THE LIMIT OF WORK.
8. ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE MAINTAINED OR REPLACED AS REQUIRED BY THE SITE CONTRACTOR TO ASSURE PROPER FUNCTION.
9. ALL BREACHES OR FAILURES IN SEDIMENT CONTROLS SHALL BE IMMEDIATELY REPAIRED OR REPLACED BY THE SITE CONTRACTOR.
10. DEBRIS AND LITTER, WHICH ACCUMULATES ALONG THE CONSTRUCTION AREA, SHALL BE REMOVED DAILY.
11. SEDIMENT BUILD-UP BEHIND ANY SILT FENCES OR EROSION CONTROL BARRIERS WILL BE MONITORED AND REMOVED WHENEVER SEDIMENT HAS ACCUMULATED TO 3-INCHES IN DEPTH.
12. OTHER CONTROLS WILL BE IMPLEMENTED, AS DEEMED NECESSARY BY THE CONTRACTOR, DURING THE CONSTRUCTION OF THE PROJECT.
13. IF CONDITIONS WARRANT, ADDITIONAL DE-WATERING CONTROLS MAY BE NEEDED SUCH AS DIRT BAGS, FRAC TANKS OR OTHER MEASURES.
14. STORMWATER INFILTRATION BASINS ARE NOT TO BE UTILIZED AS TEMPORARY SEDIMENT BASINS, IF TEMPORARY SEDIMENT BASINS AREA REQUIRED, THEY SHALL BE DESIGN AND SITED BY THE SITE ENGINEER.
15. THE LOCATION OF ALL STORMWATER INFILTRATION BASINS SHALL BE FIELD STAKED AFTER SITE CLEARING ACTIVITIES HAVE BEEN COMPLETED. INFILTRATION AREAS SHALL BE PROTECTED THROUGHOUT CONSTRUCTION TO AVOID EXCESSIVE COMPACTION OF THESE AREAS. ONCE THE BASINS HAVE BEEN GRADED PERIMETER EROSION CONTROLS IN THE FORM OF SILT/STOCK AND STAKED EROSION CONTROL FENCING SHALL BE INSTALLED ALONG THE UP-GRADE SIDE TO PREVENT UNCHECKED SURFACE RUNOFF FROM ENTERING THE BASIN AREA AND SHALL BE MAINTAINED UNTIL FINAL SITE STABILIZATION. ANY ACCUMULATED SEDIMENT WHICH ENTERS THE INFILTRATION BASIN PRIOR TO FINAL SITE STABILIZATION SHALL BE REMOVED TO A DEPTH OF 6" BELOW THE ACCUMULATED SEDIMENT AND THE BOTTOM OF THE BASIN BE FILLED WITH CLEAN SAND TO 6" BELOW FINISH GRADED WHERE 6" OF LOAM AND SEED SHALL BE INSTALLED.

EROSION CONTROL NOTES CONTINUED ON SHEET C-3.1



NO.	DATE	REVISIONS
1	01/26/2021	ISSUE FOR CONSTRUCTION
2	08/26/2021	PERMITS PERMIT NUMBER 21-01

DATE	SCALE
AUGUST 21, 2020	1" = 40'



DATE: AUGUST 21, 2020  
 DRAWN: NP/ERIC  
 SCALE: 1" = 40'

**BROOK STREET SOLAR COMMERCIAL SOLAR FACILITY**  
 ASSESSOR PARCEL - MAP 16; PARCEL 28  
 BROOK STREET  
 DIGHTON, MASSACHUSETTS



**EROSION CONTROL**

**C-3.0**

SHEET 6 OF 10

**1817.00**

THE TEMPORARY SEEDING DESIGN MIX SHALL BE COMPRISED OF THE FOLLOWING:

ANNUAL RYE GRASS	40
PERENNIAL RYE GRASS	60

**STORMWATER INLET PROTECTION**

... WILL BE UTILIZED TO PREVENT SOIL AND DEBRIS FROM ENTERING STORM DRAIN INLETS. THESE MEASURES ARE USUALLY TEMPORARY AND ARE IMPLEMENTED BEFORE A SITE IS DISTURBED.

**MAINTENANCE** - THE OPERATOR MUST CLEAN, OR REMOVE AND REPLACE THE INLET PROTECTION MEASURES AS SEDIMENT ACCUMULATES, THE FILTER BECOMES CLOGGED, AND/OR AS PERFORMANCE IS COMPROMISED. ACCUMULATED SEDIMENT ADJACENT TO THE INLET PROTECTION MEASURES SHOULD BE REMOVED BY THE END OF THE SAME WORK DAY IN WHICH IT IS FOUND OR BY THE END OF THE FOLLOWING WORK DAY IF REMOVAL BY THE SAME WORK DAY IS NOT FEASIBLE.

**STORMWATER BASINS** - ALL AREAS CONTAINING STORMWATER BASINS (ABOVE OR BELOW GROUND) SHALL BE PROTECTED THROUGHOUT CONSTRUCTION. THESE AREAS ARE NOT TO BE USED FOR MATERIAL STOCKPILES OR FOR PARKING EQUIPMENT. SURFACE BASINS ARE TO BE ROUGH GRADED AND PROTECTED UNTIL STABILIZED AND BROUGHT ON-LINE FOR STORMWATER MANAGEMENT OF THE STABILIZED SITE.

**CONSTRUCTION ENTRANCES**

CONSTRUCTION ENTRANCES SHALL BE USED IN CONJUNCTION WITH THE STABILIZATION OF CONSTRUCTION ROADS TO REDUCE THE AMOUNT OF SEDIMENT TRACKING OFF OF THE PROJECT. ANY CONSTRUCTION SITE ACCESS POINT MUST EMPLOY THE CONTROL MEASURES ON THE APPROVED SITE PLANS AND IN ACCORDANCE WITH THE STORMWATER POLLUTION PREVENTION PLAN. CONSTRUCTION ENTRANCES SHALL BE USED IN CONJUNCTION WITH THE STABILIZATION OF CONSTRUCTION ROADS TO REDUCE THE AMOUNT OF MUD PICKED UP BY CONSTRUCTION VEHICLES. ALL CONSTRUCTION ACCESS ROADS SHALL BE CONSTRUCTED PRIOR TO ANY ROADWAY ACCEPTING CONSTRUCTION TRAFFIC.

THE SITE OWNER AND OPERATOR MUST WILL RESTRICT VEHICLE USE TO PROPERLY DESIGNATED EXIT POINTS, USE PROPERLY DESIGNED AND CONSTRUCTED CONSTRUCTION ENTRANCES AT ALL POINTS THAT EXIT ONTO PAVED ROADS SO THAT SEDIMENT REMOVAL OCCURS PRIOR TO VEHICLE EXIT. WHEN AND WHERE NECESSARY, USE ADDITIONAL CONTROLS TO REMOVE SEDIMENT FROM VEHICLE TIRES PRIOR TO EXIT (I.E. WHEEL WASHING RACKS, RUMBLE STRIPS, AND RATTLE PLATES). WHERE SEDIMENT HAS BEEN TRACKED OFF FROM THE CONSTRUCTION SITE ONTO THE SURFACE OF OFF-SITE STREETS, OTHER PAVED AREAS, AND SIDEWALKS, THE DEPOSITED SEDIMENT MUST BE REMOVED BY THE END OF THE SAME WORK DAY IN WHICH THE TRACK-OUT OCCURS. TRACK-OUT MUST BE REMOVED BY SWEEPING, SHOVELING, OR VACUUMING THESE SURFACES, OR BY USING OTHER SIMILARLY EFFECTIVE MEANS OF SEDIMENT REMOVAL.

**STOCKPILE AND MATERIAL STAGING CONTAINMENT**

SHALL BE USED ON-SITE TO MINIMIZE OR ELIMINATE THE DISCHARGE OF SOIL, TOPSOIL, BASE MATERIAL OR RUBBLE, FROM ENTERING DRAINAGE SYSTEMS OR SURFACE WATERS. ALL STOCKPILES MUST BE LOCATED WITHIN THE LIMIT OF DISTURBANCE, PROTECTED FROM RUN-OFF WITH THE USE OF TEMPORARY SEDIMENT BARRIERS AND PROVIDED WITH COVER OR STABILIZATION TO AVOID CONTACT WITH PRECIPITATION AND WIND WHERE AND WHEN PRACTICAL. STOCK PILE MANAGEMENT CONSISTS OF PROCEDURES AND PRACTICES DESIGNED TO MINIMIZE OR ELIMINATE THE DISCHARGE OF STOCKPILED MATERIAL (SOIL, TOPSOIL, BASE MATERIAL, RUBBLE) FROM ENTERING DRAINAGE SYSTEMS OR SURFACE WATERS. FOR ANY STOCKPILES OR LAND CLEARING DEBRIS COMPOSED, IN WHOLE OR IN PART, OF SEDIMENT OR SOIL, YOU MUST COMPLY WITH THE FOLLOWING REQUIREMENTS - LOCATE PILES WITHIN THE DESIGNATED LIMITS OF DISTURBANCE OUTSIDE OF THE 100-FOOT BUFFER ZONE, PROTECT FROM CONTACT WITH STORMWATER (INCLUDING RUN-ON) USING A TEMPORARY PERIMETER SEDIMENT BARRIER; WHERE PRACTICABLE, PROVIDE COVER OR APPROPRIATE TEMPORARY VEGETATIVE OR STRUCTURAL STABILIZATION TO AVOID DIRECT CONTACT WITH PRECIPITATION OR TO MINIMIZE SEDIMENT DISCHARGE; NEVER HOSE DOWN OR SWEEP SOIL OR SEDIMENT ACCUMULATED ON PAVEMENT OR OTHER IMPERVIOUS SURFACES INTO ANY STORMWATER CONVEYANCE, STORM DRAIN INLET, OR SURFACE WATER; TO THE MAXIMUM EXTENT PRACTICABLE, CONTAIN AND SECURELY PROTECT FROM WIND.

**TEMPORARY SEDIMENT BASINS**

IF REQUIRED, ADDITIONAL TEMPORARY SEDIMENT BASINS ARE REQUIRED, TO THE PROPOSED MITIGATION DETAILED WITHIN THESE DESIGN PLANS, TO MITIGATE THE POTENTIAL SEDIMENT LOADING TO THE ADJACENT RESOURCE AREAS. THE DESIGN ENGINEER SHALL BE CONTACTED TO DESIGN AND SITE NEW TEMPORARY SEDIMENT BASINS AS REQUIRED. TEMPORARY SEDIMENT BASINS SHALL BE LOCATED OUTSIDE OF THE 100-FOOT BUFFER ZONE TO ANY RESOURCE AREAS THAT ARE NOT SCHEDULED FOR PERMANENT ALTERATION, UNLESS NO ALTERNATIVES ARE AVAILABLE. TEMPORARY SEDIMENT BASIN LOCATION, DESIGN AND GRADING BE DICTATED BY THE DESIGN ENGINEER. AT A MINIMUM THE VOLUME OF THE TEMPORARY SEDIMENT BASIN, MEASURED FROM THE BOTTOM OF THE BASE TO THE ELEVATION OF THE CREST OF THE PRINCIPAL SPILLWAY SHALL BE AT LEAST 3,600 CUBIC FEET PER ACRE OF DRAINAGE AREA. THIS IS EQUIVALENT TO 1.0 INCH OF SEDIMENT PER ACRE OF DRAINAGE AREA. ADDITIONAL STORAGE IN THE FORM OF A PERMANENT WET POOL SHALL BE PROVIDED WHENEVER PRACTICABLE, BUT MAY NOT BE USED TO FULFILL THE TEMPORARY STORAGE VOLUME REQUIREMENT.

SEDIMENT BASINS SHALL BE CLEANED OUT WHEN THE VOLUME REMAINING AS DESCRIBED ABOVE IS REDUCED BY SEDIMENTATION TO 1,800 CUBIC FEET PER ACRE OF DRAINAGE AREA (50 PERCENT FULL). IN NO CASE SHALL THE SEDIMENT LEVEL BE PERMITTED TO BUILD UP HIGHER THAN ONE FOOT BELOW THE PRINCIPAL SPILLWAY CREST. AT THIS ELEVATION, CLEANOUT SHALL BE PERFORMED TO RESTORE THE ORIGINAL DESIGN VOLUME TO THE SEDIMENT BASIN. THE ELEVATION OF THE MAXIMUM ALLOWABLE SEDIMENT LEVEL, SHALL BE DETERMINED AND SHALL BE STATED IN THE DESIGN DATA AS A DISTANCE BELOW THE TOP OF THE RISER AND BE CLEARLY MARKED ON THE RISER.

**CONSTRUCTION SEQUENCING**

1. CONSTRUCT WETLAND / INTERMITTENT STREAM CROSSING
2. INSTALL EROSION AND SEDIMENT CONTROLS;
3. CUT TREES
4. CLEAR TREES AND REMOVE/JOIN STUMPS
5. INSTALL TEMPORARY SEDIMENT BASINS AND CONVEYANCE SWALES AND BERMS;
6. GRUB AND ROUGH GRADE AREAS SHOWN TO BE RE-GRADED;
7. CONSTRUCT GRAVEL DRIVEWAYS;
8. INSTALL STORMWATER MANAGEMENT SYSTEM AND SITE UTILITIES WITH FINAL STABILIZATION;
9. INSTALL SOLAR PANELS AND RACKS AND STABILIZE ARRAY AREAS;
10. INSTALL SECURITY FENCING;
11. INSTALL SITE LANDSCAPING;
12. THE OWNER SHALL SOAK AND SEED ALL REMAINING DISTURBED AREAS;
13. PROJECT CLOSE OUT.

**EROSION CONTROL CONSTRUCTION NOTES**

IN ORDER TO FURTHER MINIMIZE SEDIMENT LOSS ON THE SITE, A GENERAL CONSTRUCTION SEQUENCE PLAN HAS BEEN DEVELOPED. PRIOR TO CONDUCTING WORK ASSOCIATED WITH THIS PROJECT, THE CONTRACTOR SHALL BE REQUIRED TO OBTAIN ALL COPIES OF PERMIT APPLICATIONS AND APPROVALS THAT OUTLINE CONDITIONS GOVERNING THE PROPOSED WORK. THE CONTRACTOR WILL ALSO REVIEW THE DRAWINGS PREPARED FOR THE PROJECT. THE CONTRACTOR WILL THEN FOLLOW THE GENERAL SEQUENCE OF WORK AS OUTLINED BELOW:

1. CONTRACTOR SHALL COORDINATE WITH LOCAL POLICE DEPARTMENT REGARDING TRAFFIC SAFETY MEASURES TO BE EMPLOYED DURING CONSTRUCTION.
2. A TRAFFIC CONTROL OFFICER SHALL BE USED FOR MAJOR DELIVERIES.
3. THE CONTRACTOR WILL PLACE ALL EROSION AND SEDIMENTATION CONTROL SYSTEMS IN ACCORDANCE WITH THE DRAWINGS, OR AS MAY BE DICTATED BY SITE CONDITIONS, IN ORDER TO MAINTAIN THE INTENT OF THE SPECIFICATIONS AND PERMITS. DEFICIENCIES OR CHANGES ON THE DRAWINGS SHALL BE CORRECTED OR IMPLEMENTED AS SITE CONDITIONS CHANGE. CHANGES DURING CONSTRUCTION SHALL BE NOTED AND POSTED ON THE DRAWINGS (SITE PLANS).
4. THE INTENT IS TO DIRECT ALL WATER FROM DISTURBED AREAS THROUGH SEDIMENTATION CONTROLS PRIOR TO LEAVING CONSTRUCTION BOUNDARIES. THERE SHALL BE NO DISCHARGE OF UNTREATED CONSTRUCTION RUNOFF FROM THIS SITE.
5. THE CONTRACTOR SHALL MAINTAIN TEMPORARY EROSION AND SEDIMENTATION CONTROL SYSTEMS AS DICTATED BY SITE CONDITIONS, INDICATED IN THE CONSTRUCTION DOCUMENTS, OR AS DIRECTED BY GOVERNING AUTHORITIES OR OWNER TO CONTROL SEDIMENT UNTIL FINAL STABILIZATION.
6. THE CONTRACTOR SHALL RESPOND TO ANY MAINTENANCE OR ADDITIONAL WORK ORDERED BY OWNER OR GOVERNING AUTHORITIES IMMEDIATELY, IF REQUIRED, AND ALWAYS WITHIN 7 DAYS.
8. THE CONTRACTOR SHALL INCORPORATE PERMANENT EROSION CONTROL FEATURES, PERMANENT SLOPE STABILIZATION, AND VEGETATION INTO THE PROJECT PLANS AT THE EARLIEST PRACTICAL TIME TO MINIMIZE THE NEED FOR TEMPORARY CONTROLS.
9. TREE AND VEGETATION CLEARING AND ANY ROUGH GRADING SHALL ONLY OCCUR IF THE DISTURBED SOIL SURFACE CAN BE STABILIZED WITHIN 48 HOURS OF CLEARING. TREE AND VEGETATION CLEARING SHALL BE SCHEDULED IN CONJUNCTION WITH WEATHER FORECAST SUCH THAT NO MORE THAN 1/4" OF RAIN IS TO BE EXPECTED WITHIN 48 HOURS OF ANY CLEARING OR GRADING ACTIVITY.
10. ANY AREA DISTURBED WITHIN THE LIMIT OF WORK, BUT NOT WITHIN THE LIMITS OF THE SOLAR ARRAY FOOTPRINT ARE TO BE RESEED WITH NEW ENGLAND CONSERVATION/ WILDLIFE SEED MIX UNLESS SPECIFIED OTHERWISE IN THE PLAN SET.
11. THE CONTRACTOR SHALL STABILIZE ALL DISTURBED AREAS WITHIN 48 HOURS AFTER FINAL GRADING. IN THE EVENT THAT IT IS NOT PRACTICAL TO SEED AREAS, SLOPES MUST BE STABILIZED WITH GEOTEXTILE FABRIC OR OTHER MEANS TO REDUCE THE EROSION POTENTIAL OF THE AREA.

**EROSION STRUCTURAL PRACTICES**

**SILTATION CONTROL USING EROSION 18" DIA. FILTER SOCKS, OR APPROVED EQUAL.**

EROSION CONTROL LINE IS TO BE USUALLY INSPECTED AFTER EVERY RAIN FALL AND REPAIRS MADE AS REQUIRED TO THE 18" SILT SOCKS AFTER EACH RAIN FALL. CLEANOUT OF ACCUMULATED SEDIMENT BEHIND THE WATTLE IS NECESSARY IF 1/2 OF THE ORIGINAL HEIGHT OF THE WATTLE APPEARS TO HAVE BEEN INUNDATED WITH SEDIMENT.

**PRESERVE TOPSOIL**

SITE OWNERS AND OPERATORS MUST PRESERVE EXISTING TOPSOIL ON THE CONSTRUCTION SITE TO THE MAXIMUM EXTENT FEASIBLE AND AS NECESSARY TO SUPPORT HEALTHY VEGETATION, PROMOTE SOIL STABILIZATION, AND INCREASE STORMWATER INFILTRATION RATES IN THE POST-CONSTRUCTION PHASE OF THE PROJECT.

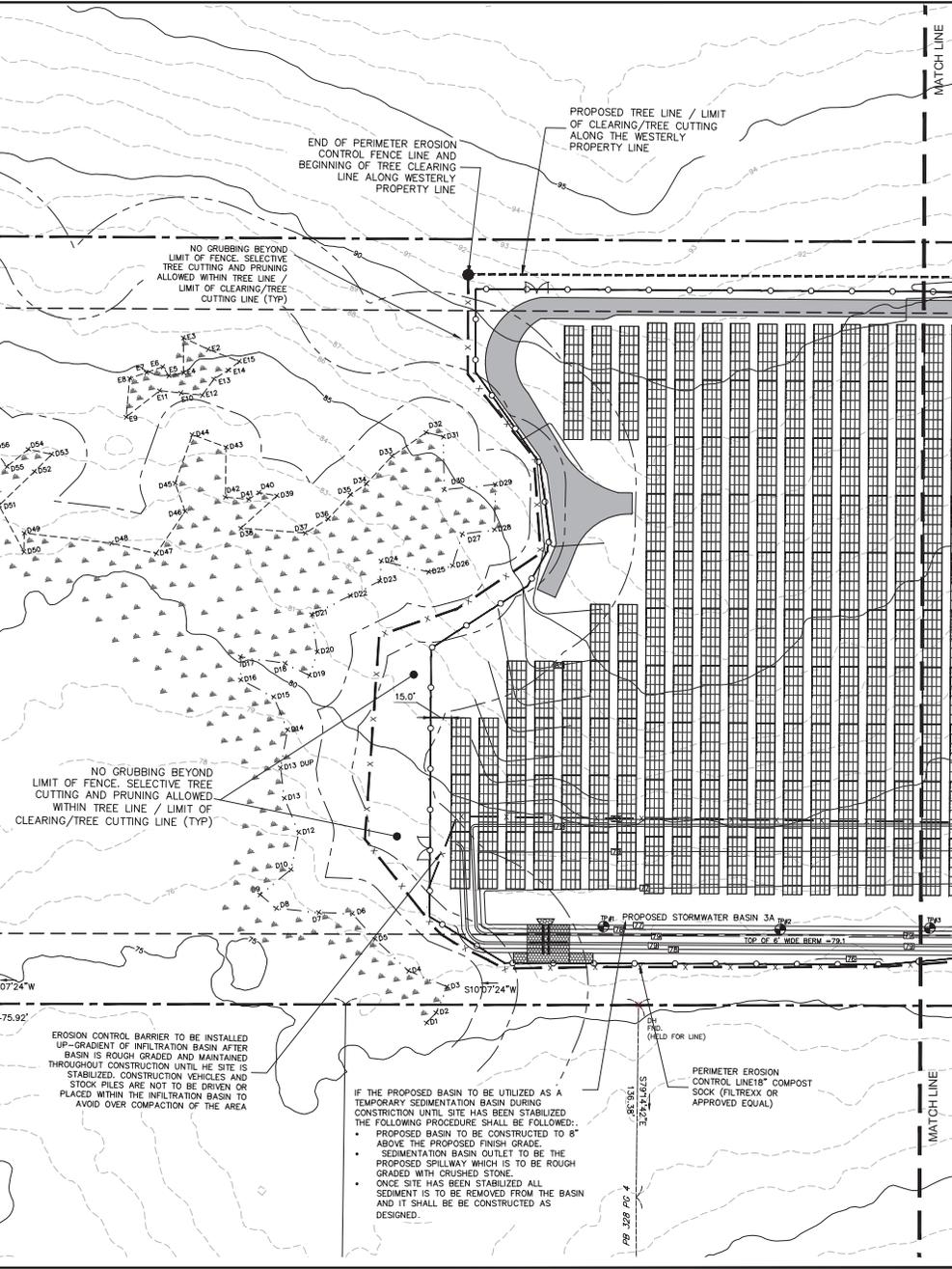
**STABILIZATION OF SOILS**

UPON COMPLETION AND ACCEPTANCE OF SITE PREPARATION AND INITIAL INSTALLATION OF EROSION, RUNOFF, AND SEDIMENT CONTROLS AND TEMPORARY POLLUTION PREVENTION MEASURES, THE CONTRACTOR SHALL INITIATE APPROPRIATE TEMPORARY OR PERMANENT STABILIZATION PRACTICES DURING ALL PHASES OF CONSTRUCTION ON ALL DISTURBED AREAS AS SOON AS POSSIBLE BUT NOT MORE THAN FOURTEEN (14) DAYS AFTER THE CONSTRUCTION ACTIVITY IN THAT AREA HAS TEMPORARILY OR PERMANENTLY CEASED UNLESS THE ACTIVITY IS TO RESUME WITHIN TWENTY-ONE (21) DAYS.

ANY DISTURBED AREAS THAT WILL NOT HAVE ACTIVE CONSTRUCTION ACTIVITY OCCURRING WITHIN FOURTEEN (14) DAYS AFTER THE CONSTRUCTION ACTIVITY IN THAT AREA HAS TEMPORARILY OR PERMANENTLY CEASED UNLESS THE ACTIVITY IS TO RESUME WITHIN TWENTY-ONE (21) DAYS MUST BE STABILIZED BY THE USE OF TEMPORARY AND/OR FINAL SEEDING OF THAT AREA.

ONLY AREAS THAT CAN BE REASONABLY EXPECTED TO HAVE ACTIVE CONSTRUCTION WORK BEING PERFORMED WITHIN 14 DAYS OF DISTURBANCE WILL BE CLEARED/GRUBBED AT ANY ONE TIME. IT IS NOT ACCEPTABLE TO GRUB AND STRIP TOP SOIL THE ENTIRE CONSTRUCTION SITE IF PORTIONS WILL NOT BE ACTIVE WITHIN THE 14-DAY TIME FRAME. PROPER PHASING OF CLEARING AND GRUBBING ACTIVITIES SHALL INCLUDE TEMPORARY STABILIZATION TECHNIQUES FOR AREAS CLEARED AND GRUBBED THAT WILL NOT BE ACTIVE WITHIN THE 14-DAY TIME FRAME.

STEEP SLOPES SHALL NOT BE LEFT UNATTENDED OR EXPOSED FOR EXCESSIVE PERIODS OF TIME SUCH AS THE INACTIVE WINTER SEASON. THE CONTRACTOR SHALL INITIATE APPROPRIATE VEGETATIVE PRACTICES ON ALL DISTURBED AREAS IN AREAS OF STEEP SLOPES AS SOON AS POSSIBLE BUT NOT MORE THAN FOURTEEN (14) DAYS AFTER THE CONSTRUCTION ACTIVITY IN THAT AREA HAS TEMPORARILY OR PERMANENTLY CEASED, UNLESS THE ACTIVITY IS TO RESUME WITHIN TWENTY-ONE (21) DAYS. ONCE AN STEEP SLOPE AREA HAS BEEN TEMPORARY AND/OR FINAL SEEDING IT SHALL BE PROTECTED WITH 4" HIGH ORANGE CONSTRUCTION TO PREVENT FURTHER DISTURBANCE OF THE AREA.



NO.	DATE	REVISIONS
1	01/26/2021	ISSUE FOR CONSTRUCTION
2	08/26/2021	REVISION FOR SHEET 1817.00

SCALE: 1" = 40'

DATE: AUGUST 21, 2020  
DRAWN: NP/ERIC

PROJECT: BROOK STREET COMMERCIAL SOLAR FACILITY

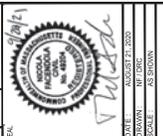
**BROOK STREET SOLAR COMMERCIAL SOLAR FACILITY**  
ASSESSOR PARCEL - MAP 16; PARCEL 28  
BROOK STREET  
DIGHTON, MASSACHUSETTS

**LEVEL**  
CIVIL ENGINEERING / LAND SURVEYING  
240 SOUTH STREET  
LITTLETON, CO 80120  
TEL: (303) 695-2221 FAX: (303) 695-2219

**EROSION CONTROL**  
**C-3.1**  
SHEET 2 OF 10  
1817.00



NO.	DATE	REVISIONS
1	11/15/2017	ISSUE FOR PERMITS
2	11/15/2017	ISSUE FOR PERMITS
3	11/15/2017	ISSUE FOR PERMITS



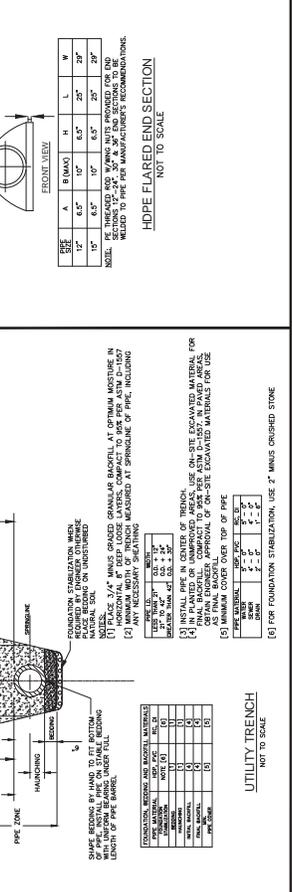
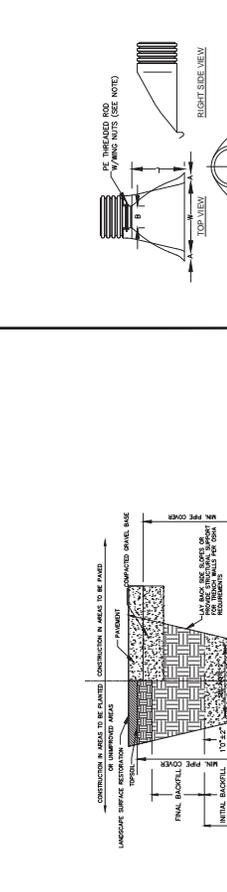
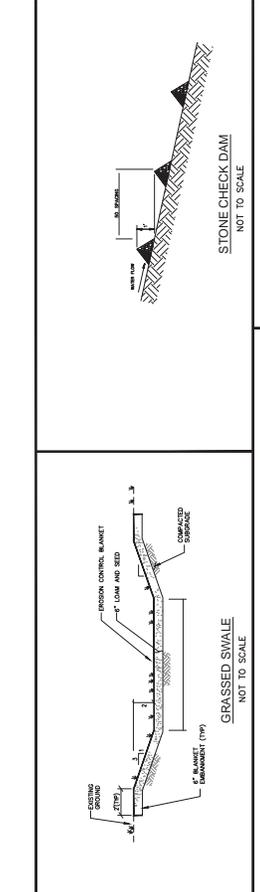
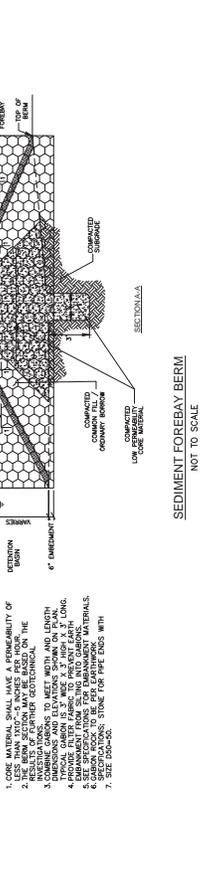
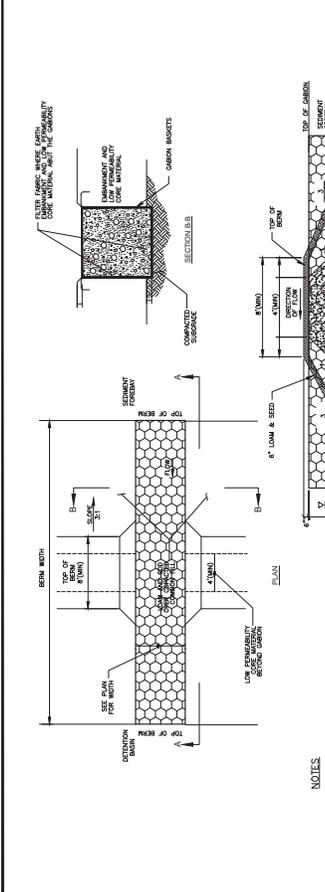
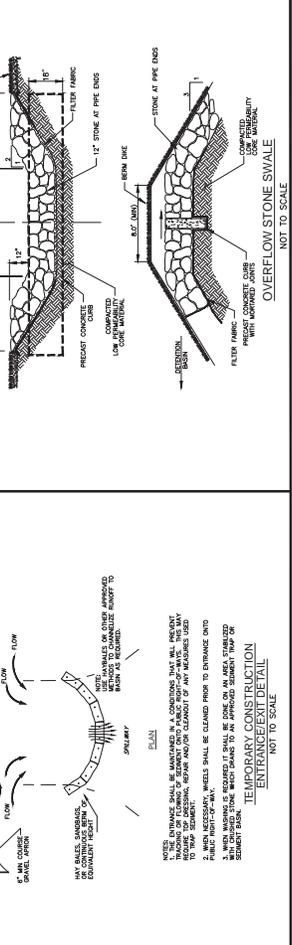
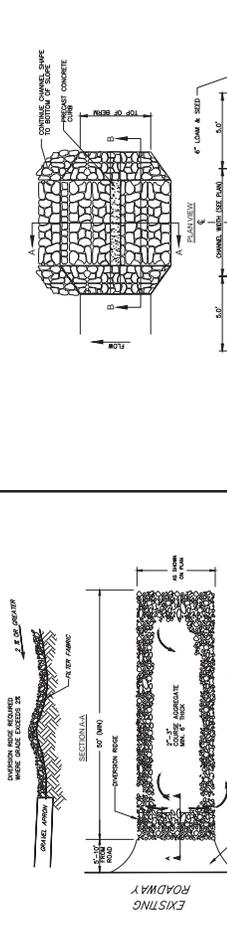
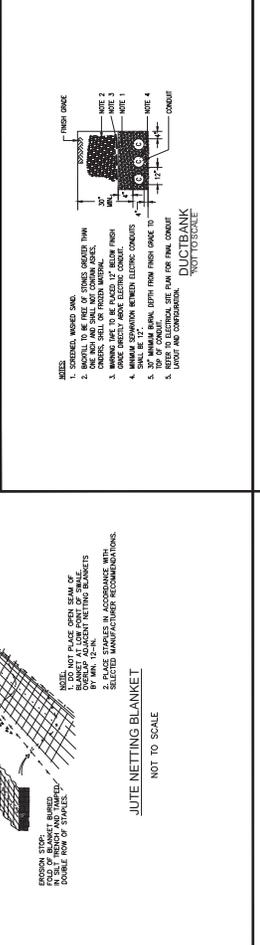
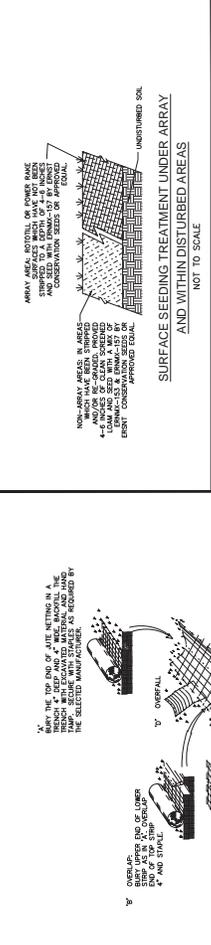
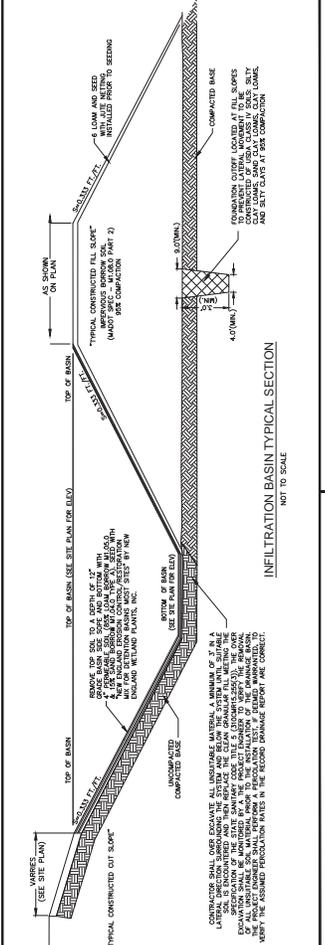
DATE: 11/15/2017  
 DRAWN BY: DDC  
 SCALE: AS SHOWN

# BROOK STREET SOLAR COMMERCIAL SOLAR FACILITY

ASSESSOR PARCEL - MAP 16; PARCEL 28  
 BROOK STREET  
 DIGHTON, MASSACHUSETTS

**LEVED**  
 CIVIL ENGINEERING AND SURVEYING  
 100 WASHINGTON STREET  
 DIGHTON, MA 01920  
 TEL: (508) 952-2221 FAX: (508) 952-2219

**DETAILS**  
**C-5.0**  
 SHEET TOP 10  
**1817.00**



NOT TO SCALE





# TOWN OF DIGHTON

## PLANNING BOARD

979 Somerset Avenue  
Dighton, MA 02715  
Tel: (508) 669-6636, Ext. 114

### NOTICE OF DECISION MINOR SITE PLAN APPROVAL

APPLICANT: GRASSHOPPER ENERGY, LLC  
c/o GHTJA03, LLC  
5935 AIRPORT ROAD, SUITE 210  
MISSISSAUGA, ON L4V 1W5

1. On or about December 10, 2020 the Dighton Planning Board received notification for a request for a Minor Site Plan Review. The proposed modification seeks to reduce the culvert width from 25' to 18' wide, realign the width and layout of the gravel access driveway, reposition the proposed access gate and signage and to relocate the proposed utility poles from the west side of the driveway to the east side of the driveway.

The proposed use requires SITE PLAN APPROVAL from the Planning Board pursuant to 5460 of the Dighton Zoning Bylaws, entitled Minor Site Plan.

2. The site is located at 0 Brook Street and shown on Assessors' Map 16, Lot 28.
3. This decision is accompanied by plan entitled Driveway Modification Site Plan dated December 10, 2020 consisting of one (1) sheet.
4. The Dighton Planning Board at a regular scheduled meeting held on January 6, 2021 Voted to: ( ) grant, (X) grant, subject to conditions, ( ) deny the above referenced request to APPROVE the MINOR Special Permit/Site Plan. Condition of approval, if any: the Applicant will maintain the culvert in perpetuity as determined by the Stormwater Committee.

**DIGHTON PLANNING BOARD**

*Timothy F. Rhines*

Timothy Rhines, Chairman

Robert Boughner, Vice Chairman

*Joseph Figueredo*

Joseph Figueredo, Member

Robert Woods, Member

Jeff Carvalho, Member

The following members of the Planning Board are in opposition to the grant of the special permit:

\_\_\_\_\_  
\_\_\_\_\_

Filed with the Town Clerk on January 21, 2021.

*Susana Medeiros*  
Susana Medeiros, Town Clerk

- cc: Conservation Commission
- Board of Health
- Building Commissioner
- Town Engineer
- Highway Department
- Fire Chief

RECEIVED  
2021 JAN 21 AM 9:18  
TOWN CLERK  
DIGHTON, MA

STORMWATER SUMMARY FOR  
BASIN 1 MODIFICATION  
TO SUPPORT A  
SPECIAL PERMIT MODIFICATION  
FOR BROOK STREET SOLAR-COMMERCIAL SOLAR FACILITY  
893 BROOK STREET, DIGHTON, MA  
ASSESSOR MAP 16; PARCEL 28

Level Design Group, L.L.C. (LDG), on behalf of the project developer, GHTJA03, LLC (Grasshopper Energy), has prepared the following analysis for the maintenance/repair of the two existing on-site stormwater management basins located at the above-referenced parcel. The analysis intends to provide a modified design that will result in the basins draining within 72 hours after a storm event. Currently, Basin 1 is retaining stormwater for a prolonged period of time despite the basins being reconstructed in the fall of 2022 to remove unsuitable materials from below the basin floor and to regrade and re-install the basin outlets per the original design plan. As part of the review and design of the basin modification, LDG has taken into account recommendations and findings by Weston & Sampson detailed in two letters dated December 11, 2023, & March 15, 2024, addressed to the Town of Dighton Stormwater Committee.

The proposed basin improvements and calculations included in this review are based on a drainage as-built survey prepared by LDG dated November 17, 2022. The drainage as-built survey details existing as-built site grades within the basin footprints, installed outlets, and installed solar panel racking within the basin areas.

**Basin 1 Maintenance / Repair:**

The proposed modifications to Basin 1 include the installation of a new 4" perforated pipe basin subdrain which will daylight to a solid 4" PVC outlet pipe discharging to the existing splash pad/level spreader. The subdrain consists of a network of 4" perforated PVC pipes at an installed slope of 0.005 ft/ft embedded in the crushed stone floor of Basin 1. The subdrain is located within the low point of the existing basin in the northeast corner of the basin floor. The existing grade of the basin floor in this area is between 75.7 – 76.3. As part of the proposed basin modification, the basin floor in this area will be filled with additional crushed stone to provide an approximately level basin floor elevation of 76.5. The additional crushed stone will provide adequate cover over the proposed basin subdrain and allow for the water in the basin to be efficiently collected into the subdrain network and discharged through the 4" solid PVC pipe.

A review of the existing basin volume and adjustments made for the additional crushed stone to be added to the basin floor detail a total basin volume 28,778 cu.ft. of storage volume below the crest of the installed outlet weir at elevation 78.70. Based on the total storage volume and the calculated capacity of a 4" PVC pipe flowing full installed at a 0.010 ft/ft slope being equal to 0.22 cfs, the basin if full, will be able to fully drain through the 4" pipe within 36.34 hours (see the calculation below).

$$[(28,788 \text{ cu.ft.}) / (0.22 \text{ cu.ft /sec})] / (3,600 \text{ seconds/hour}) = 36.34 \text{ hours (note: this calculation assumes no infiltration occurs through the bottom of the basin floor).}$$

Based on the provided calculation the basin will be able to fully drain through the proposed 4" pipe well within the required 72-hour time period. If the 4" pipe were to be only flowing half-full due to a partial blockage the basin would still drain in approximately 72.6 hours based on an analysis of the 4" pipe flowing a half its calculated capacity.

In addition to the analysis of the proposed 4" PVC outlet, LDG has recreated the HydroCAD model to evaluate the peak rate of runoff and flows from the 2-, 10-, 25-, & 100-year storm events at Design Point 1. Within the provided analysis the contributing sub-catchments are identical to the approved stormwater report prepared by Atlantic Engineers dated 07/16/2018 and the subsequent Addendums dated 11/19/2018 & 12/05/2018. The original analysis for Basin 1 included an exfiltration rate of 2.41 inches per hour associated with Loamy Sand material. The new HydroCAD model for the proposed modifications to Basin 1 includes the new 4" subdrain outlet pipe, the as-built basin volume and outlet weir, and an exfiltration rate that has been adjusted to 0.27 inches per hour for a Sandy Clay Loam soil textural class to more accurately model the infiltration through the basin. The table below details the previously approved pre-development and post-development flows and volumes as compared to the currently proposed basin modification flow and volume for the design storm events.

The table above details that the proposed post-development flow is mitigated for all storm events as compared to the originally approved pre-development flow rates. There are minor increases to the calculated proposed post-development volumes associated with each design storm. The post-development flows are unavoidable given that

<b>Design Point 1</b>	Pre - Development Flow	Pre - Development Volume	Approved Post-Development Flow	Approved Post-Development Volume	Proposed Post-Development Flow	Proposed Post-Development Volume	
	cfs	af	cfs	af	cfs	af	increase
2-year	<b>7.13</b>	<b>1.53</b>	6.40	1.31	<b>6.78</b>	<b>1.68</b>	<b>0.15</b>
10-year	<b>20.48</b>	<b>4.00</b>	19.44	3.43	<b>18.26</b>	<b>4.07</b>	<b>0.07</b>
25-year	<b>30.02</b>	<b>5.75</b>	29.42	5.11	<b>28.14</b>	<b>5.83</b>	<b>0.08</b>
100-year	<b>45.69</b>	<b>8.67</b>	45.30	7.93	<b>44.76</b>	<b>8.80</b>	<b>0.13</b>

current basin configuration was originally designed to fully infiltrate the 2-year storm event and was designed with no outlets other than the overflow weir and an infiltration rate that is nine (9) times the infiltration rate utilized in the current analysis.

Based on the analysis above and provided calculations and updated HydroCAD model of the proposed modifications to Basin 1 will allow for the basin to fully drain within 72-hours after a storm event. The modified basin continues to mitigate peak flows at the original design points as required by current MADEP Stormwater Management Standards and current Town of Dighton Stormwater Regulations.

**Basin 3 Maintenance / Repair (not included as part of the Special Permit Modification):**

The proposed modifications to Basin 3 include re-grading the basin floor to provide a positive pitch from the northerly end of the basin to the southerly end of the basin where the basin outlet pipes are located. A review of the current Basin 3 grading details that the basin below point is located in the northerly part of the basin at the approximate elevation of 76±. The proposed re-grading of the basin will pull the 76 contour to the southerly side of the basin creating the low point of the basin floor in the location of the two outlet pipes allowing the basin to properly drain.

In addition to re-grading the basin floor, the two outlet pipes will have their outlets reset to the regraded bottom of the basin. Outlet Pipe 1 will have a 6"x4" reducer installed in order to maintain the post-development design flow at less than 0.92 cfs for the 2-year storm. Outlet Pipe 2 will remain as a 6" outlet with a modified invert elevation. These proposed minor modifications to the installed basin outlets will minimize site disturbance to the existing basin while providing the required peak flow mitigation.

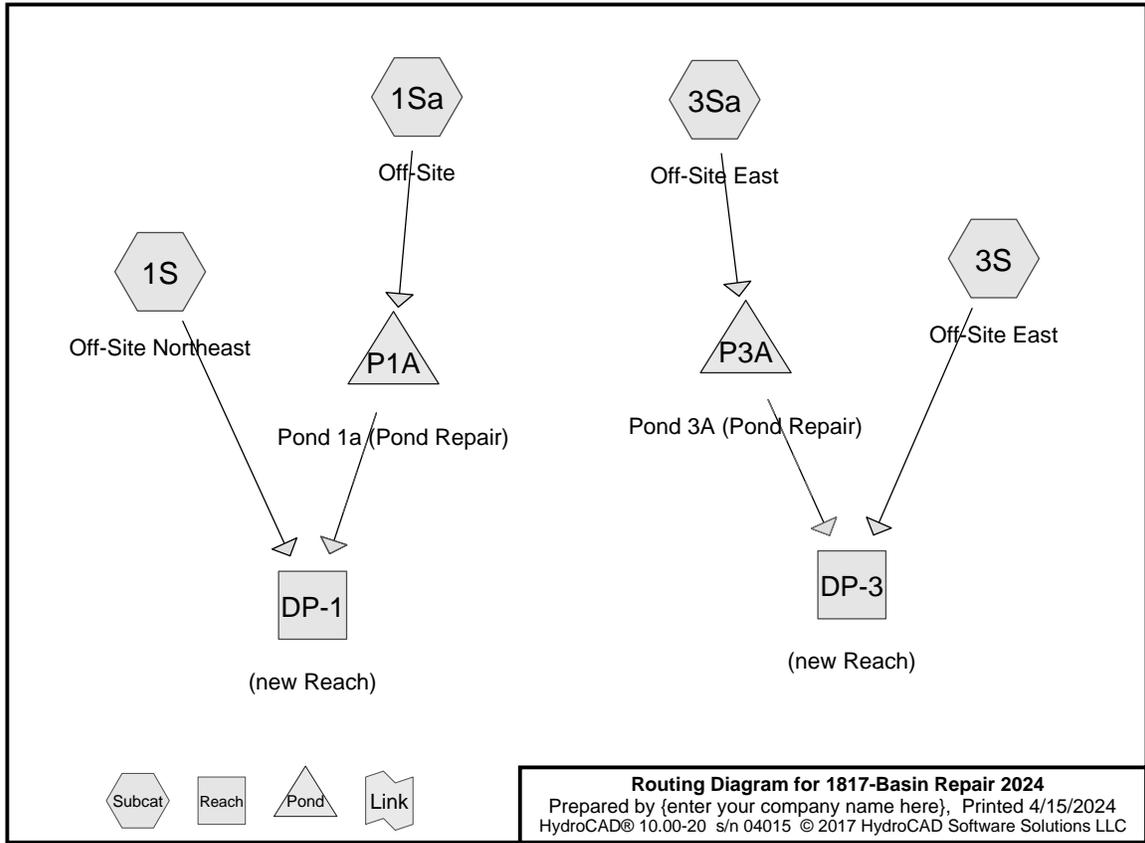
The table above details that the proposed post-development flow is mitigated for all storm events as compared to the originally approved pre-development flow rates. Despite the minor change in basin volume the proposed post-development volume is exactly the same as the current approved post-development design volume. The approved post-development design volumes all exceeded the pre-development design volumes as detailed in the table above.

<b>Design Point 3</b>	Pre - Development Flow	Pre - Development Volume	Approved Post-Development Flow	Approved Post-Development Volume	Proposed Post-Development Flow	Proposed Post-Development Volume
Storm	cfs	af	cfs	af	cfs	af
2-year	<b>0.92</b>	<b>0.14</b>	0.86	0.30	<b>0.91</b>	<b>0.30</b>
10-year	<b>2.63</b>	<b>0.36</b>	2.17	0.63	<b>2.20</b>	<b>0.63</b>
25-year	<b>3.84</b>	<b>0.52</b>	2.95	0.85	<b>2.95</b>	<b>0.85</b>
100-year	<b>5.81</b>	<b>0.78</b>	5.75	1.20	<b>4.07</b>	<b>1.20</b>

Based on the analysis above and the updated HydroCAD model the proposed modifications to the approved Basin 3 will allow for the basin to fully drain to the basin floor elevation of 76.0 within 72-hours of a storm event. The modified basin continues to mitigate peak flows at the original design point as required by as required by current MADEP Stormwater Management Standards and current Town of Dighton Stormwater Regulations.

**Summary:**

The proposed design changes changes to Basin 1 will allow the stormwater basins to dewater within the required 72-hour time period after a stormwater event and are in line with the recommendations and findings by Weston & Sampson detailed in two letters dated December 11, 2023 & March 15, 2024 addressed to the Town of Dighton Stormwater Committee. The modified basin will continue to mitigate peak flows at the original design points originally approved and as required by as required by current MADEP Stormwater Management Standards and current Town of Dighton Stormwater Regulations.



Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

**1817-Basin Repair 2024**

Prepared by {enter your company name here}  
 HydroCAD® 10.00-20 s/n 04015 © 2017 HydroCAD Software Solutions LLC

Printed 4/15/2024  
 Page 2

**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
7.602	74	>75% Grass cover, Good, HSG C (1S, 1Sa, 3S, 3Sa)
0.015	98	Equipment Pad, HSG C (1Sa)
0.073	96	Gravel Road (3Sa)
0.133	96	Gravel Road, HSG C (1S)
0.228	98	Gravel Road, HSG C (1Sa)
1.250	98	Water Surface, HSG C (1Sa, 3Sa)
15.202	70	Woods, Good, HSG C (1S, 3S)
<b>24.502</b>	<b>73</b>	<b>TOTAL AREA</b>

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Page 3**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
24.430	HSG C	1S, 1Sa, 3S, 3Sa
0.000	HSG D	
0.073	Other	3Sa
<b>24.502</b>		<b>TOTAL AREA</b>

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Page 4**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	7.602	0.000	0.000	7.602	>75% Grass cover, Good	1S, 1Sa, 3S, 3Sa
0.000	0.000	0.015	0.000	0.000	0.015	Equipment Pad	1Sa
0.000	0.000	0.361	0.000	0.073	0.434	Gravel Road	1S, 1Sa, 3Sa
0.000	0.000	1.250	0.000	0.000	1.250	Water Surface	1Sa, 3Sa
0.000	0.000	15.202	0.000	0.000	15.202	Woods, Good	1S, 3S
<b>0.000</b>	<b>0.000</b>	<b>24.430</b>	<b>0.000</b>	<b>0.073</b>	<b>24.502</b>	<b>TOTAL AREA</b>	

**1817-Basin Repair 2024**

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**Pipe Listing (all nodes)**

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	P1A	75.50	75.10	40.0	0.0100	0.013	4.0	0.0	0.0
2	P3A	76.00	75.52	20.0	0.0240	0.013	4.0	0.0	0.0
3	P3A	76.55	75.60	20.0	0.0475	0.013	6.0	0.0	0.0

**1817-Basin Repair 2024**

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Type III 24-hr 2 Year Rainfall=3.21"

Time span=1.00-73.00 hrs, dt=0.01 hrs, 7201 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment 1S: Off-Site Northeast**

Runoff Area=772,071 sf 0.00% Impervious Runoff Depth=0.88"  
Flow Length=1,645' Tc=61.7 min CN=71 Runoff=6.40 cfs 1.306 af

**Subcatchment 1Sa: Off-Site**

Runoff Area=190,352 sf 20.04% Impervious Runoff Depth=1.34"  
Flow Length=540' Tc=12.8 min CN=79 Runoff=5.43 cfs 0.490 af

**Subcatchment 3S: Off-Site East**

Runoff Area=21,487 sf 0.00% Impervious Runoff Depth=0.94"  
Tc=6.0 min CN=72 Runoff=0.50 cfs 0.038 af

**Subcatchment 3Sa: Off-Site East**

Runoff Area=83,406 sf 32.23% Impervious Runoff Depth=1.62"  
Flow Length=366' Tc=8.6 min CN=83 Runoff=3.31 cfs 0.258 af

**Reach DP-1: (new Reach)**

Inflow=6.78 cfs 1.681 af  
Outflow=6.78 cfs 1.681 af

**Reach DP-3: (new Reach)**

Inflow=0.91 cfs 0.297 af  
Outflow=0.91 cfs 0.297 af

**Pond P1A: Pond 1a (Pond Repair)**

Peak Elev=77.57' Storage=9,773 cf Inflow=5.43 cfs 0.490 af  
Discarded=0.16 cfs 0.114 af Primary=0.38 cfs 0.375 af Secondary=0.00 cfs 0.000 af Outflow=0.53 cfs 0.490 af

**Pond P3A: Pond 3A (Pond Repair)**

Peak Elev=77.03' Storage=4,350 cf Inflow=3.31 cfs 0.258 af  
Primary=0.34 cfs 0.200 af Secondary=0.40 cfs 0.058 af Tertiary=0.00 cfs 0.000 af Outflow=0.74 cfs 0.258 af

**Total Runoff Area = 24.502 ac Runoff Volume = 2.092 af Average Runoff Depth = 1.02"**  
**93.91% Pervious = 23.009 ac 6.09% Impervious = 1.493 ac**

**1817-Basin Repair 2024**

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**Summary for Subcatchment 1S: Off-Site Northeast**

Runoff = 6.40 cfs @ 12.95 hrs, Volume= 1.306 af, Depth= 0.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2 Year Rainfall=3.21"

Area (sf)	CN	Description
650,962	70	Woods, Good, HSG C
115,309	74	>75% Grass cover, Good, HSG C
* 5,800	96	Gravel Road, HSG C
772,071	71	Weighted Average
772,071		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.0	50	0.0080	0.03		<b>Sheet Flow,</b> Woods: Dense underbrush n= 0.800 P2= 3.00"
12.6	628	0.0276	0.83		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
3.3	496	0.0276	2.49		<b>Shallow Concentrated Flow,</b> Grassed Waterway Kv= 15.0 fps
13.8	471	0.0130	0.57		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
61.7	1,645	Total			

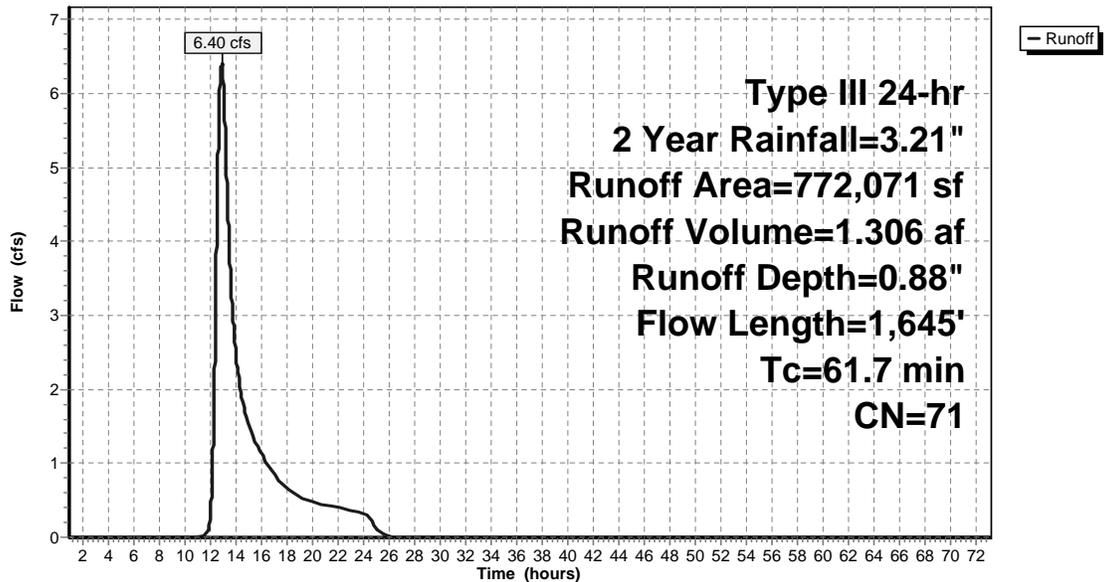
**1817-Basin Repair 2024**

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**Subcatchment 1S: Off-Site Northeast**

**Hydrograph**



**1817-Basin Repair 2024**

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**Hydrograph for Subcatchment 1S: Off-Site Northeast**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.03	0.00	0.00	36.00	3.21	0.88	0.00	71.00	3.21	0.88	0.00
2.00	0.06	0.00	0.00	37.00	3.21	0.88	0.00	72.00	3.21	0.88	0.00
3.00	0.10	0.00	0.00	38.00	3.21	0.88	0.00	73.00	3.21	0.88	0.00
4.00	0.14	0.00	0.00	39.00	3.21	0.88	0.00				
5.00	0.18	0.00	0.00	40.00	3.21	0.88	0.00				
6.00	0.23	0.00	0.00	41.00	3.21	0.88	0.00				
7.00	0.29	0.00	0.00	42.00	3.21	0.88	0.00				
8.00	0.37	0.00	0.00	43.00	3.21	0.88	0.00				
9.00	0.47	0.00	0.00	44.00	3.21	0.88	0.00				
10.00	0.61	0.00	0.00	45.00	3.21	0.88	0.00				
11.00	0.80	0.00	0.00	46.00	3.21	0.88	0.00				
12.00	1.60	0.13	0.25	47.00	3.21	0.88	0.00				
13.00	2.41	0.45	6.30	48.00	3.21	0.88	0.00				
14.00	2.60	0.54	2.54	49.00	3.21	0.88	0.00				
15.00	2.74	0.62	1.54	50.00	3.21	0.88	0.00				
16.00	2.84	0.67	1.14	51.00	3.21	0.88	0.00				
17.00	2.92	0.71	0.85	52.00	3.21	0.88	0.00				
18.00	2.98	0.75	0.67	53.00	3.21	0.88	0.00				
19.00	3.03	0.78	0.54	54.00	3.21	0.88	0.00				
20.00	3.07	0.80	0.48	55.00	3.21	0.88	0.00				
21.00	3.11	0.83	0.44	56.00	3.21	0.88	0.00				
22.00	3.15	0.85	0.40	57.00	3.21	0.88	0.00				
23.00	3.18	0.87	0.37	58.00	3.21	0.88	0.00				
24.00	3.21	0.88	0.33	59.00	3.21	0.88	0.00				
25.00	3.21	0.88	0.12	60.00	3.21	0.88	0.00				
26.00	3.21	0.88	0.01	61.00	3.21	0.88	0.00				
27.00	3.21	0.88	0.00	62.00	3.21	0.88	0.00				
28.00	3.21	0.88	0.00	63.00	3.21	0.88	0.00				
29.00	3.21	0.88	0.00	64.00	3.21	0.88	0.00				
30.00	3.21	0.88	0.00	65.00	3.21	0.88	0.00				
31.00	3.21	0.88	0.00	66.00	3.21	0.88	0.00				
32.00	3.21	0.88	0.00	67.00	3.21	0.88	0.00				
33.00	3.21	0.88	0.00	68.00	3.21	0.88	0.00				
34.00	3.21	0.88	0.00	69.00	3.21	0.88	0.00				
35.00	3.21	0.88	0.00	70.00	3.21	0.88	0.00				

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**Summary for Subcatchment 1Sa: Off-Site**

Runoff = 5.43 cfs @ 12.18 hrs, Volume= 0.490 af, Depth= 1.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 2 Year Rainfall=3.21"

Area (sf)	CN	Description
152,204	74	>75% Grass cover, Good, HSG C
* 9,937	98	Gravel Road, HSG C
27,571	98	Water Surface, HSG C
* 640	98	Equipment Pad, HSG C
190,352	79	Weighted Average
152,204		79.96% Pervious Area
38,148		20.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	50	0.0380	0.19		<b>Sheet Flow,</b> Grass: Short n=0.150 P2= 3.00"
8.3	490	0.0196	0.98		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
12.8	540	Total			

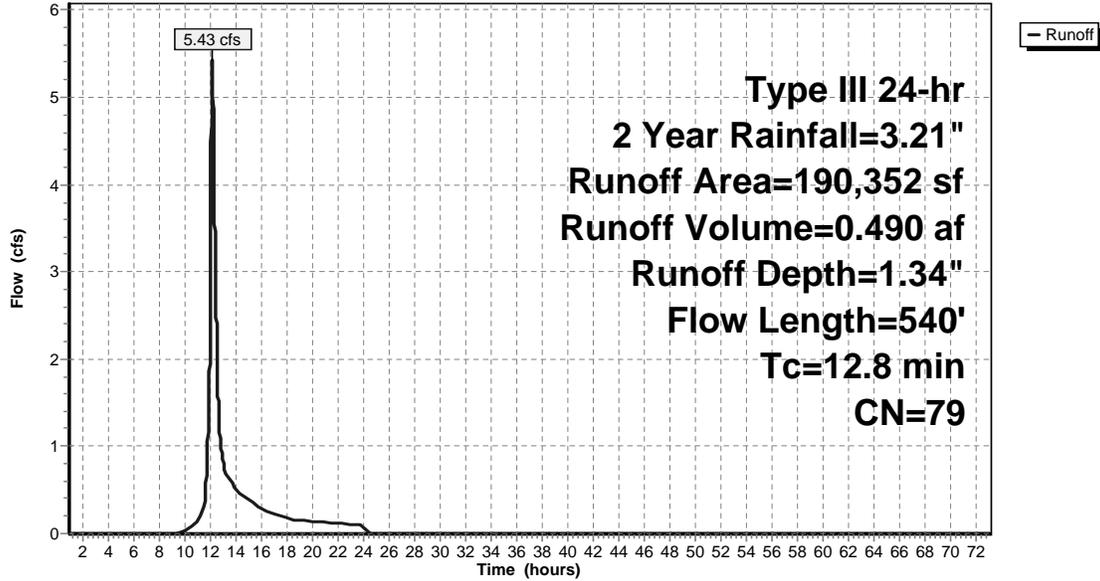
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Subcatchment 1Sa: Off-Site

Hydrograph



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Hydrograph for Subcatchment 1Sa: Off-Site

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.03	0.00	0.00	36.00	3.21	1.34	0.00	71.00	3.21	1.34	0.00
2.00	0.06	0.00	0.00	37.00	3.21	1.34	0.00	72.00	3.21	1.34	0.00
3.00	0.10	0.00	0.00	38.00	3.21	1.34	0.00	73.00	3.21	1.34	0.00
4.00	0.14	0.00	0.00	39.00	3.21	1.34	0.00				
5.00	0.18	0.00	0.00	40.00	3.21	1.34	0.00				
6.00	0.23	0.00	0.00	41.00	3.21	1.34	0.00				
7.00	0.29	0.00	0.00	42.00	3.21	1.34	0.00				
8.00	0.37	0.00	0.00	43.00	3.21	1.34	0.00				
9.00	0.47	0.00	0.00	44.00	3.21	1.34	0.00				
10.00	0.61	0.00	0.02	45.00	3.21	1.34	0.00				
11.00	0.80	0.03	0.15	46.00	3.21	1.34	0.00				
12.00	1.60	0.31	2.14	47.00	3.21	1.34	0.00				
13.00	2.41	0.78	0.84	48.00	3.21	1.34	0.00				
14.00	2.60	0.91	0.52	49.00	3.21	1.34	0.00				
15.00	2.74	1.00	0.39	50.00	3.21	1.34	0.00				
16.00	2.84	1.08	0.28	51.00	3.21	1.34	0.00				
17.00	2.92	1.13	0.22	52.00	3.21	1.34	0.00				
18.00	2.98	1.17	0.17	53.00	3.21	1.34	0.00				
19.00	3.03	1.21	0.15	54.00	3.21	1.34	0.00				
20.00	3.07	1.24	0.14	55.00	3.21	1.34	0.00				
21.00	3.11	1.27	0.13	56.00	3.21	1.34	0.00				
22.00	3.15	1.30	0.12	57.00	3.21	1.34	0.00				
23.00	3.18	1.32	0.10	58.00	3.21	1.34	0.00				
24.00	3.21	1.34	0.09	59.00	3.21	1.34	0.00				
25.00	3.21	1.34	0.00	60.00	3.21	1.34	0.00				
26.00	3.21	1.34	0.00	61.00	3.21	1.34	0.00				
27.00	3.21	1.34	0.00	62.00	3.21	1.34	0.00				
28.00	3.21	1.34	0.00	63.00	3.21	1.34	0.00				
29.00	3.21	1.34	0.00	64.00	3.21	1.34	0.00				
30.00	3.21	1.34	0.00	65.00	3.21	1.34	0.00				
31.00	3.21	1.34	0.00	66.00	3.21	1.34	0.00				
32.00	3.21	1.34	0.00	67.00	3.21	1.34	0.00				
33.00	3.21	1.34	0.00	68.00	3.21	1.34	0.00				
34.00	3.21	1.34	0.00	69.00	3.21	1.34	0.00				
35.00	3.21	1.34	0.00	70.00	3.21	1.34	0.00				

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**Summary for Subcatchment 3S: Off-Site East**

Runoff = 0.50 cfs @ 12.10 hrs, Volume= 0.038 af, Depth= 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 2 Year Rainfall=3.21"

Area (sf)	CN	Description
11,216	70	Woods, Good, HSG C
10,271	74	>75% Grass cover, Good, HSG C
21,487	72	Weighted Average
21,487		100.00% Pervious Area

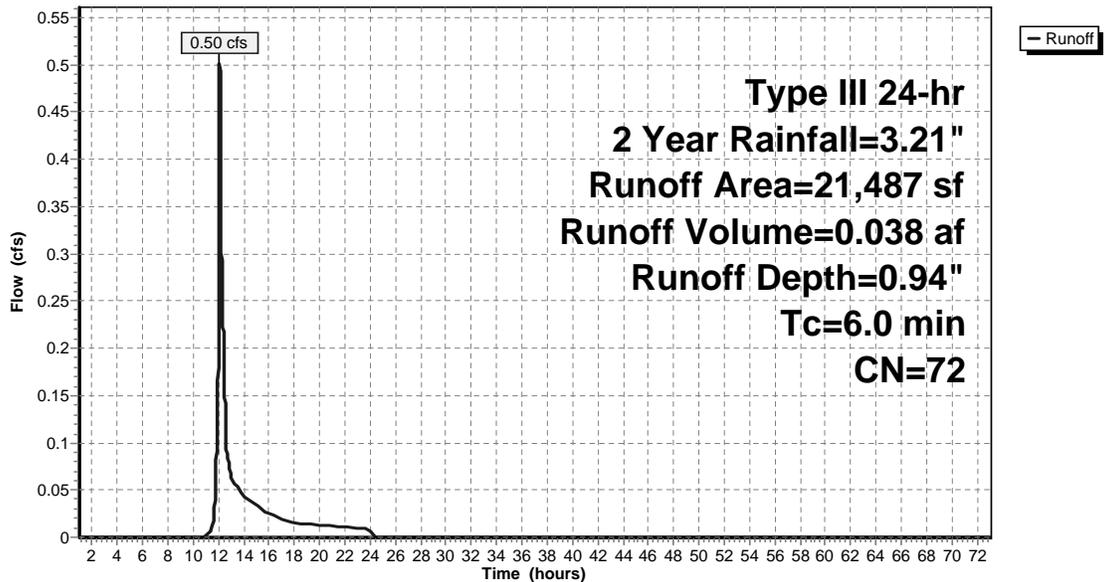
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

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**Subcatchment 3S: Off-Site East**

**Hydrograph**



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**Hydrograph for Subcatchment 3S: Off-Site East**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.03	0.00	0.00	36.00	3.21	0.94	0.00	71.00	3.21	0.94	0.00
2.00	0.06	0.00	0.00	37.00	3.21	0.94	0.00	72.00	3.21	0.94	0.00
3.00	0.10	0.00	0.00	38.00	3.21	0.94	0.00	73.00	3.21	0.94	0.00
4.00	0.14	0.00	0.00	39.00	3.21	0.94	0.00				
5.00	0.18	0.00	0.00	40.00	3.21	0.94	0.00				
6.00	0.23	0.00	0.00	41.00	3.21	0.94	0.00				
7.00	0.29	0.00	0.00	42.00	3.21	0.94	0.00				
8.00	0.37	0.00	0.00	43.00	3.21	0.94	0.00				
9.00	0.47	0.00	0.00	44.00	3.21	0.94	0.00				
10.00	0.61	0.00	0.00	45.00	3.21	0.94	0.00				
11.00	0.80	0.00	0.00	46.00	3.21	0.94	0.00				
12.00	1.60	0.15	0.25	47.00	3.21	0.94	0.00				
13.00	2.41	0.48	0.06	48.00	3.21	0.94	0.00				
14.00	2.60	0.58	0.04	49.00	3.21	0.94	0.00				
15.00	2.74	0.66	0.03	50.00	3.21	0.94	0.00				
16.00	2.84	0.72	0.02	51.00	3.21	0.94	0.00				
17.00	2.92	0.76	0.02	52.00	3.21	0.94	0.00				
18.00	2.98	0.80	0.02	53.00	3.21	0.94	0.00				
19.00	3.03	0.82	0.01	54.00	3.21	0.94	0.00				
20.00	3.07	0.85	0.01	55.00	3.21	0.94	0.00				
21.00	3.11	0.88	0.01	56.00	3.21	0.94	0.00				
22.00	3.15	0.90	0.01	57.00	3.21	0.94	0.00				
23.00	3.18	0.92	0.01	58.00	3.21	0.94	0.00				
24.00	3.21	0.94	0.01	59.00	3.21	0.94	0.00				
25.00	3.21	0.94	0.00	60.00	3.21	0.94	0.00				
26.00	3.21	0.94	0.00	61.00	3.21	0.94	0.00				
27.00	3.21	0.94	0.00	62.00	3.21	0.94	0.00				
28.00	3.21	0.94	0.00	63.00	3.21	0.94	0.00				
29.00	3.21	0.94	0.00	64.00	3.21	0.94	0.00				
30.00	3.21	0.94	0.00	65.00	3.21	0.94	0.00				
31.00	3.21	0.94	0.00	66.00	3.21	0.94	0.00				
32.00	3.21	0.94	0.00	67.00	3.21	0.94	0.00				
33.00	3.21	0.94	0.00	68.00	3.21	0.94	0.00				
34.00	3.21	0.94	0.00	69.00	3.21	0.94	0.00				
35.00	3.21	0.94	0.00	70.00	3.21	0.94	0.00				

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**Summary for Subcatchment 3Sa: Off-Site East**

Runoff = 3.31 cfs @ 12.12 hrs, Volume= 0.258 af, Depth= 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 2 Year Rainfall=3.21"

Area (sf)	CN	Description
53,364	74	>75% Grass cover, Good, HSG C
26,882	98	Water Surface, HSG C
* 3,160	96	Gravel Road
83,406	83	Weighted Average
56,524		67.77% Pervious Area
26,882		32.23% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	50	0.0280	0.16		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.00"
0.4	82	0.0316	3.61		<b>Shallow Concentrated Flow, Shallow Conc. Flow</b> Paved Kv= 20.3 fps
3.1	234	0.0317	1.25		<b>Shallow Concentrated Flow, Shallow Conc Flow</b> Short Grass Pasture Kv= 7.0 fps
8.6	366	Total			

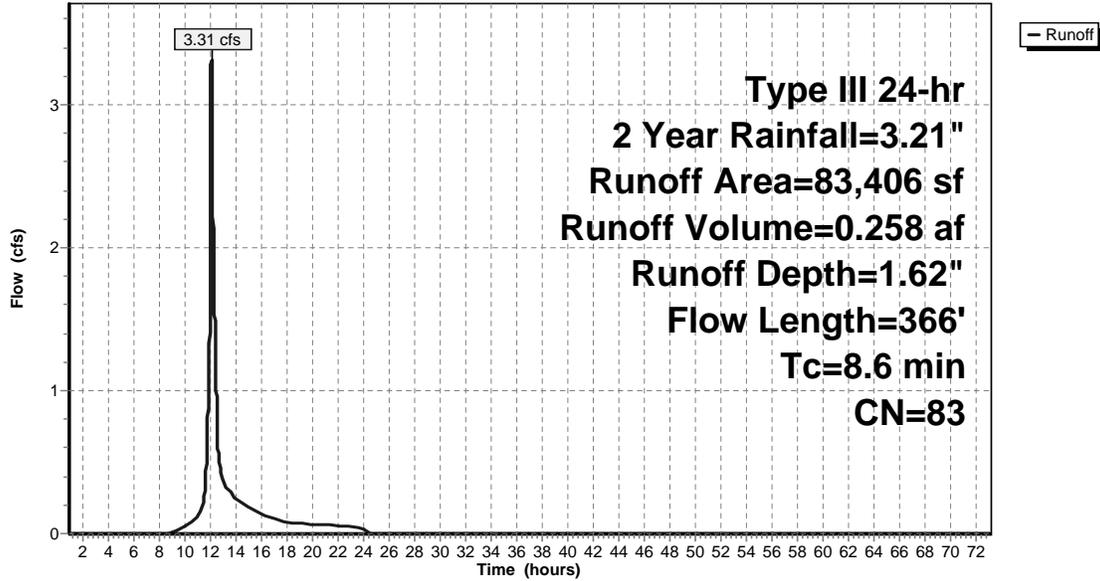
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Subcatchment 3Sa: Off-Site East

Hydrograph



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Hydrograph for Subcatchment 3Sa: Off-Site East

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.03	0.00	0.00	36.00	3.21	1.62	0.00	71.00	3.21	1.62	0.00
2.00	0.06	0.00	0.00	37.00	3.21	1.62	0.00	72.00	3.21	1.62	0.00
3.00	0.10	0.00	0.00	38.00	3.21	1.62	0.00	73.00	3.21	1.62	0.00
4.00	0.14	0.00	0.00	39.00	3.21	1.62	0.00				
5.00	0.18	0.00	0.00	40.00	3.21	1.62	0.00				
6.00	0.23	0.00	0.00	41.00	3.21	1.62	0.00				
7.00	0.29	0.00	0.00	42.00	3.21	1.62	0.00				
8.00	0.37	0.00	0.00	43.00	3.21	1.62	0.00				
9.00	0.47	0.00	0.01	44.00	3.21	1.62	0.00				
10.00	0.61	0.02	0.04	45.00	3.21	1.62	0.00				
11.00	0.80	0.06	0.12	46.00	3.21	1.62	0.00				
12.00	1.60	0.44	1.61	47.00	3.21	1.62	0.00				
13.00	2.41	0.99	0.39	48.00	3.21	1.62	0.00				
14.00	2.60	1.13	0.25	49.00	3.21	1.62	0.00				
15.00	2.74	1.24	0.19	50.00	3.21	1.62	0.00				
16.00	2.84	1.32	0.13	51.00	3.21	1.62	0.00				
17.00	2.92	1.38	0.11	52.00	3.21	1.62	0.00				
18.00	2.98	1.43	0.08	53.00	3.21	1.62	0.00				
19.00	3.03	1.47	0.07	54.00	3.21	1.62	0.00				
20.00	3.07	1.50	0.07	55.00	3.21	1.62	0.00				
21.00	3.11	1.54	0.06	56.00	3.21	1.62	0.00				
22.00	3.15	1.57	0.06	57.00	3.21	1.62	0.00				
23.00	3.18	1.59	0.05	58.00	3.21	1.62	0.00				
24.00	3.21	1.62	0.04	59.00	3.21	1.62	0.00				
25.00	3.21	1.62	0.00	60.00	3.21	1.62	0.00				
26.00	3.21	1.62	0.00	61.00	3.21	1.62	0.00				
27.00	3.21	1.62	0.00	62.00	3.21	1.62	0.00				
28.00	3.21	1.62	0.00	63.00	3.21	1.62	0.00				
29.00	3.21	1.62	0.00	64.00	3.21	1.62	0.00				
30.00	3.21	1.62	0.00	65.00	3.21	1.62	0.00				
31.00	3.21	1.62	0.00	66.00	3.21	1.62	0.00				
32.00	3.21	1.62	0.00	67.00	3.21	1.62	0.00				
33.00	3.21	1.62	0.00	68.00	3.21	1.62	0.00				
34.00	3.21	1.62	0.00	69.00	3.21	1.62	0.00				
35.00	3.21	1.62	0.00	70.00	3.21	1.62	0.00				

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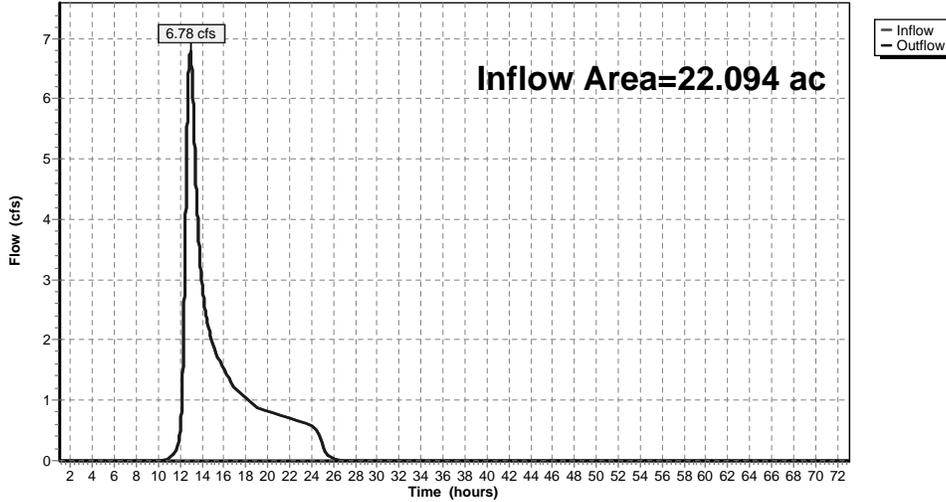
**Summary for Reach DP-1: (new Reach)**

Inflow Area = 22.094 ac, 3.96% Impervious, Inflow Depth = 0.91" for 2 Year event  
 Inflow = 6.78 cfs @ 12.95 hrs, Volume= 1.681 af  
 Outflow = 6.78 cfs @ 12.95 hrs, Volume= 1.681 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-1: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-1: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.00		0.00	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.00		0.00	42.00	0.00		0.00				
8.00	0.00		0.00	43.00	0.00		0.00				
9.00	0.00		0.00	44.00	0.00		0.00				
10.00	0.00		0.00	45.00	0.00		0.00				
11.00	0.04		0.04	46.00	0.00		0.00				
12.00	<b>0.53</b>		<b>0.53</b>	47.00	0.00		0.00				
13.00	<b>6.68</b>		<b>6.68</b>	48.00	0.00		0.00				
14.00	2.92		2.92	49.00	0.00		0.00				
15.00	1.92		1.92	50.00	0.00		0.00				
16.00	1.51		1.51	51.00	0.00		0.00				
17.00	1.21		1.21	52.00	0.00		0.00				
18.00	1.03		1.03	53.00	0.00		0.00				
19.00	0.89		0.89	54.00	0.00		0.00				
20.00	0.82		0.82	55.00	0.00		0.00				
21.00	0.76		0.76	56.00	0.00		0.00				
22.00	0.71		0.71	57.00	0.00		0.00				
23.00	0.65		0.65	58.00	0.00		0.00				
24.00	0.59		0.59	59.00	0.00		0.00				
25.00	0.25		0.25	60.00	0.00		0.00				
26.00	0.03		0.03	61.00	0.00		0.00				
27.00	0.00		0.00	62.00	0.00		0.00				
28.00	0.00		0.00	63.00	0.00		0.00				
29.00	0.00		0.00	64.00	0.00		0.00				
30.00	0.00		0.00	65.00	0.00		0.00				
31.00	0.00		0.00	66.00	0.00		0.00				
32.00	0.00		0.00	67.00	0.00		0.00				
33.00	0.00		0.00	68.00	0.00		0.00				
34.00	0.00		0.00	69.00	0.00		0.00				
35.00	0.00		0.00	70.00	0.00		0.00				

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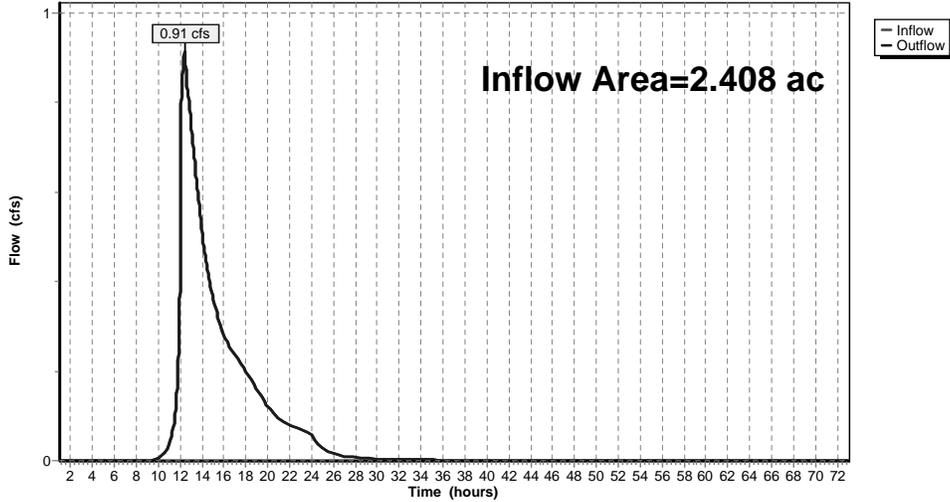
**Summary for Reach DP-3: (new Reach)**

Inflow Area = 2.408 ac, 25.63% Impervious, Inflow Depth = 1.48" for 2 Year event  
 Inflow = 0.91 cfs @ 12.38 hrs, Volume= 0.297 af  
 Outflow = 0.91 cfs @ 12.38 hrs, Volume= 0.297 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-3: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-3: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.00		0.00	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.00		0.00	42.00	0.00		0.00				
8.00	0.00		0.00	43.00	0.00		0.00				
9.00	0.00		0.00	44.00	0.00		0.00				
10.00	0.00		0.00	45.00	0.00		0.00				
11.00	0.04		0.04	46.00	0.00		0.00				
12.00	<b>0.46</b>		<b>0.46</b>	47.00	0.00		0.00				
13.00	<b>0.75</b>		<b>0.75</b>	48.00	0.00		0.00				
14.00	0.51		0.51	49.00	0.00		0.00				
15.00	0.36		0.36	50.00	0.00		0.00				
16.00	0.28		0.28	51.00	0.00		0.00				
17.00	0.24		0.24	52.00	0.00		0.00				
18.00	0.20		0.20	53.00	0.00		0.00				
19.00	0.16		0.16	54.00	0.00		0.00				
20.00	0.12		0.12	55.00	0.00		0.00				
21.00	0.10		0.10	56.00	0.00		0.00				
22.00	0.08		0.08	57.00	0.00		0.00				
23.00	0.07		0.07	58.00	0.00		0.00				
24.00	0.06		0.06	59.00	0.00		0.00				
25.00	0.03		0.03	60.00	0.00		0.00				
26.00	0.02		0.02	61.00	0.00		0.00				
27.00	0.01		0.01	62.00	0.00		0.00				
28.00	0.01		0.01	63.00	0.00		0.00				
29.00	0.00		0.00	64.00	0.00		0.00				
30.00	0.00		0.00	65.00	0.00		0.00				
31.00	0.00		0.00	66.00	0.00		0.00				
32.00	0.00		0.00	67.00	0.00		0.00				
33.00	0.00		0.00	68.00	0.00		0.00				
34.00	0.00		0.00	69.00	0.00		0.00				
35.00	0.00		0.00	70.00	0.00		0.00				

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**Summary for Pond P1A: Pond 1a (Pond Repair)**

Inflow Area = 4.370 ac, 20.04% Impervious, Inflow Depth = 1.34" for 2 Year event  
 Inflow = 5.43 cfs @ 12.18 hrs, Volume= 0.490 af  
 Outflow = 0.53 cfs @ 13.92 hrs, Volume= 0.490 af, Atten= 90%, Lag= 104.0 min  
 Discarded = 0.16 cfs @ 13.92 hrs, Volume= 0.114 af  
 Primary = 0.38 cfs @ 13.92 hrs, Volume= 0.375 af  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 77.57' @ 13.92 hrs Surf.Area= 14,738 sf Storage= 9,773 cf

Plug-Flow detention time= 214.3 min calculated for 0.489 af (100% of inflow)  
 Center-of-Mass det. time= 214.3 min ( 1,066.4 - 852.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	75.50'	1,242 cf	<b>Custom Stage Data (Irregular)</b> Listed below 3,106 cf Overall x 40.0% Voids
#2	76.50'	37,823 cf	<b>Custom Stage Data (Irregular)</b> Listed below 39,065 cf Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
75.50	3,106	220.0	0	0	3,106
76.00	3,106	220.0	1,553	1,553	3,216
76.50	3,106	220.0	1,553	3,106	3,326

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.50	3,106	220.0	0	0	3,106
77.00	6,731	331.0	2,402	2,402	7,975
78.00	15,313	639.8	10,732	13,134	31,836
79.20	26,330	782.0	24,689	37,823	47,947

**1817-Basin Repair 2024**

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Device	Routing	Invert	Outlet Devices
#1	Secondary	78.70'	<b>14.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	75.50'	<b>0.270 in/hr Exfiltration over Wetted area</b>
#3	Primary	75.50'	<b>4.0" Round Culvert</b> L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 75.50' / 75.10' S= 0.0100 ' S= 0.0100 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.16 cfs @ 13.92 hrs HW=77.57' (Free Discharge)  
 ↳ **2=Exfiltration** (Exfiltration Controls 0.16 cfs)

**Primary OutFlow** Max=0.38 cfs @ 13.92 hrs HW=77.57' (Free Discharge)  
 ↳ **3=Culvert** (Barrel Controls 0.38 cfs @ 4.33 fps)

**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=75.50' (Free Discharge)  
 ↳ **1=Broad-Crested Rectangular Weir** ( Controls 0.00 cfs)

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Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

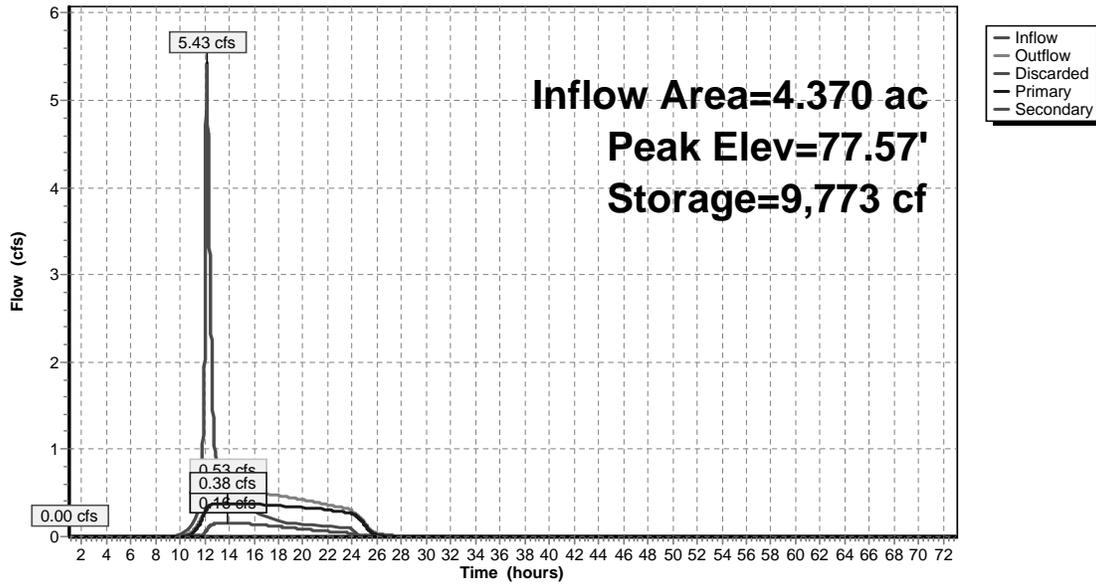
Type III 24-hr 2 Year Rainfall=3.21"

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Pond P1A: Pond 1a (Pond Repair)

Hydrograph



1817-Basin Repair 2024

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Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

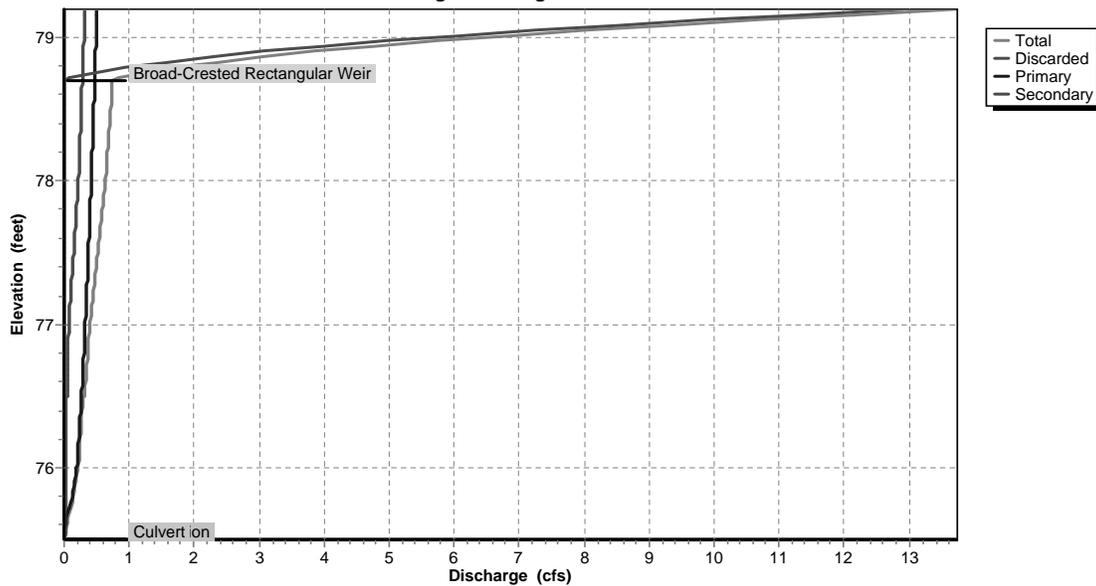
Type III 24-hr 2 Year Rainfall=3.21"

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Pond P1A: Pond 1a (Pond Repair)

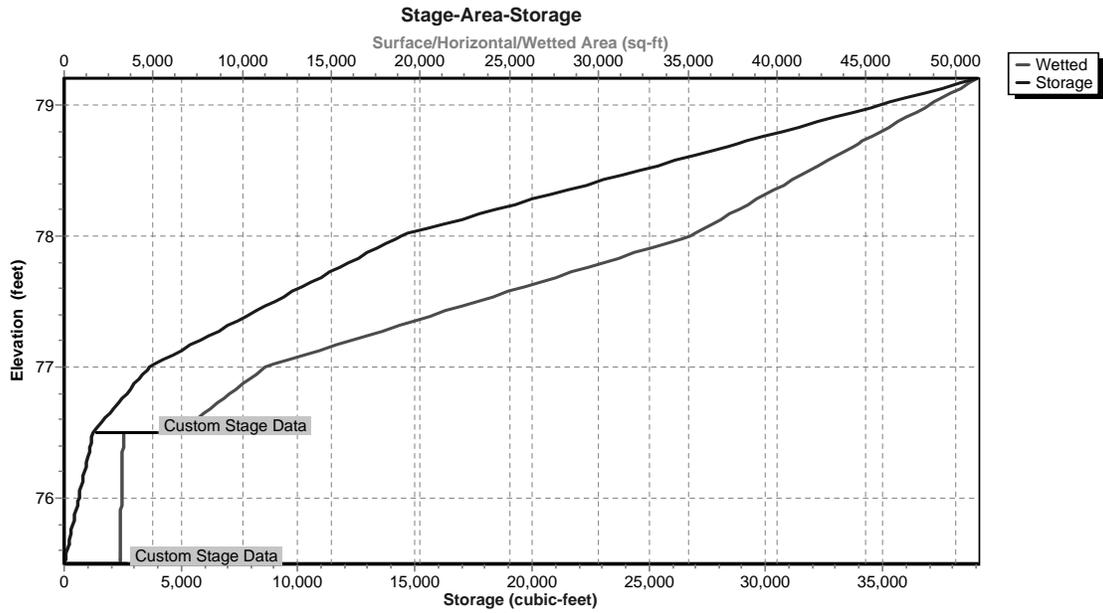
Stage-Discharge



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**Pond P1A: Pond 1a (Pond Repair)**



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**Hydrograph for Pond P1A: Pond 1a (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
1.00	0.00	0	75.50	0.00	0.00	0.00	0.00
6.00	0.00	0	75.50	0.00	0.00	0.00	0.00
11.00	0.15	186	75.65	0.06	0.02	0.04	0.00
16.00	0.28	8,815	77.48	0.51	0.14	0.37	0.00
21.00	0.13	3,797	77.01	0.40	0.07	0.33	0.00
26.00	0.00	126	75.60	0.04	0.02	0.02	0.00
31.00	0.00	0	75.50	0.00	0.00	0.00	0.00
36.00	0.00	0	75.50	0.00	0.00	0.00	0.00
41.00	0.00	0	75.50	0.00	0.00	0.00	0.00
46.00	0.00	0	75.50	0.00	0.00	0.00	0.00
51.00	0.00	0	75.50	0.00	0.00	0.00	0.00
56.00	0.00	0	75.50	0.00	0.00	0.00	0.00
61.00	0.00	0	75.50	0.00	0.00	0.00	0.00
66.00	0.00	0	75.50	0.00	0.00	0.00	0.00
71.00	0.00	0	75.50	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
75.50	0.00	0.00	0.00	0.00	79.00	6.41	0.30	0.49	5.61
75.60	0.04	0.02	0.02	0.00	79.10	9.70	0.31	0.50	8.89
75.70	0.09	0.02	0.07	0.00	79.20	<b>13.72</b>	<b>0.32</b>	<b>0.50</b>	<b>12.89</b>
75.80	0.14	0.02	0.12	0.00					
75.90	0.18	0.02	0.16	0.00					
76.00	0.21	0.02	0.19	0.00					
76.10	0.23	0.02	0.21	0.00					
76.20	0.25	0.02	0.23	0.00					
76.30	0.26	0.02	0.24	0.00					
76.40	0.27	0.02	0.25	0.00					
76.50	0.31	0.04	0.27	0.00					
76.60	0.33	0.05	0.28	0.00					
76.70	0.34	0.05	0.29	0.00					
76.80	0.36	0.06	0.30	0.00					
76.90	0.38	0.06	0.31	0.00					
77.00	0.39	0.07	0.32	0.00					
77.10	0.42	0.09	0.33	0.00					
77.20	0.44	0.10	0.34	0.00					
77.30	0.47	0.12	0.35	0.00					
77.40	0.49	0.13	0.36	0.00					
77.50	0.52	0.15	0.37	0.00					
77.60	0.54	0.16	0.38	0.00					
77.70	0.56	0.18	0.39	0.00					
77.80	0.59	0.19	0.40	0.00					
77.90	0.61	0.20	0.41	0.00					
78.00	0.63	0.22	0.41	0.00					
78.10	0.65	0.23	0.42	0.00					
78.20	0.67	0.24	0.43	0.00					
78.30	0.68	0.24	0.44	0.00					
78.40	0.70	0.25	0.45	0.00					
78.50	0.71	0.26	0.45	0.00					
78.60	0.73	0.27	0.46	0.00					
78.70	0.75	0.28	0.47	0.00					
78.80	1.81	0.29	0.47	1.05					
78.90	3.74	0.30	0.48	2.97					

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**Stage-Area-Storage for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)
75.50	3,106	0	77.25	17,266	6,327	79.00	48,588	34,950
75.55	3,117	62	77.30	18,459	6,864	79.05	49,260	35,979
75.60	3,128	124	77.35	19,652	7,400	79.10	49,931	37,008
75.65	3,139	186	77.40	20,845	7,937	79.15	50,602	38,036
75.70	3,150	248	77.45	22,038	8,473	79.20	<b>51,273</b>	<b>39,065</b>
75.75	3,161	311	77.50	23,231	9,010			
75.80	3,172	373	77.55	24,424	9,547			
75.85	3,183	435	77.60	25,618	10,083			
75.90	3,194	497	77.65	26,811	10,620			
75.95	3,205	559	77.70	28,004	11,156			
76.00	3,216	621	77.75	29,197	11,693			
76.05	3,227	683	77.80	30,390	12,230			
76.10	3,238	745	77.85	31,583	12,766			
76.15	3,249	808	77.90	32,776	13,303			
76.20	3,260	870	77.95	33,969	13,839			
76.25	3,271	932	78.00	35,162	14,376			
76.30	3,282	994	78.05	35,833	15,405			
76.35	3,293	1,056	78.10	36,505	16,434			
76.40	3,304	1,118	78.15	37,176	17,462			
76.45	3,315	1,180	78.20	37,847	18,491			
76.50	6,432	1,242	78.25	38,518	19,520			
76.55	6,919	1,483	78.30	39,190	20,548			
76.60	7,406	1,723	78.35	39,861	21,577			
76.65	7,893	1,963	78.40	40,532	22,606			
76.70	8,380	2,203	78.45	41,204	23,634			
76.75	8,866	2,443	78.50	41,875	24,663			
76.80	9,353	2,683	78.55	42,546	25,692			
76.85	9,840	2,923	78.60	43,218	26,721			
76.90	10,327	3,164	78.65	43,889	27,749			
76.95	10,814	3,404	78.70	44,560	28,778			
77.00	11,301	3,644	78.75	45,232	29,807			
77.05	12,494	4,181	78.80	45,903	30,835			
77.10	13,687	4,717	78.85	46,574	31,864			
77.15	14,880	5,254	78.90	47,246	32,893			
77.20	16,073	5,790	78.95	47,917	33,922			

**1817-Basin Repair 2024**

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**Summary for Pond P3A: Pond 3A (Pond Repair)**

Inflow Area = 1.915 ac, 32.23% Impervious, Inflow Depth = 1.62" for 2 Year event  
 Inflow = 3.31 cfs @ 12.12 hrs, Volume= 0.258 af  
 Outflow = 0.74 cfs @ 12.58 hrs, Volume= 0.258 af, Atten= 78%, Lag= 27.4 min  
 Primary = 0.34 cfs @ 12.58 hrs, Volume= 0.200 af  
 Secondary = 0.40 cfs @ 12.58 hrs, Volume= 0.058 af  
 Tertiary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 77.03' @ 12.58 hrs Surf.Area= 6,943 sf Storage= 4,350 cf  
 Flood Elev= 79.50' Surf.Area= 25,484 sf Storage= 37,166 cf

Plug-Flow detention time= 113.3 min calculated for 0.258 af (100% of inflow)  
 Center-of-Mass det. time= 113.5 min ( 948.7 - 835.2 )

Volume	Invert	Avail.Storage	Storage Description		
#1	76.00'	37,166 cf	<b>Custom Stage Data (Irregular)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.00	2,053	339.0	0	0	2,053
77.00	6,709	559.0	4,158	4,158	17,781
78.00	17,458	791.4	11,663	15,821	42,764
79.00	25,484	883.5	21,345	37,166	55,068

Device	Routing	Invert	Outlet Devices
#1	Primary	76.00'	<b>4.0" Round 6" Culvert 1</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.00' / 75.52' S= 0.0240 ' S Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Secondary	76.55'	<b>6.0" Round 6" Culvert 2</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.55' / 75.60' S= 0.0475 ' S Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#3	Tertiary	78.50'	<b>20.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50

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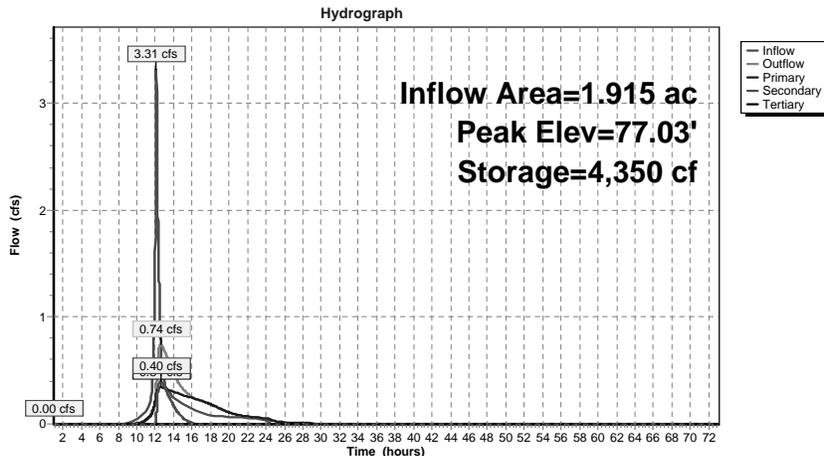
Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76  
 2.83

**Primary OutFlow** Max=0.34 cfs @ 12.58 hrs HW=77.03' (Free Discharge)  
 1-6" Culvert 1 (Inlet Controls 0.34 cfs @ 3.94 fps)

**Secondary OutFlow** Max=0.40 cfs @ 12.58 hrs HW=77.03' (Free Discharge)  
 2-6" Culvert 2 (Inlet Controls 0.40 cfs @ 2.08 fps)

**Tertiary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=76.00' (Free Discharge)  
 3-Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Pond P3A: Pond 3A (Pond Repair)**



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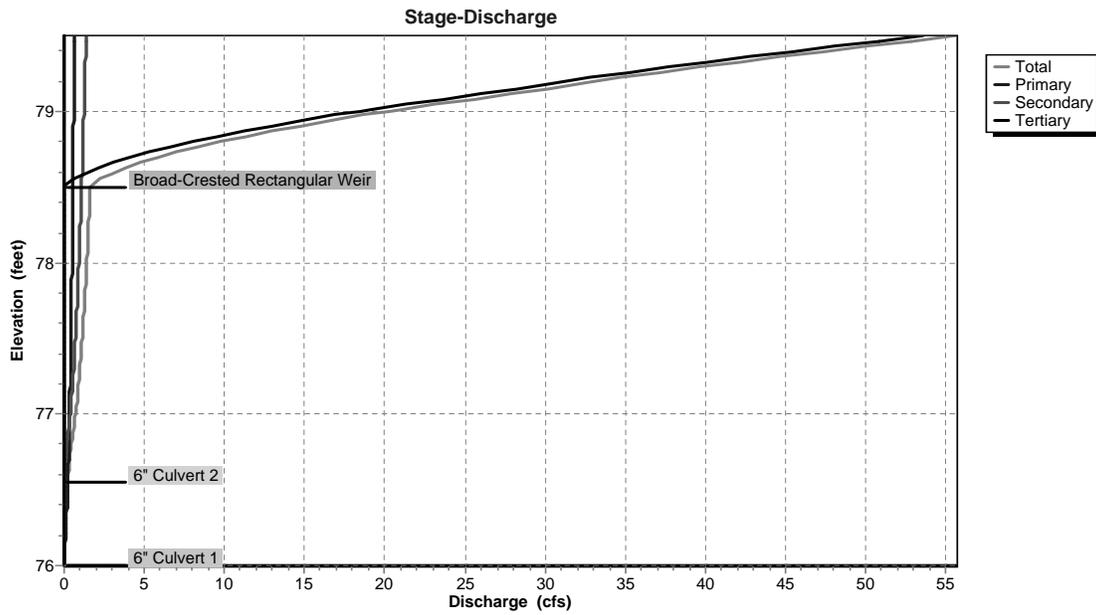
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 2 Year Rainfall=3.21"

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Pond P3A: Pond 3A (Pond Repair)



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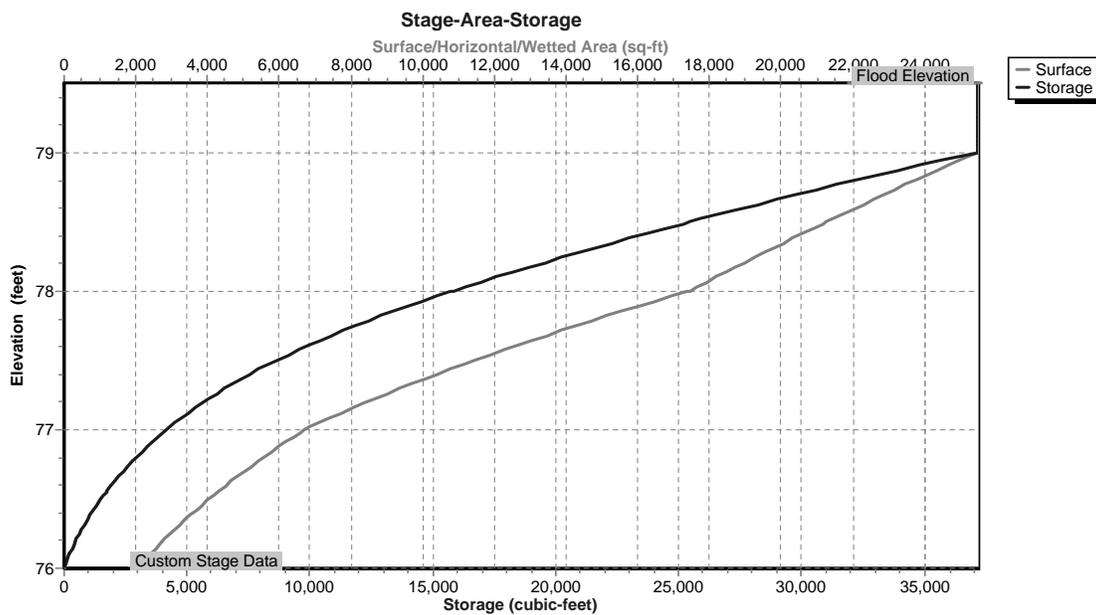
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 2 Year Rainfall=3.21"

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Pond P3A: Pond 3A (Pond Repair)



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**Hydrograph for Pond P3A: Pond 3A (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
1.00	0.00	0	76.00	0.00	0.00	0.00	0.00
6.00	0.00	0	76.00	0.00	0.00	0.00	0.00
11.00	0.12	312	76.14	0.04	0.04	0.00	0.00
16.00	0.13	1,952	76.61	0.25	0.25	0.01	0.00
21.00	0.06	525	76.22	0.08	0.08	0.00	0.00
26.00	0.00	186	76.08	0.02	0.02	0.00	0.00
31.00	0.00	69	76.03	0.00	0.00	0.00	0.00
36.00	0.00	35	76.02	0.00	0.00	0.00	0.00
41.00	0.00	18	76.01	0.00	0.00	0.00	0.00
46.00	0.00	9	76.00	0.00	0.00	0.00	0.00
51.00	0.00	5	76.00	0.00	0.00	0.00	0.00
56.00	0.00	2	76.00	0.00	0.00	0.00	0.00
61.00	0.00	1	76.00	0.00	0.00	0.00	0.00
66.00	0.00	1	76.00	0.00	0.00	0.00	0.00
71.00	0.00	0	76.00	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
76.00	0.00	0.00	0.00	0.00	79.50	55.61	0.64	1.37	53.60
76.10	0.02	0.02	0.00	0.00					
76.20	0.07	0.07	0.00	0.00					
76.30	0.14	0.14	0.00	0.00					
76.40	0.18	0.18	0.00	0.00					
76.50	0.21	0.21	0.00	0.00					
76.60	0.25	0.24	0.01	0.00					
76.70	0.33	0.27	0.06	0.00					
76.80	0.44	0.30	0.15	0.00					
76.90	0.58	0.32	0.26	0.00					
77.00	0.71	0.34	0.38	0.00					
77.10	0.82	0.36	0.46	0.00					
77.20	0.90	0.38	0.53	0.00					
77.30	0.98	0.39	0.59	0.00					
77.40	1.06	0.41	0.65	0.00					
77.50	1.13	0.43	0.70	0.00					
77.60	1.19	0.44	0.75	0.00					
77.70	1.24	0.45	0.79	0.00					
77.80	1.30	0.46	0.83	0.00					
77.90	1.35	0.48	0.87	0.00					
78.00	1.40	0.49	0.91	0.00					
78.10	1.45	0.50	0.95	0.00					
78.20	1.50	0.51	0.99	0.00					
78.30	1.54	0.52	1.02	0.00					
78.40	1.59	0.53	1.06	0.00					
78.50	1.63	0.54	1.09	0.00					
78.60	3.17	0.55	1.12	1.50					
78.70	5.95	0.56	1.15	4.24					
78.80	9.77	0.57	1.18	8.02					
78.90	14.49	0.58	1.21	12.70					
79.00	20.25	0.59	1.24	18.42					
79.10	26.96	0.60	1.27	25.10					
79.20	33.41	0.61	1.29	31.51					
79.30	40.29	0.62	1.32	38.35					
79.40	47.74	0.63	1.35	45.76					

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**Stage-Area-Storage for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
76.00	2,053	0	77.75	14,298	11,858	79.50	25,484	37,166
76.05	2,222	107	77.80	14,905	12,588			
76.10	2,398	222	77.85	15,524	13,349			
76.15	2,581	347	77.90	16,156	14,141			
76.20	2,770	481	77.95	16,801	14,964			
76.25	2,966	624	78.00	17,458	15,821			
76.30	3,169	777	78.05	17,823	16,703			
76.35	3,378	941	78.10	18,192	17,603			
76.40	3,594	1,115	78.15	18,565	18,522			
76.45	3,817	1,300	78.20	18,942	19,460			
76.50	4,046	1,497	78.25	19,323	20,417			
76.55	4,282	1,705	78.30	19,707	21,392			
76.60	4,525	1,925	78.35	20,095	22,387			
76.65	4,775	2,158	78.40	20,487	23,402			
76.70	5,031	2,403	78.45	20,882	24,436			
76.75	5,294	2,661	78.50	21,282	25,490			
76.80	5,563	2,932	78.55	21,685	26,564			
76.85	5,840	3,217	78.60	22,092	27,659			
76.90	6,123	3,516	78.65	22,503	28,774			
76.95	6,413	3,830	78.70	22,917	29,909			
77.00	6,709	4,158	78.75	23,336	31,065			
77.05	7,127	4,504	78.80	23,758	32,243			
77.10	7,557	4,871	78.85	24,184	33,441			
77.15	8,000	5,259	78.90	24,613	34,661			
77.20	8,455	5,671	78.95	25,047	35,903			
77.25	8,923	6,105	79.00	<b>25,484</b>	<b>37,166</b>			
77.30	9,404	6,563	79.05	25,484	37,166			
77.35	9,897	7,046	79.10	25,484	37,166			
77.40	10,403	7,553	79.15	25,484	37,166			
77.45	10,922	8,086	79.20	25,484	37,166			
77.50	11,453	8,646	79.25	25,484	37,166			
77.55	11,997	9,232	79.30	25,484	37,166			
77.60	12,553	9,846	79.35	25,484	37,166			
77.65	13,122	10,487	79.40	25,484	37,166			
77.70	13,704	11,158	79.45	25,484	37,166			

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Time span=1.00-73.00 hrs, dt=0.01 hrs, 7201 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment 1S: Off-Site Northeast**

Runoff Area=772,071 sf 0.00% Impervious Runoff Depth=2.25"  
 Flow Length=1,645' Tc=61.7 min CN=71 Runoff=17.81 cfs 3.328 af

**Subcatchment 1Sa: Off-Site**

Runoff Area=190,352 sf 20.04% Impervious Runoff Depth=2.96"  
 Flow Length=540' Tc=12.8 min CN=79 Runoff=12.16 cfs 1.077 af

**Subcatchment 3S: Off-Site East**

Runoff Area=21,487 sf 0.00% Impervious Runoff Depth=2.34"  
 Tc=6.0 min CN=72 Runoff=1.34 cfs 0.096 af

**Subcatchment 3Sa: Off-Site East**

Runoff Area=83,406 sf 32.23% Impervious Runoff Depth=3.34"  
 Flow Length=366' Tc=8.6 min CN=83 Runoff=6.82 cfs 0.533 af

**Reach DP-1: (new Reach)**

Inflow=18.26 cfs 4.066 af  
 Outflow=18.26 cfs 4.066 af

**Reach DP-3: (new Reach)**

Inflow=2.20 cfs 0.629 af  
 Outflow=2.20 cfs 0.629 af

**Pond P1A: Pond 1a (Pond Repair)**

Peak Elev=78.58' Storage=26,263 cf Inflow=12.16 cfs 1.077 af  
 Discarded=0.27 cfs 0.340 af Primary=0.46 cfs 0.737 af Secondary=0.00 cfs 0.000 af Outflow=0.73 cfs 1.077 af

**Pond P3A: Pond 3A (Pond Repair)**

Peak Elev=77.59' Storage=9,691 cf Inflow=6.82 cfs 0.533 af  
 Primary=0.44 cfs 0.316 af Secondary=0.74 cfs 0.217 af Tertiary=0.00 cfs 0.000 af Outflow=1.18 cfs 0.533 af

**Total Runoff Area = 24.502 ac Runoff Volume = 5.034 af Average Runoff Depth = 2.47"**  
**93.91% Pervious = 23.009 ac 6.09% Impervious = 1.493 ac**

**1817-Basin Repair 2024**

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**Summary for Subcatchment 1S: Off-Site Northeast**

Runoff = 17.81 cfs @ 12.83 hrs, Volume= 3.328 af, Depth= 2.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10 Year Rainfall=5.18"

Area (sf)	CN	Description
650,962	70	Woods, Good, HSG C
115,309	74	>75% Grass cover, Good, HSG C
* 5,800	96	Gravel Road, HSG C
772,071	71	Weighted Average
772,071		100.00% Pervious Area

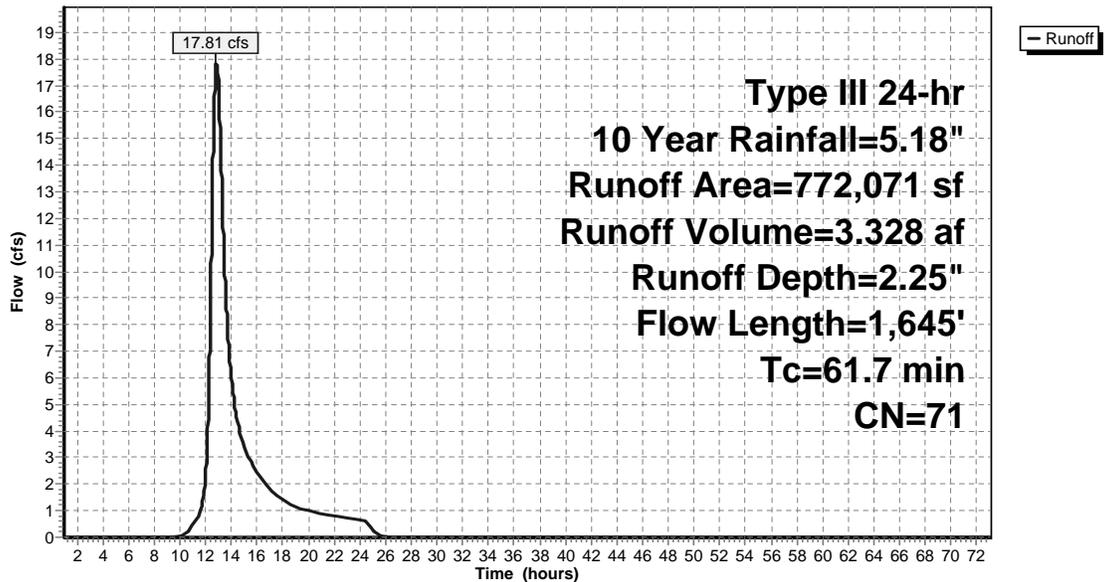
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.0	50	0.0080	0.03		<b>Sheet Flow,</b> Woods: Dense underbrush n= 0.800 P2= 3.00"
12.6	628	0.0276	0.83		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
3.3	496	0.0276	2.49		<b>Shallow Concentrated Flow,</b> Grassed Waterway Kv= 15.0 fps
13.8	471	0.0130	0.57		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
61.7	1,645	Total			

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**Subcatchment 1S: Off-Site Northeast**

**Hydrograph**



**1817-Basin Repair 2024**

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**Hydrograph for Subcatchment 1S: Off-Site Northeast**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.05	0.00	0.00	36.00	5.18	2.25	0.00	71.00	5.18	2.25	0.00
2.00	0.10	0.00	0.00	37.00	5.18	2.25	0.00	72.00	5.18	2.25	0.00
3.00	0.16	0.00	0.00	38.00	5.18	2.25	0.00	73.00	5.18	2.25	0.00
4.00	0.22	0.00	0.00	39.00	5.18	2.25	0.00				
5.00	0.29	0.00	0.00	40.00	5.18	2.25	0.00				
6.00	0.37	0.00	0.00	41.00	5.18	2.25	0.00				
7.00	0.47	0.00	0.00	42.00	5.18	2.25	0.00				
8.00	0.59	0.00	0.00	43.00	5.18	2.25	0.00				
9.00	0.75	0.00	0.00	44.00	5.18	2.25	0.00				
10.00	0.98	0.01	0.02	45.00	5.18	2.25	0.00				
11.00	1.30	0.05	0.44	46.00	5.18	2.25	0.00				
12.00	2.59	0.54	<b>2.24</b>	47.00	5.18	2.25	0.00				
13.00	3.88	1.32	<b>17.06</b>	48.00	5.18	2.25	0.00				
14.00	4.20	1.53	6.00	49.00	5.18	2.25	0.00				
15.00	4.43	1.69	3.41	50.00	5.18	2.25	0.00				
16.00	4.59	1.81	2.47	51.00	5.18	2.25	0.00				
17.00	4.71	1.90	1.81	52.00	5.18	2.25	0.00				
18.00	4.81	1.97	1.42	53.00	5.18	2.25	0.00				
19.00	4.89	2.03	1.14	54.00	5.18	2.25	0.00				
20.00	4.96	2.08	1.00	55.00	5.18	2.25	0.00				
21.00	5.02	2.13	0.91	56.00	5.18	2.25	0.00				
22.00	5.08	2.18	0.83	57.00	5.18	2.25	0.00				
23.00	5.13	2.22	0.75	58.00	5.18	2.25	0.00				
24.00	<b>5.18</b>	<b>2.25</b>	0.68	59.00	5.18	2.25	0.00				
25.00	5.18	2.25	0.24	60.00	5.18	2.25	0.00				
26.00	5.18	2.25	0.02	61.00	5.18	2.25	0.00				
27.00	5.18	2.25	0.00	62.00	5.18	2.25	0.00				
28.00	5.18	2.25	0.00	63.00	5.18	2.25	0.00				
29.00	5.18	2.25	0.00	64.00	5.18	2.25	0.00				
30.00	5.18	2.25	0.00	65.00	5.18	2.25	0.00				
31.00	5.18	2.25	0.00	66.00	5.18	2.25	0.00				
32.00	5.18	2.25	0.00	67.00	5.18	2.25	0.00				
33.00	5.18	2.25	0.00	68.00	5.18	2.25	0.00				
34.00	5.18	2.25	0.00	69.00	5.18	2.25	0.00				
35.00	5.18	2.25	0.00	70.00	5.18	2.25	0.00				

**1817-Basin Repair 2024**

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**Summary for Subcatchment 1Sa: Off-Site**

Runoff = 12.16 cfs @ 12.18 hrs, Volume= 1.077 af, Depth= 2.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10 Year Rainfall=5.18"

Area (sf)	CN	Description
152,204	74	>75% Grass cover, Good, HSG C
* 9,937	98	Gravel Road, HSG C
27,571	98	Water Surface, HSG C
* 640	98	Equipment Pad, HSG C
190,352	79	Weighted Average
152,204		79.96% Pervious Area
38,148		20.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	50	0.0380	0.19		<b>Sheet Flow,</b> Grass: Short n=0.150 P2= 3.00"
8.3	490	0.0196	0.98		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
12.8	540	Total			

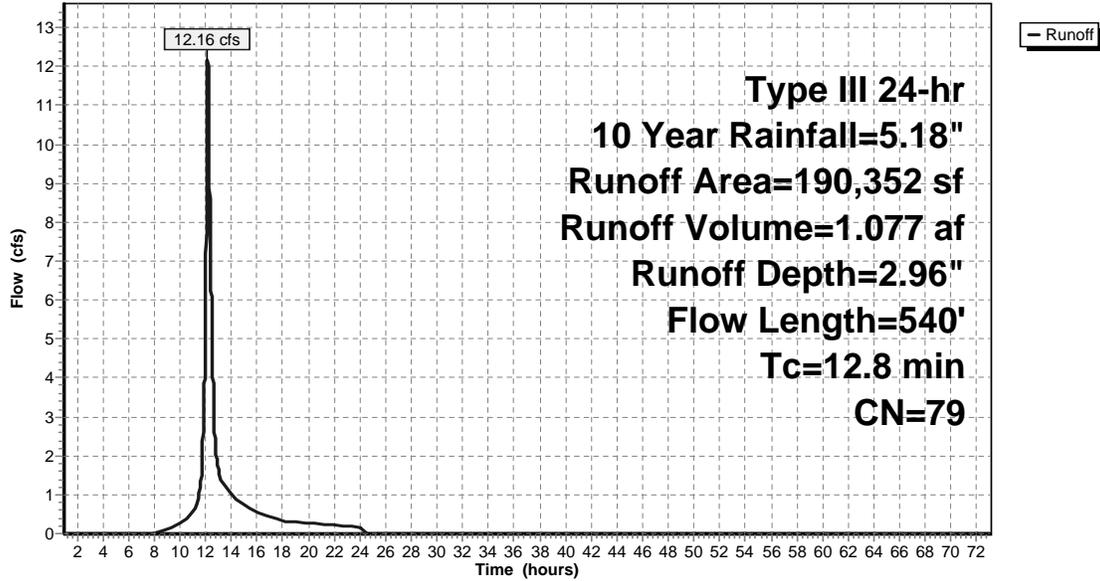
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Subcatchment 1Sa: Off-Site

Hydrograph



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Hydrograph for Subcatchment 1Sa: Off-Site

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.05	0.00	0.00	36.00	5.18	2.96	0.00	71.00	5.18	2.96	0.00
2.00	0.10	0.00	0.00	37.00	5.18	2.96	0.00	72.00	5.18	2.96	0.00
3.00	0.16	0.00	0.00	38.00	5.18	2.96	0.00	73.00	5.18	2.96	0.00
4.00	0.22	0.00	0.00	39.00	5.18	2.96	0.00				
5.00	0.29	0.00	0.00	40.00	5.18	2.96	0.00				
6.00	0.37	0.00	0.00	41.00	5.18	2.96	0.00				
7.00	0.47	0.00	0.00	42.00	5.18	2.96	0.00				
8.00	0.59	0.00	0.01	43.00	5.18	2.96	0.00				
9.00	0.75	0.02	0.10	44.00	5.18	2.96	0.00				
10.00	0.98	0.06	0.26	45.00	5.18	2.96	0.00				
11.00	1.30	0.17	0.58	46.00	5.18	2.96	0.00				
12.00	2.59	0.90	5.37	47.00	5.18	2.96	0.00				
13.00	3.88	1.87	1.67	48.00	5.18	2.96	0.00				
14.00	4.20	2.13	1.01	49.00	5.18	2.96	0.00				
15.00	4.43	2.31	0.76	50.00	5.18	2.96	0.00				
16.00	4.59	2.45	0.54	51.00	5.18	2.96	0.00				
17.00	4.71	2.55	0.43	52.00	5.18	2.96	0.00				
18.00	4.81	2.64	0.33	53.00	5.18	2.96	0.00				
19.00	4.89	2.70	0.29	54.00	5.18	2.96	0.00				
20.00	4.96	2.76	0.26	55.00	5.18	2.96	0.00				
21.00	5.02	2.82	0.24	56.00	5.18	2.96	0.00				
22.00	5.08	2.87	0.22	57.00	5.18	2.96	0.00				
23.00	5.13	2.92	0.19	58.00	5.18	2.96	0.00				
24.00	5.18	2.96	0.17	59.00	5.18	2.96	0.00				
25.00	5.18	2.96	0.00	60.00	5.18	2.96	0.00				
26.00	5.18	2.96	0.00	61.00	5.18	2.96	0.00				
27.00	5.18	2.96	0.00	62.00	5.18	2.96	0.00				
28.00	5.18	2.96	0.00	63.00	5.18	2.96	0.00				
29.00	5.18	2.96	0.00	64.00	5.18	2.96	0.00				
30.00	5.18	2.96	0.00	65.00	5.18	2.96	0.00				
31.00	5.18	2.96	0.00	66.00	5.18	2.96	0.00				
32.00	5.18	2.96	0.00	67.00	5.18	2.96	0.00				
33.00	5.18	2.96	0.00	68.00	5.18	2.96	0.00				
34.00	5.18	2.96	0.00	69.00	5.18	2.96	0.00				
35.00	5.18	2.96	0.00	70.00	5.18	2.96	0.00				

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**Summary for Subcatchment 3S: Off-Site East**

Runoff = 1.34 cfs @ 12.09 hrs, Volume= 0.096 af, Depth= 2.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10 Year Rainfall=5.18"

Area (sf)	CN	Description
11,216	70	Woods, Good, HSG C
10,271	74	>75% Grass cover, Good, HSG C
21,487	72	Weighted Average
21,487		100.00% Pervious Area

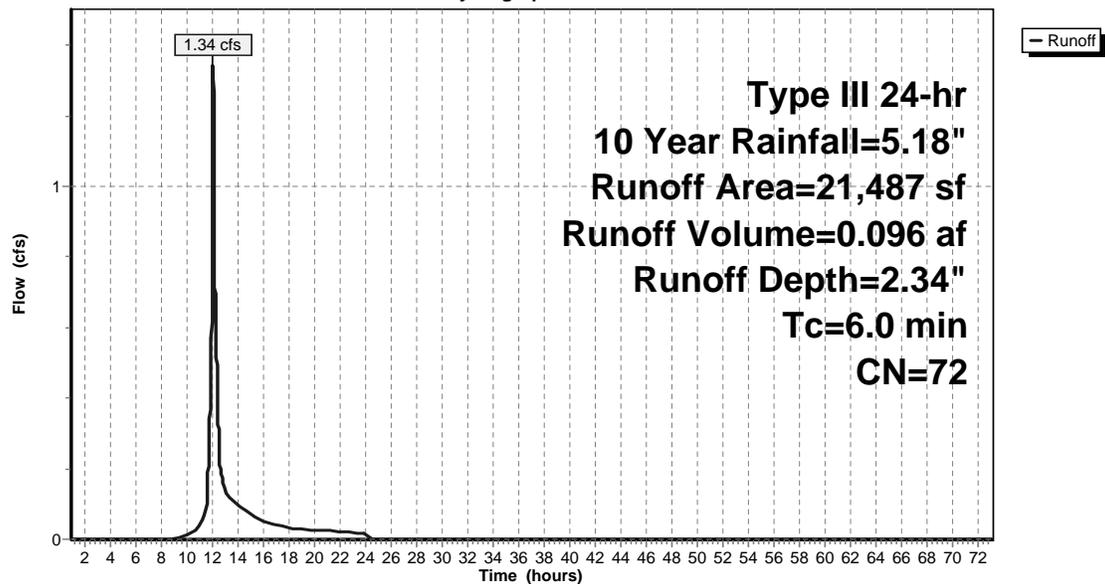
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

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**Subcatchment 3S: Off-Site East**

**Hydrograph**



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**Hydrograph for Subcatchment 3S: Off-Site East**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.05	0.00	0.00	36.00	5.18	2.34	0.00	71.00	5.18	2.34	0.00
2.00	0.10	0.00	0.00	37.00	5.18	2.34	0.00	72.00	5.18	2.34	0.00
3.00	0.16	0.00	0.00	38.00	5.18	2.34	0.00	73.00	5.18	2.34	0.00
4.00	0.22	0.00	0.00	39.00	5.18	2.34	0.00				
5.00	0.29	0.00	0.00	40.00	5.18	2.34	0.00				
6.00	0.37	0.00	0.00	41.00	5.18	2.34	0.00				
7.00	0.47	0.00	0.00	42.00	5.18	2.34	0.00				
8.00	0.59	0.00	0.00	43.00	5.18	2.34	0.00				
9.00	0.75	0.00	0.00	44.00	5.18	2.34	0.00				
10.00	0.98	0.01	0.01	45.00	5.18	2.34	0.00				
11.00	1.30	0.06	0.04	46.00	5.18	2.34	0.00				
12.00	2.59	0.58	<b>0.74</b>	47.00	5.18	2.34	0.00				
13.00	3.88	1.38	<b>0.14</b>	48.00	5.18	2.34	0.00				
14.00	4.20	1.60	0.09	49.00	5.18	2.34	0.00				
15.00	4.43	1.77	0.07	50.00	5.18	2.34	0.00				
16.00	4.59	1.89	0.05	51.00	5.18	2.34	0.00				
17.00	4.71	1.98	0.04	52.00	5.18	2.34	0.00				
18.00	4.81	2.05	0.03	53.00	5.18	2.34	0.00				
19.00	4.89	2.11	0.03	54.00	5.18	2.34	0.00				
20.00	4.96	2.17	0.03	55.00	5.18	2.34	0.00				
21.00	5.02	2.21	0.02	56.00	5.18	2.34	0.00				
22.00	5.08	2.26	0.02	57.00	5.18	2.34	0.00				
23.00	5.13	2.30	0.02	58.00	5.18	2.34	0.00				
24.00	<b>5.18</b>	<b>2.34</b>	0.02	59.00	5.18	2.34	0.00				
25.00	5.18	2.34	0.00	60.00	5.18	2.34	0.00				
26.00	5.18	2.34	0.00	61.00	5.18	2.34	0.00				
27.00	5.18	2.34	0.00	62.00	5.18	2.34	0.00				
28.00	5.18	2.34	0.00	63.00	5.18	2.34	0.00				
29.00	5.18	2.34	0.00	64.00	5.18	2.34	0.00				
30.00	5.18	2.34	0.00	65.00	5.18	2.34	0.00				
31.00	5.18	2.34	0.00	66.00	5.18	2.34	0.00				
32.00	5.18	2.34	0.00	67.00	5.18	2.34	0.00				
33.00	5.18	2.34	0.00	68.00	5.18	2.34	0.00				
34.00	5.18	2.34	0.00	69.00	5.18	2.34	0.00				
35.00	5.18	2.34	0.00	70.00	5.18	2.34	0.00				

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**Summary for Subcatchment 3Sa: Off-Site East**

Runoff = 6.82 cfs @ 12.12 hrs, Volume= 0.533 af, Depth= 3.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10 Year Rainfall=5.18"

Area (sf)	CN	Description
53,364	74	>75% Grass cover, Good, HSG C
26,882	98	Water Surface, HSG C
* 3,160	96	Gravel Road
83,406	83	Weighted Average
56,524		67.77% Pervious Area
26,882		32.23% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	50	0.0280	0.16		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.00"
0.4	82	0.0316	3.61		<b>Shallow Concentrated Flow, Shallow Conc. Flow</b> Paved Kv= 20.3 fps
3.1	234	0.0317	1.25		<b>Shallow Concentrated Flow, Shallow Conc Flow</b> Short Grass Pasture Kv= 7.0 fps
8.6	366	Total			

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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

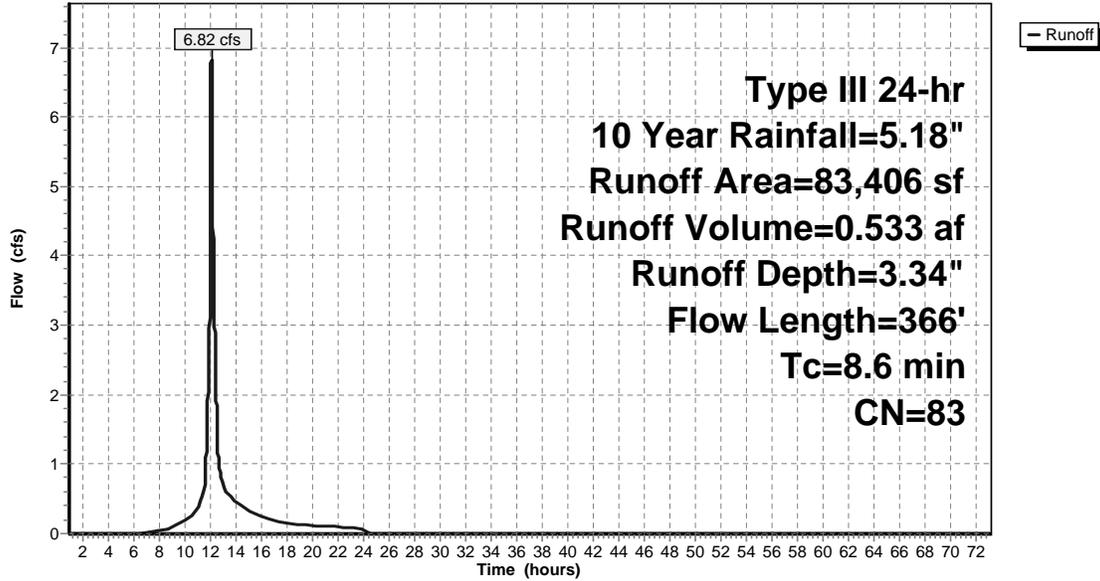
Type III 24-hr 10 Year Rainfall=5.18"

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**Subcatchment 3Sa: Off-Site East**

**Hydrograph**



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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 10 Year Rainfall=5.18"

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**Hydrograph for Subcatchment 3Sa: Off-Site East**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.05	0.00	0.00	36.00	5.18	3.34	0.00	71.00	5.18	3.34	0.00
2.00	0.10	0.00	0.00	37.00	5.18	3.34	0.00	72.00	5.18	3.34	0.00
3.00	0.16	0.00	0.00	38.00	5.18	3.34	0.00	73.00	5.18	3.34	0.00
4.00	0.22	0.00	0.00	39.00	5.18	3.34	0.00				
5.00	0.29	0.00	0.00	40.00	5.18	3.34	0.00				
6.00	0.37	0.00	0.00	41.00	5.18	3.34	0.00				
7.00	0.47	0.00	0.01	42.00	5.18	3.34	0.00				
8.00	0.59	0.01	0.04	43.00	5.18	3.34	0.00				
9.00	0.75	0.05	0.09	44.00	5.18	3.34	0.00				
10.00	0.98	0.12	0.18	45.00	5.18	3.34	0.00				
11.00	1.30	0.27	0.35	46.00	5.18	3.34	0.00				
12.00	2.59	1.12	<b>3.52</b>	47.00	5.18	3.34	0.00				
13.00	3.88	2.19	<b>0.73</b>	48.00	5.18	3.34	0.00				
14.00	4.20	2.46	0.46	49.00	5.18	3.34	0.00				
15.00	4.43	2.66	0.35	50.00	5.18	3.34	0.00				
16.00	4.59	2.81	0.25	51.00	5.18	3.34	0.00				
17.00	4.71	2.91	0.19	52.00	5.18	3.34	0.00				
18.00	4.81	3.00	0.15	53.00	5.18	3.34	0.00				
19.00	4.89	3.07	0.13	54.00	5.18	3.34	0.00				
20.00	4.96	3.14	0.12	55.00	5.18	3.34	0.00				
21.00	5.02	3.19	0.11	56.00	5.18	3.34	0.00				
22.00	5.08	3.25	0.10	57.00	5.18	3.34	0.00				
23.00	5.13	3.29	0.09	58.00	5.18	3.34	0.00				
24.00	<b>5.18</b>	<b>3.34</b>	0.08	59.00	5.18	3.34	0.00				
25.00	5.18	3.34	0.00	60.00	5.18	3.34	0.00				
26.00	5.18	3.34	0.00	61.00	5.18	3.34	0.00				
27.00	5.18	3.34	0.00	62.00	5.18	3.34	0.00				
28.00	5.18	3.34	0.00	63.00	5.18	3.34	0.00				
29.00	5.18	3.34	0.00	64.00	5.18	3.34	0.00				
30.00	5.18	3.34	0.00	65.00	5.18	3.34	0.00				
31.00	5.18	3.34	0.00	66.00	5.18	3.34	0.00				
32.00	5.18	3.34	0.00	67.00	5.18	3.34	0.00				
33.00	5.18	3.34	0.00	68.00	5.18	3.34	0.00				
34.00	5.18	3.34	0.00	69.00	5.18	3.34	0.00				
35.00	5.18	3.34	0.00	70.00	5.18	3.34	0.00				

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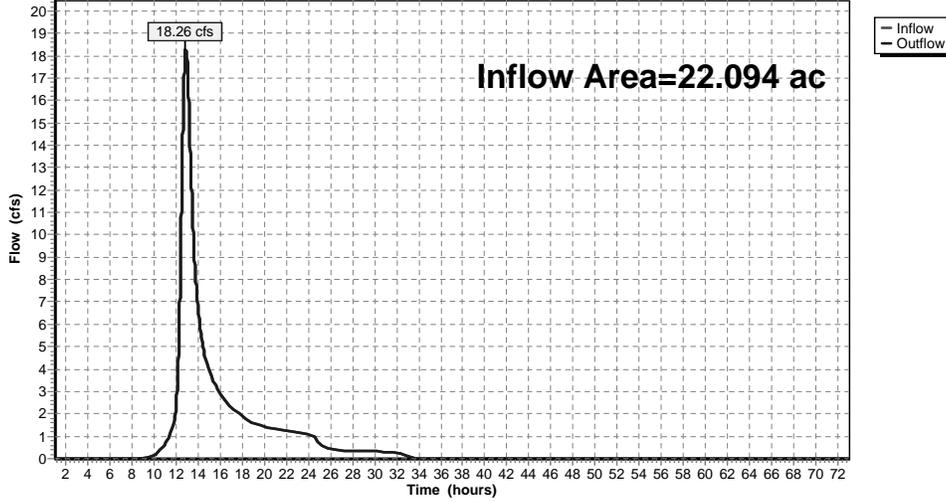
**Summary for Reach DP-1: (new Reach)**

Inflow Area = 22.094 ac, 3.96% Impervious, Inflow Depth = 2.21" for 10 Year event  
 Inflow = 18.26 cfs @ 12.83 hrs, Volume= 4.066 af  
 Outflow = 18.26 cfs @ 12.83 hrs, Volume= 4.066 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-1: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-1: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.00		0.00	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.00		0.00	42.00	0.00		0.00				
8.00	0.00		0.00	43.00	0.00		0.00				
9.00	0.02		0.02	44.00	0.00		0.00				
10.00	0.16		0.16	45.00	0.00		0.00				
11.00	0.69		0.69	46.00	0.00		0.00				
12.00	<b>2.58</b>		<b>2.58</b>	47.00	0.00		0.00				
13.00	<b>17.51</b>		<b>17.51</b>	48.00	0.00		0.00				
14.00	6.46		6.46	49.00	0.00		0.00				
15.00	3.87		3.87	50.00	0.00		0.00				
16.00	2.92		2.92	51.00	0.00		0.00				
17.00	2.26		2.26	52.00	0.00		0.00				
18.00	1.87		1.87	53.00	0.00		0.00				
19.00	1.58		1.58	54.00	0.00		0.00				
20.00	1.44		1.44	55.00	0.00		0.00				
21.00	1.34		1.34	56.00	0.00		0.00				
22.00	1.26		1.26	57.00	0.00		0.00				
23.00	1.17		1.17	58.00	0.00		0.00				
24.00	1.09		1.09	59.00	0.00		0.00				
25.00	0.64		0.64	60.00	0.00		0.00				
26.00	0.40		0.40	61.00	0.00		0.00				
27.00	0.37		0.37	62.00	0.00		0.00				
28.00	0.35		0.35	63.00	0.00		0.00				
29.00	0.34		0.34	64.00	0.00		0.00				
30.00	0.32		0.32	65.00	0.00		0.00				
31.00	0.29		0.29	66.00	0.00		0.00				
32.00	0.26		0.26	67.00	0.00		0.00				
33.00	0.12		0.12	68.00	0.00		0.00				
34.00	0.02		0.02	69.00	0.00		0.00				
35.00	0.00		0.00	70.00	0.00		0.00				

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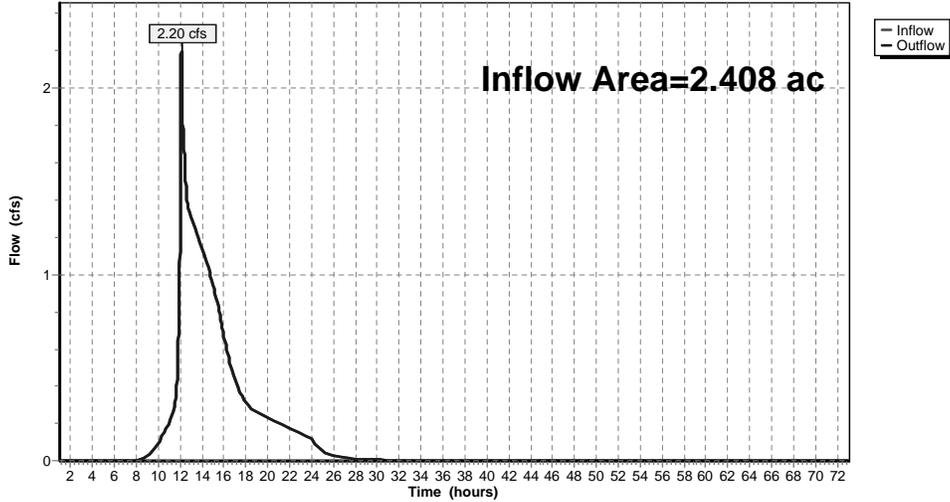
**Summary for Reach DP-3: (new Reach)**

Inflow Area = 2.408 ac, 25.63% Impervious, Inflow Depth = 3.13" for 10 Year event  
 Inflow = 2.20 cfs @ 12.10 hrs, Volume= 0.629 af  
 Outflow = 2.20 cfs @ 12.10 hrs, Volume= 0.629 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-3: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-3: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.00		0.00	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.00		0.00	42.00	0.00		0.00				
8.00	0.00		0.00	43.00	0.00		0.00				
9.00	0.03		0.03	44.00	0.00		0.00				
10.00	0.10		0.10	45.00	0.00		0.00				
11.00	0.20		0.20	46.00	0.00		0.00				
12.00	<b>1.36</b>		<b>1.36</b>	47.00	0.00		0.00				
13.00	<b>1.31</b>		<b>1.31</b>	48.00	0.00		0.00				
14.00	1.14		1.14	49.00	0.00		0.00				
15.00	0.94		0.94	50.00	0.00		0.00				
16.00	0.67		0.67	51.00	0.00		0.00				
17.00	0.43		0.43	52.00	0.00		0.00				
18.00	0.31		0.31	53.00	0.00		0.00				
19.00	0.26		0.26	54.00	0.00		0.00				
20.00	0.23		0.23	55.00	0.00		0.00				
21.00	0.20		0.20	56.00	0.00		0.00				
22.00	0.17		0.17	57.00	0.00		0.00				
23.00	0.15		0.15	58.00	0.00		0.00				
24.00	0.12		0.12	59.00	0.00		0.00				
25.00	0.05		0.05	60.00	0.00		0.00				
26.00	0.03		0.03	61.00	0.00		0.00				
27.00	0.01		0.01	62.00	0.00		0.00				
28.00	0.01		0.01	63.00	0.00		0.00				
29.00	0.01		0.01	64.00	0.00		0.00				
30.00	0.00		0.00	65.00	0.00		0.00				
31.00	0.00		0.00	66.00	0.00		0.00				
32.00	0.00		0.00	67.00	0.00		0.00				
33.00	0.00		0.00	68.00	0.00		0.00				
34.00	0.00		0.00	69.00	0.00		0.00				
35.00	0.00		0.00	70.00	0.00		0.00				

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**Summary for Pond P1A: Pond 1a (Pond Repair)**

Inflow Area = 4.370 ac, 20.04% Impervious, Inflow Depth = 2.96" for 10 Year event  
 Inflow = 12.16 cfs @ 12.18 hrs, Volume= 1.077 af  
 Outflow = 0.73 cfs @ 15.14 hrs, Volume= 1.077 af, Atten= 94%, Lag= 177.9 min  
 Discarded = 0.27 cfs @ 15.14 hrs, Volume= 0.340 af  
 Primary = 0.46 cfs @ 15.14 hrs, Volume= 0.737 af  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 78.58' @ 15.14 hrs Surf.Area= 23,723 sf Storage= 26,263 cf

Plug-Flow detention time= 412.6 min calculated for 1.077 af (100% of inflow)  
 Center-of-Mass det. time= 412.6 min ( 1,241.9 - 829.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	75.50'	1,242 cf	<b>Custom Stage Data (Irregular)</b> Listed below 3,106 cf Overall x 40.0% Voids
#2	76.50'	37,823 cf	<b>Custom Stage Data (Irregular)</b> Listed below 39,065 cf Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
75.50	3,106	220.0	0	0	3,106
76.00	3,106	220.0	1,553	1,553	3,216
76.50	3,106	220.0	1,553	3,106	3,326

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.50	3,106	220.0	0	0	3,106
77.00	6,731	331.0	2,402	2,402	7,975
78.00	15,313	639.8	10,732	13,134	31,836
79.20	26,330	782.0	24,689	37,823	47,947

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Device	Routing	Invert	Outlet Devices
#1	Secondary	78.70'	<b>14.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	75.50'	<b>0.270 in/hr Exfiltration over Wetted area</b>
#3	Primary	75.50'	<b>4.0" Round Culvert</b> L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 75.50' / 75.10' S= 0.0100 ' S= 0.0100 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.27 cfs @ 15.14 hrs HW=78.58' (Free Discharge)  
 ↳ **2=Exfiltration** (Exfiltration Controls 0.27 cfs)

**Primary OutFlow** Max=0.46 cfs @ 15.14 hrs HW=78.58' (Free Discharge)  
 ↳ **3=Culvert** (Barrel Controls 0.46 cfs @ 5.26 fps)

**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=75.50' (Free Discharge)  
 ↳ **1=Broad-Crested Rectangular Weir** ( Controls 0.00 cfs)

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Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

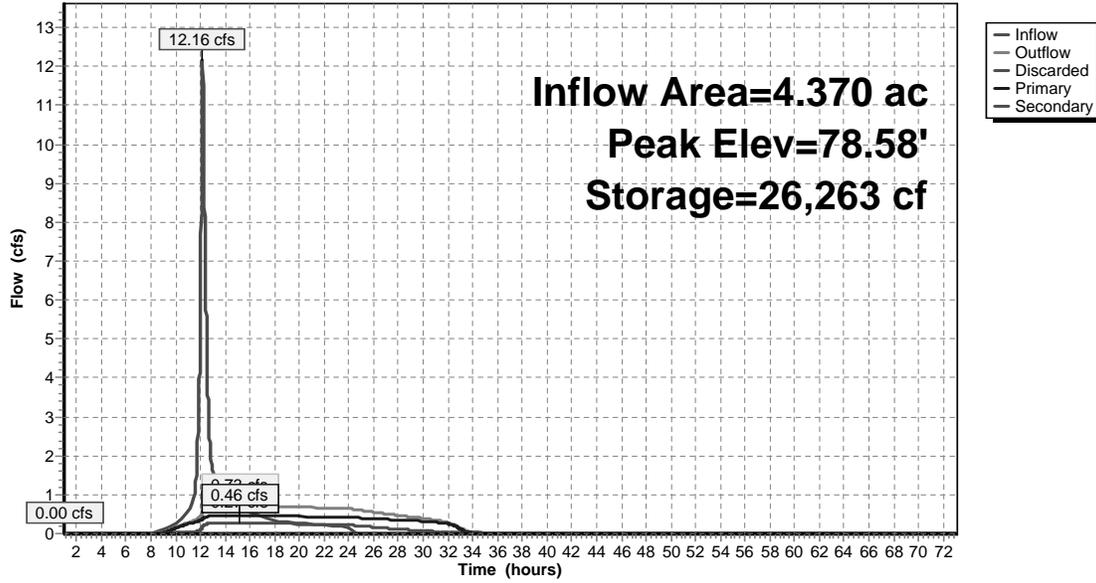
Type III 24-hr 10 Year Rainfall=5.18"

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Pond P1A: Pond 1a (Pond Repair)

Hydrograph



1817-Basin Repair 2024

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Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

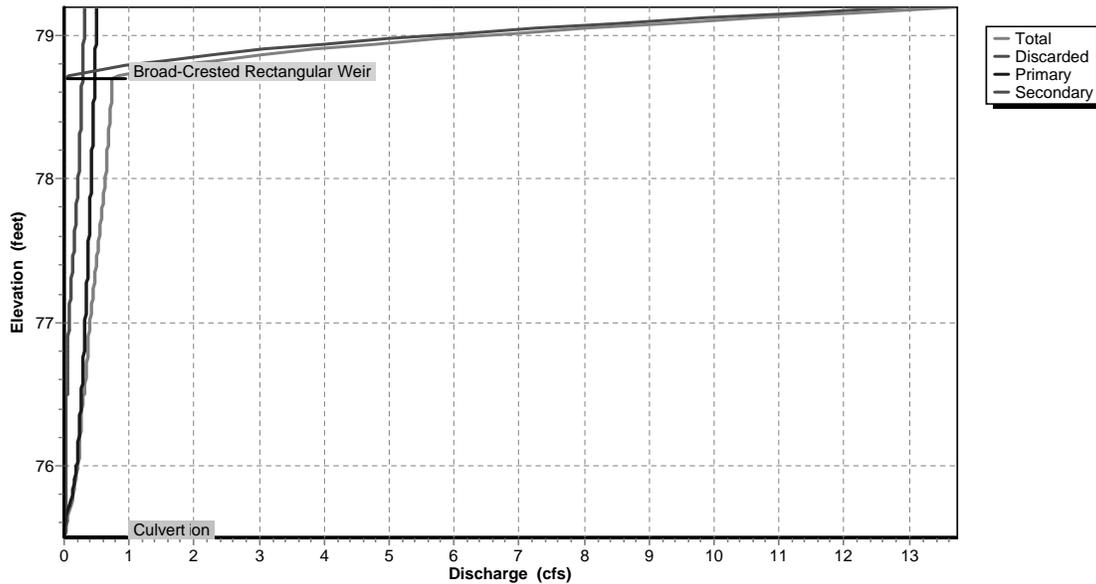
Type III 24-hr 10 Year Rainfall=5.18"

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Pond P1A: Pond 1a (Pond Repair)

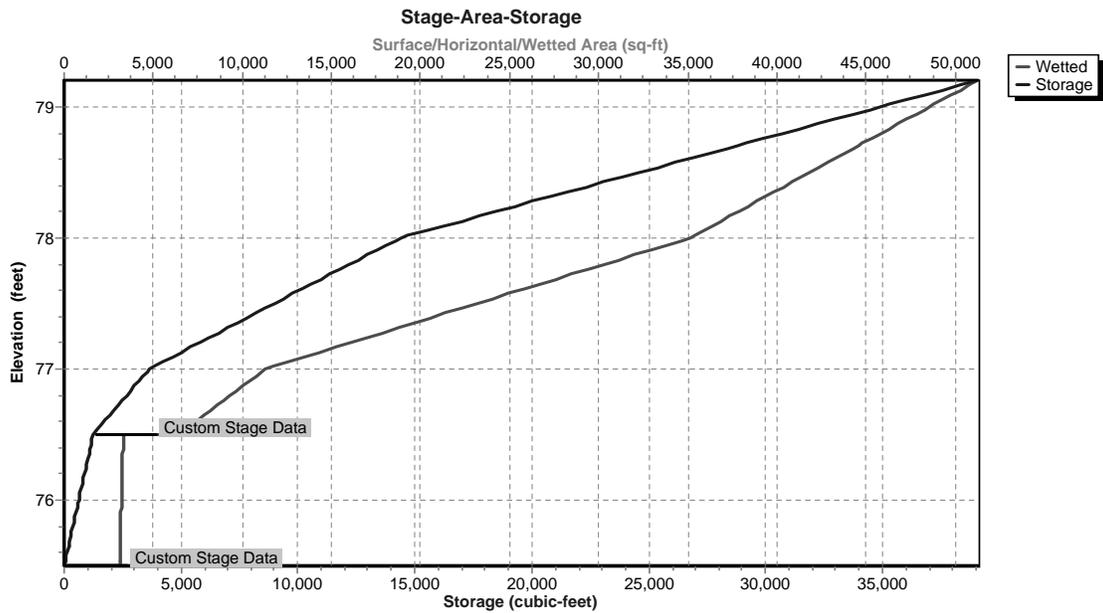
Stage-Discharge



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**Pond P1A: Pond 1a (Pond Repair)**



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**Hydrograph for Pond P1A: Pond 1a (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
1.00	0.00	0	75.50	0.00	0.00	0.00	0.00
6.00	0.00	0	75.50	0.00	0.00	0.00	0.00
11.00	<b>0.58</b>	<b>1,085</b>	<b>76.37</b>	<b>0.27</b>	<b>0.02</b>	<b>0.25</b>	0.00
16.00	<b>0.54</b>	<b>25,983</b>	<b>78.56</b>	<b>0.72</b>	<b>0.27</b>	<b>0.46</b>	0.00
21.00	0.24	19,400	78.24	0.67	0.24	0.43	0.00
26.00	0.00	10,398	77.63	0.55	0.16	0.38	0.00
31.00	0.00	2,324	76.73	0.35	0.05	0.29	0.00
36.00	0.00	5	75.50	0.00	0.00	0.00	0.00
41.00	0.00	0	75.50	0.00	0.00	0.00	0.00
46.00	0.00	0	75.50	0.00	0.00	0.00	0.00
51.00	0.00	0	75.50	0.00	0.00	0.00	0.00
56.00	0.00	0	75.50	0.00	0.00	0.00	0.00
61.00	0.00	0	75.50	0.00	0.00	0.00	0.00
66.00	0.00	0	75.50	0.00	0.00	0.00	0.00
71.00	0.00	0	75.50	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
75.50	0.00	0.00	0.00	0.00	79.00	6.41	0.30	0.49	5.61
75.60	0.04	0.02	0.02	0.00	79.10	9.70	0.31	0.50	8.89
75.70	0.09	0.02	0.07	0.00	79.20	<b>13.72</b>	<b>0.32</b>	<b>0.50</b>	<b>12.89</b>
75.80	0.14	0.02	0.12	0.00					
75.90	0.18	0.02	0.16	0.00					
76.00	0.21	0.02	0.19	0.00					
76.10	0.23	0.02	0.21	0.00					
76.20	0.25	0.02	0.23	0.00					
76.30	0.26	0.02	0.24	0.00					
76.40	0.27	0.02	0.25	0.00					
76.50	0.31	0.04	0.27	0.00					
76.60	0.33	0.05	0.28	0.00					
76.70	0.34	0.05	0.29	0.00					
76.80	0.36	0.06	0.30	0.00					
76.90	0.38	0.06	0.31	0.00					
77.00	0.39	0.07	0.32	0.00					
77.10	0.42	0.09	0.33	0.00					
77.20	0.44	0.10	0.34	0.00					
77.30	0.47	0.12	0.35	0.00					
77.40	0.49	0.13	0.36	0.00					
77.50	0.52	0.15	0.37	0.00					
77.60	0.54	0.16	0.38	0.00					
77.70	0.56	0.18	0.39	0.00					
77.80	0.59	0.19	0.40	0.00					
77.90	0.61	0.20	0.41	0.00					
78.00	0.63	0.22	0.41	0.00					
78.10	0.65	0.23	0.42	0.00					
78.20	0.67	0.24	0.43	0.00					
78.30	0.68	0.24	0.44	0.00					
78.40	0.70	0.25	0.45	0.00					
78.50	0.71	0.26	0.45	0.00					
78.60	0.73	0.27	0.46	0.00					
78.70	0.75	0.28	0.47	0.00					
78.80	1.81	0.29	0.47	1.05					
78.90	3.74	0.30	0.48	2.97					

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**Stage-Area-Storage for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)
75.50	3,106	0	77.25	17,266	6,327	79.00	48,588	34,950
75.55	3,117	62	77.30	18,459	6,864	79.05	49,260	35,979
75.60	3,128	124	77.35	19,652	7,400	79.10	49,931	37,008
75.65	3,139	186	77.40	20,845	7,937	79.15	50,602	38,036
75.70	3,150	248	77.45	22,038	8,473	79.20	<b>51,273</b>	<b>39,065</b>
75.75	3,161	311	77.50	23,231	9,010			
75.80	3,172	373	77.55	24,424	9,547			
75.85	3,183	435	77.60	25,618	10,083			
75.90	3,194	497	77.65	26,811	10,620			
75.95	3,205	559	77.70	28,004	11,156			
76.00	3,216	621	77.75	29,197	11,693			
76.05	3,227	683	77.80	30,390	12,230			
76.10	3,238	745	77.85	31,583	12,766			
76.15	3,249	808	77.90	32,776	13,303			
76.20	3,260	870	77.95	33,969	13,839			
76.25	3,271	932	78.00	35,162	14,376			
76.30	3,282	994	78.05	35,833	15,405			
76.35	3,293	1,056	78.10	36,505	16,434			
76.40	3,304	1,118	78.15	37,176	17,462			
76.45	3,315	1,180	78.20	37,847	18,491			
76.50	6,432	1,242	78.25	38,518	19,520			
76.55	6,919	1,483	78.30	39,190	20,548			
76.60	7,406	1,723	78.35	39,861	21,577			
76.65	7,893	1,963	78.40	40,532	22,606			
76.70	8,380	2,203	78.45	41,204	23,634			
76.75	8,866	2,443	78.50	41,875	24,663			
76.80	9,353	2,683	78.55	42,546	25,692			
76.85	9,840	2,923	78.60	43,218	26,721			
76.90	10,327	3,164	78.65	43,889	27,749			
76.95	10,814	3,404	78.70	44,560	28,778			
77.00	11,301	3,644	78.75	45,232	29,807			
77.05	12,494	4,181	78.80	45,903	30,835			
77.10	13,687	4,717	78.85	46,574	31,864			
77.15	14,880	5,254	78.90	47,246	32,893			
77.20	16,073	5,790	78.95	47,917	33,922			

**1817-Basin Repair 2024**

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**Summary for Pond P3A: Pond 3A (Pond Repair)**

Inflow Area = 1.915 ac, 32.23% Impervious, Inflow Depth = 3.34" for 10 Year event  
 Inflow = 6.82 cfs @ 12.12 hrs, Volume= 0.533 af  
 Outflow = 1.18 cfs @ 12.63 hrs, Volume= 0.533 af, Atten= 83%, Lag= 30.6 min  
 Primary = 0.44 cfs @ 12.63 hrs, Volume= 0.316 af  
 Secondary = 0.74 cfs @ 12.63 hrs, Volume= 0.217 af  
 Tertiary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 77.59' @ 12.63 hrs Surf.Area= 12,414 sf Storage= 9,691 cf  
 Flood Elev= 79.50' Surf.Area= 25,484 sf Storage= 37,166 cf

Plug-Flow detention time= 117.2 min calculated for 0.532 af (100% of inflow)  
 Center-of-Mass det. time= 117.4 min ( 931.9 - 814.4 )

Volume	Invert	Avail.Storage	Storage Description		
#1	76.00'	37,166 cf	<b>Custom Stage Data (Irregular)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.00	2,053	339.0	0	0	2,053
77.00	6,709	559.0	4,158	4,158	17,781
78.00	17,458	791.4	11,663	15,821	42,764
79.00	25,484	883.5	21,345	37,166	55,068

Device	Routing	Invert	Outlet Devices
#1	Primary	76.00'	<b>4.0" Round 6" Culvert 1</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.00' / 75.52' S= 0.0240 1/8" Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Secondary	76.55'	<b>6.0" Round 6" Culvert 2</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.55' / 75.60' S= 0.0475 1/8" Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#3	Tertiary	78.50'	<b>20.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50

**1817-Basin Repair 2024**

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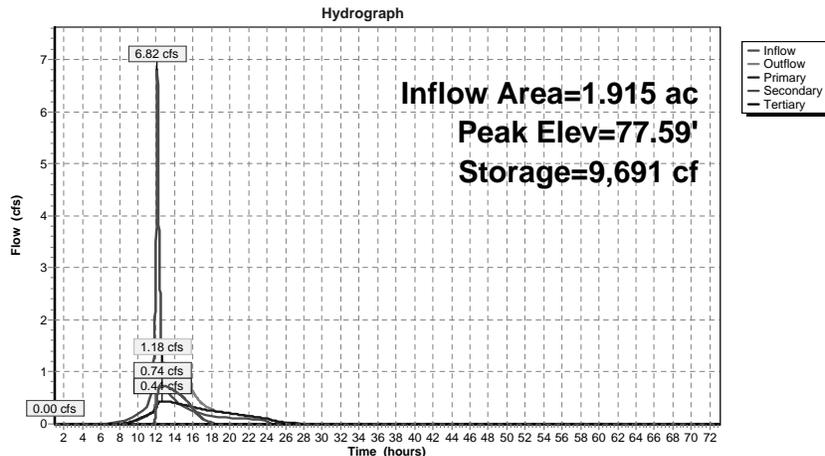
Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76  
 2.83

**Primary OutFlow** Max=0.44 cfs @ 12.63 hrs HW=77.59' (Free Discharge)  
 1=6" Culvert 1 (Barrel Controls 0.44 cfs @ 5.03 fps)

**Secondary OutFlow** Max=0.74 cfs @ 12.63 hrs HW=77.59' (Free Discharge)  
 2=6" Culvert 2 (Inlet Controls 0.74 cfs @ 3.77 fps)

**Tertiary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=76.00' (Free Discharge)  
 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Pond P3A: Pond 3A (Pond Repair)**



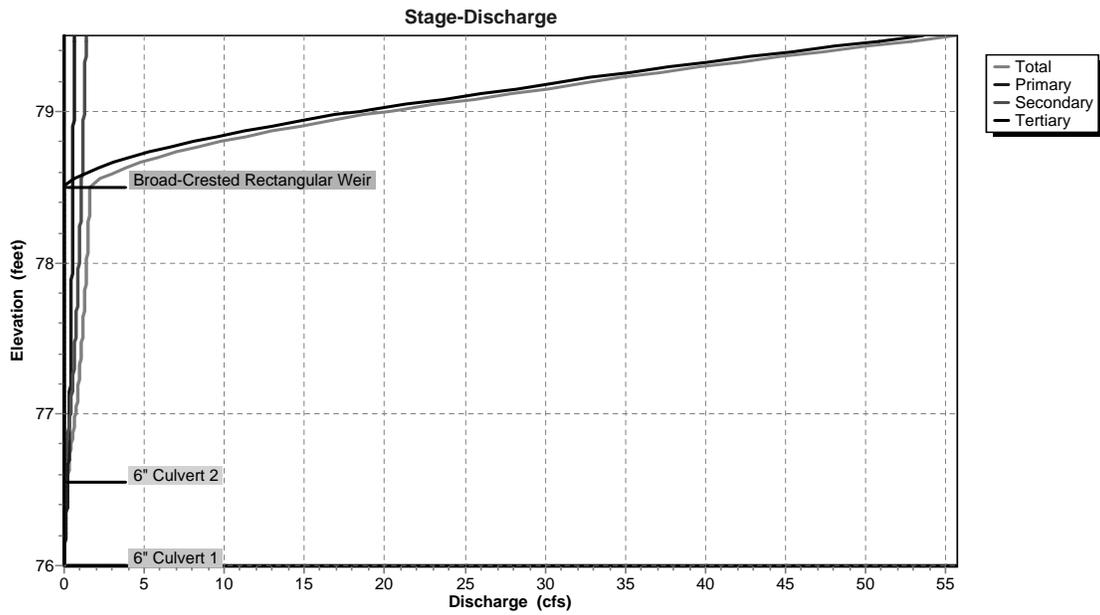
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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms  
Type III 24-hr 10 Year Rainfall=5.18"

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Pond P3A: Pond 3A (Pond Repair)



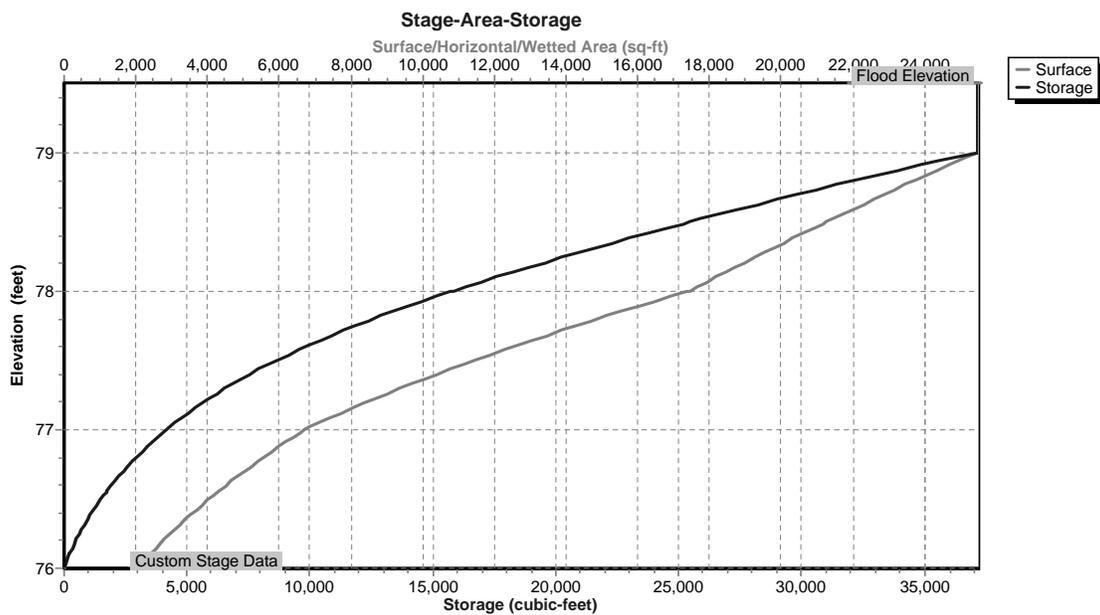
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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms  
Type III 24-hr 10 Year Rainfall=5.18"

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Pond P3A: Pond 3A (Pond Repair)



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**Hydrograph for Pond P3A: Pond 3A (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
1.00	0.00	0	76.00	0.00	0.00	0.00	0.00
6.00	0.00	0	76.00	0.00	0.00	0.00	0.00
11.00	0.35	995	76.37	0.17	0.17	0.00	0.00
16.00	0.25	3,686	76.93	0.62	0.32	0.29	0.00
21.00	0.11	1,113	76.40	0.18	0.18	0.00	0.00
26.00	0.00	247	76.11	0.03	0.03	0.00	0.00
31.00	0.00	77	76.04	0.00	0.00	0.00	0.00
36.00	0.00	40	76.02	0.00	0.00	0.00	0.00
41.00	0.00	20	76.01	0.00	0.00	0.00	0.00
46.00	0.00	10	76.00	0.00	0.00	0.00	0.00
51.00	0.00	5	76.00	0.00	0.00	0.00	0.00
56.00	0.00	3	76.00	0.00	0.00	0.00	0.00
61.00	0.00	1	76.00	0.00	0.00	0.00	0.00
66.00	0.00	1	76.00	0.00	0.00	0.00	0.00
71.00	0.00	0	76.00	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
76.00	0.00	0.00	0.00	0.00	79.50	55.61	0.64	1.37	53.60
76.10	0.02	0.02	0.00	0.00					
76.20	0.07	0.07	0.00	0.00					
76.30	0.14	0.14	0.00	0.00					
76.40	0.18	0.18	0.00	0.00					
76.50	0.21	0.21	0.00	0.00					
76.60	0.25	0.24	0.01	0.00					
76.70	0.33	0.27	0.06	0.00					
76.80	0.44	0.30	0.15	0.00					
76.90	0.58	0.32	0.26	0.00					
77.00	0.71	0.34	0.38	0.00					
77.10	0.82	0.36	0.46	0.00					
77.20	0.90	0.38	0.53	0.00					
77.30	0.98	0.39	0.59	0.00					
77.40	1.06	0.41	0.65	0.00					
77.50	1.13	0.43	0.70	0.00					
77.60	1.19	0.44	0.75	0.00					
77.70	1.24	0.45	0.79	0.00					
77.80	1.30	0.46	0.83	0.00					
77.90	1.35	0.48	0.87	0.00					
78.00	1.40	0.49	0.91	0.00					
78.10	1.45	0.50	0.95	0.00					
78.20	1.50	0.51	0.99	0.00					
78.30	1.54	0.52	1.02	0.00					
78.40	1.59	0.53	1.06	0.00					
78.50	1.63	0.54	1.09	0.00					
78.60	3.17	0.55	1.12	1.50					
78.70	5.95	0.56	1.15	4.24					
78.80	9.77	0.57	1.18	8.02					
78.90	14.49	0.58	1.21	12.70					
79.00	20.25	0.59	1.24	18.42					
79.10	26.96	0.60	1.27	25.10					
79.20	33.41	0.61	1.29	31.51					
79.30	40.29	0.62	1.32	38.35					
79.40	47.74	0.63	1.35	45.76					

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**Stage-Area-Storage for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
76.00	2,053	0	77.75	14,298	11,858	79.50	25,484	37,166
76.05	2,222	107	77.80	14,905	12,588			
76.10	2,398	222	77.85	15,524	13,349			
76.15	2,581	347	77.90	16,156	14,141			
76.20	2,770	481	77.95	16,801	14,964			
76.25	2,966	624	78.00	17,458	15,821			
76.30	3,169	777	78.05	17,823	16,703			
76.35	3,378	941	78.10	18,192	17,603			
76.40	3,594	1,115	78.15	18,565	18,522			
76.45	3,817	1,300	78.20	18,942	19,460			
76.50	4,046	1,497	78.25	19,323	20,417			
76.55	4,282	1,705	78.30	19,707	21,392			
76.60	4,525	1,925	78.35	20,095	22,387			
76.65	4,775	2,158	78.40	20,487	23,402			
76.70	5,031	2,403	78.45	20,882	24,436			
76.75	5,294	2,661	78.50	21,282	25,490			
76.80	5,563	2,932	78.55	21,685	26,564			
76.85	5,840	3,217	78.60	22,092	27,659			
76.90	6,123	3,516	78.65	22,503	28,774			
76.95	6,413	3,830	78.70	22,917	29,909			
77.00	6,709	4,158	78.75	23,336	31,065			
77.05	7,127	4,504	78.80	23,758	32,243			
77.10	7,557	4,871	78.85	24,184	33,441			
77.15	8,000	5,259	78.90	24,613	34,661			
77.20	8,455	5,671	78.95	25,047	35,903			
77.25	8,923	6,105	79.00	<b>25,484</b>	<b>37,166</b>			
77.30	9,404	6,563	79.05	25,484	37,166			
77.35	9,897	7,046	79.10	25,484	37,166			
77.40	10,403	7,553	79.15	25,484	37,166			
77.45	10,922	8,086	79.20	25,484	37,166			
77.50	11,453	8,646	79.25	25,484	37,166			
77.55	11,997	9,232	79.30	25,484	37,166			
77.60	12,553	9,846	79.35	25,484	37,166			
77.65	13,122	10,487	79.40	25,484	37,166			
77.70	13,704	11,158	79.45	25,484	37,166			

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Time span=1.00-73.00 hrs, dt=0.01 hrs, 7201 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment 1S: Off-Site Northeast**

Runoff Area=772,071 sf 0.00% Impervious Runoff Depth=3.22"  
 Flow Length=1,645' Tc=61.7 min CN=71 Runoff=25.87 cfs 4.762 af

**Subcatchment 1Sa: Off-Site**

Runoff Area=190,352 sf 20.04% Impervious Runoff Depth=4.04"  
 Flow Length=540' Tc=12.8 min CN=79 Runoff=16.56 cfs 1.471 af

**Subcatchment 3S: Off-Site East**

Runoff Area=21,487 sf 0.00% Impervious Runoff Depth=3.32"  
 Tc=6.0 min CN=72 Runoff=1.92 cfs 0.137 af

**Subcatchment 3Sa: Off-Site East**

Runoff Area=83,406 sf 32.23% Impervious Runoff Depth=4.46"  
 Flow Length=366' Tc=8.6 min CN=83 Runoff=9.04 cfs 0.712 af

**Reach DP-1: (new Reach)**

Inflow=28.14 cfs 5.832 af  
 Outflow=28.14 cfs 5.832 af

**Reach DP-3: (new Reach)**

Inflow=2.95 cfs 0.849 af  
 Outflow=2.95 cfs 0.849 af

**Pond P1A: Pond 1a (Pond Repair)**

Peak Elev=78.84' Storage=31,721 cf Inflow=16.56 cfs 1.471 af  
 Discarded=0.29 cfs 0.401 af Primary=0.48 cfs 0.843 af Secondary=1.80 cfs 0.227 af Outflow=2.57 cfs 1.471 af

**Pond P3A: Pond 3A (Pond Repair)**

Peak Elev=77.86' Storage=13,503 cf Inflow=9.04 cfs 0.712 af  
 Primary=0.47 cfs 0.383 af Secondary=0.86 cfs 0.329 af Tertiary=0.00 cfs 0.000 af Outflow=1.33 cfs 0.712 af

**Total Runoff Area = 24.502 ac Runoff Volume = 7.082 af Average Runoff Depth = 3.47"**  
**93.91% Pervious = 23.009 ac 6.09% Impervious = 1.493 ac**

**1817-Basin Repair 2024**

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**Summary for Subcatchment 1S: Off-Site Northeast**

Runoff = 25.87 cfs @ 12.82 hrs, Volume= 4.762 af, Depth= 3.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25 Year Rainfall=6.40"

Area (sf)	CN	Description
650,962	70	Woods, Good, HSG C
115,309	74	>75% Grass cover, Good, HSG C
* 5,800	96	Gravel Road, HSG C
772,071	71	Weighted Average
772,071		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.0	50	0.0080	0.03		<b>Sheet Flow,</b> Woods: Dense underbrush n= 0.800 P2= 3.00"
12.6	628	0.0276	0.83		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
3.3	496	0.0276	2.49		<b>Shallow Concentrated Flow,</b> Grassed Waterway Kv= 15.0 fps
13.8	471	0.0130	0.57		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
61.7	1,645	Total			

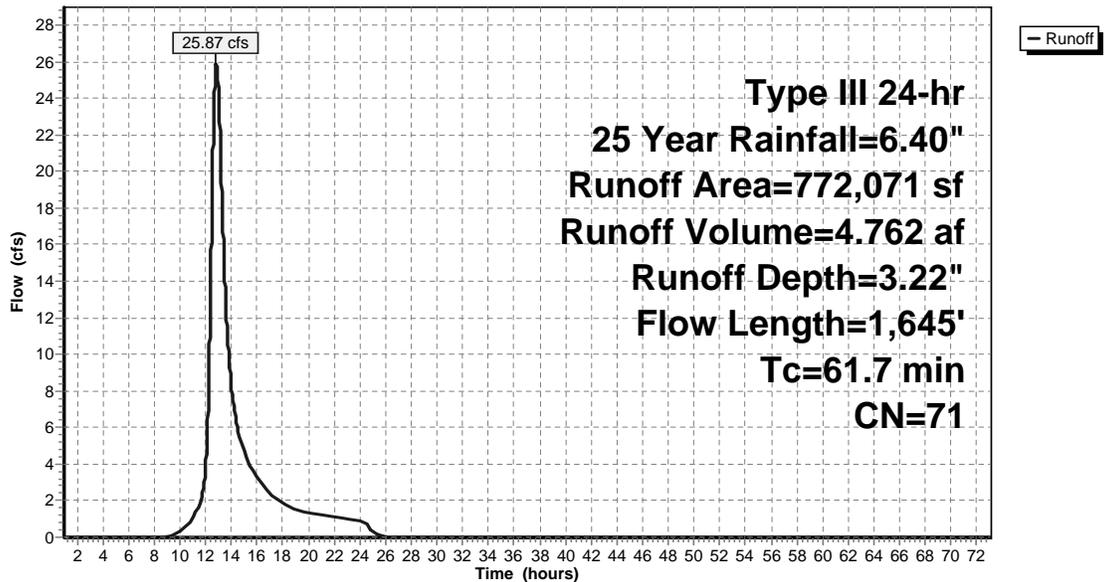
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**Subcatchment 1S: Off-Site Northeast**

**Hydrograph**



**1817-Basin Repair 2024**

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**Hydrograph for Subcatchment 1S: Off-Site Northeast**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.06	0.00	0.00	36.00	6.40	3.22	0.00	71.00	6.40	3.22	0.00
2.00	0.13	0.00	0.00	37.00	6.40	3.22	0.00	72.00	6.40	3.22	0.00
3.00	0.20	0.00	0.00	38.00	6.40	3.22	0.00	73.00	6.40	3.22	0.00
4.00	0.28	0.00	0.00	39.00	6.40	3.22	0.00				
5.00	0.36	0.00	0.00	40.00	6.40	3.22	0.00				
6.00	0.46	0.00	0.00	41.00	6.40	3.22	0.00				
7.00	0.58	0.00	0.00	42.00	6.40	3.22	0.00				
8.00	0.73	0.00	0.00	43.00	6.40	3.22	0.00				
9.00	0.93	0.00	0.01	44.00	6.40	3.22	0.00				
10.00	1.21	0.03	0.30	45.00	6.40	3.22	0.00				
11.00	1.60	0.13	1.09	46.00	6.40	3.22	0.00				
12.00	3.20	0.88	<b>3.87</b>	47.00	6.40	3.22	0.00				
13.00	4.80	1.97	<b>24.50</b>	48.00	6.40	3.22	0.00				
14.00	5.19	2.26	8.30	49.00	6.40	3.22	0.00				
15.00	5.47	2.48	4.62	50.00	6.40	3.22	0.00				
16.00	5.67	2.64	3.32	51.00	6.40	3.22	0.00				
17.00	5.82	2.76	2.42	52.00	6.40	3.22	0.00				
18.00	5.94	2.85	1.90	53.00	6.40	3.22	0.00				
19.00	6.04	2.93	1.51	54.00	6.40	3.22	0.00				
20.00	6.12	3.00	1.34	55.00	6.40	3.22	0.00				
21.00	6.20	3.06	1.21	56.00	6.40	3.22	0.00				
22.00	6.28	3.12	1.10	57.00	6.40	3.22	0.00				
23.00	6.34	3.18	1.00	58.00	6.40	3.22	0.00				
24.00	<b>6.40</b>	<b>3.22</b>	0.90	59.00	6.40	3.22	0.00				
25.00	6.40	3.22	0.32	60.00	6.40	3.22	0.00				
26.00	6.40	3.22	0.03	61.00	6.40	3.22	0.00				
27.00	6.40	3.22	0.00	62.00	6.40	3.22	0.00				
28.00	6.40	3.22	0.00	63.00	6.40	3.22	0.00				
29.00	6.40	3.22	0.00	64.00	6.40	3.22	0.00				
30.00	6.40	3.22	0.00	65.00	6.40	3.22	0.00				
31.00	6.40	3.22	0.00	66.00	6.40	3.22	0.00				
32.00	6.40	3.22	0.00	67.00	6.40	3.22	0.00				
33.00	6.40	3.22	0.00	68.00	6.40	3.22	0.00				
34.00	6.40	3.22	0.00	69.00	6.40	3.22	0.00				
35.00	6.40	3.22	0.00	70.00	6.40	3.22	0.00				

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**Summary for Subcatchment 1Sa: Off-Site**

Runoff = 16.56 cfs @ 12.17 hrs, Volume= 1.471 af, Depth= 4.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25 Year Rainfall=6.40"

Area (sf)	CN	Description
152,204	74	>75% Grass cover, Good, HSG C
* 9,937	98	Gravel Road, HSG C
27,571	98	Water Surface, HSG C
* 640	98	Equipment Pad, HSG C
190,352	79	Weighted Average
152,204		79.96% Pervious Area
38,148		20.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	50	0.0380	0.19		<b>Sheet Flow,</b> Grass: Short n=0.150 P2= 3.00"
8.3	490	0.0196	0.98		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
12.8	540	Total			

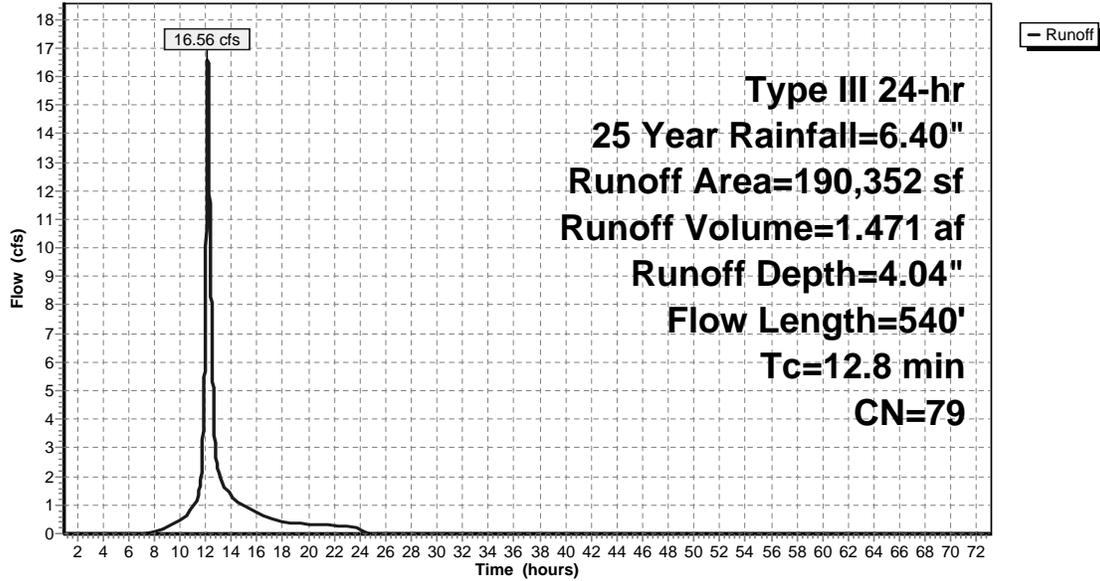
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Subcatchment 1Sa: Off-Site

Hydrograph



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Hydrograph for Subcatchment 1Sa: Off-Site

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.06	0.00	0.00	36.00	6.40	4.04	0.00	71.00	6.40	4.04	0.00
2.00	0.13	0.00	0.00	37.00	6.40	4.04	0.00	72.00	6.40	4.04	0.00
3.00	0.20	0.00	0.00	38.00	6.40	4.04	0.00	73.00	6.40	4.04	0.00
4.00	0.28	0.00	0.00	39.00	6.40	4.04	0.00				
5.00	0.36	0.00	0.00	40.00	6.40	4.04	0.00				
6.00	0.46	0.00	0.00	41.00	6.40	4.04	0.00				
7.00	0.58	0.00	0.01	42.00	6.40	4.04	0.00				
8.00	0.73	0.01	0.08	43.00	6.40	4.04	0.00				
9.00	0.93	0.05	0.22	44.00	6.40	4.04	0.00				
10.00	1.21	0.14	0.45	45.00	6.40	4.04	0.00				
11.00	1.60	0.31	0.90	46.00	6.40	4.04	0.00				
12.00	3.20	1.34	7.55	47.00	6.40	4.04	0.00				
13.00	4.80	2.63	2.19	48.00	6.40	4.04	0.00				
14.00	5.19	2.97	1.31	49.00	6.40	4.04	0.00				
15.00	5.47	3.21	0.98	50.00	6.40	4.04	0.00				
16.00	5.67	3.39	0.70	51.00	6.40	4.04	0.00				
17.00	5.82	3.52	0.55	52.00	6.40	4.04	0.00				
18.00	5.94	3.63	0.43	53.00	6.40	4.04	0.00				
19.00	6.04	3.71	0.37	54.00	6.40	4.04	0.00				
20.00	6.12	3.79	0.34	55.00	6.40	4.04	0.00				
21.00	6.20	3.86	0.31	56.00	6.40	4.04	0.00				
22.00	6.28	3.93	0.28	57.00	6.40	4.04	0.00				
23.00	6.34	3.99	0.25	58.00	6.40	4.04	0.00				
24.00	6.40	4.04	0.22	59.00	6.40	4.04	0.00				
25.00	6.40	4.04	0.00	60.00	6.40	4.04	0.00				
26.00	6.40	4.04	0.00	61.00	6.40	4.04	0.00				
27.00	6.40	4.04	0.00	62.00	6.40	4.04	0.00				
28.00	6.40	4.04	0.00	63.00	6.40	4.04	0.00				
29.00	6.40	4.04	0.00	64.00	6.40	4.04	0.00				
30.00	6.40	4.04	0.00	65.00	6.40	4.04	0.00				
31.00	6.40	4.04	0.00	66.00	6.40	4.04	0.00				
32.00	6.40	4.04	0.00	67.00	6.40	4.04	0.00				
33.00	6.40	4.04	0.00	68.00	6.40	4.04	0.00				
34.00	6.40	4.04	0.00	69.00	6.40	4.04	0.00				
35.00	6.40	4.04	0.00	70.00	6.40	4.04	0.00				

**1817-Basin Repair 2024**

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Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 25 Year Rainfall=6.40"

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**Summary for Subcatchment 3S: Off-Site East**

Runoff = 1.92 cfs @ 12.09 hrs, Volume= 0.137 af, Depth= 3.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25 Year Rainfall=6.40"

Area (sf)	CN	Description
11,216	70	Woods, Good, HSG C
10,271	74	>75% Grass cover, Good, HSG C
21,487	72	Weighted Average
21,487		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

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Proposed Basin Repair Analysis for, 2-, 10-, 25-, 100-Year Storms

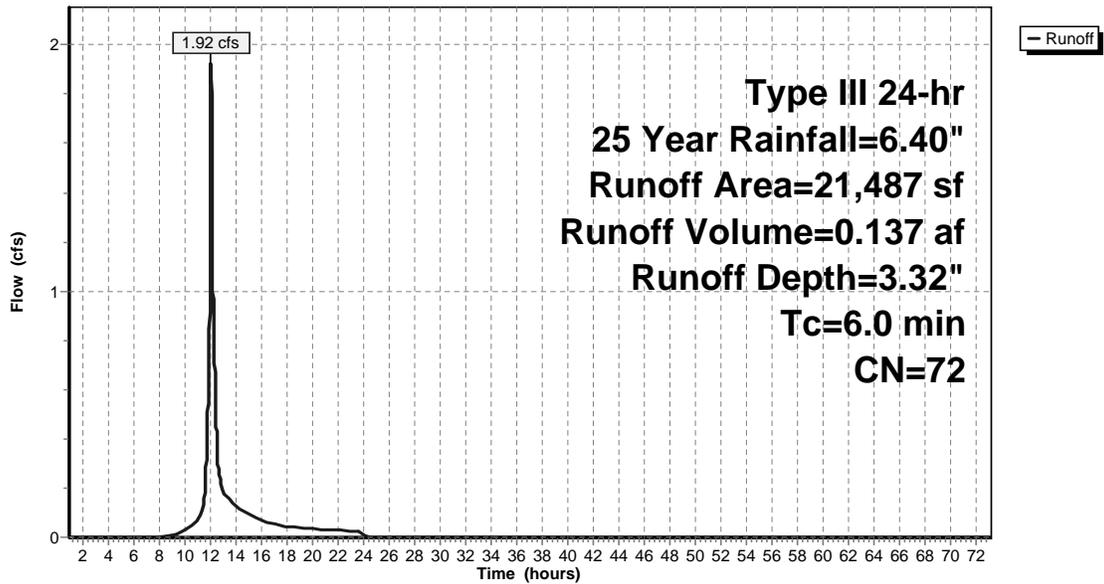
Type III 24-hr 25 Year Rainfall=6.40"

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**Subcatchment 3S: Off-Site East**

**Hydrograph**



**1817-Basin Repair 2024**

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**Hydrograph for Subcatchment 3S: Off-Site East**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.06	0.00	0.00	36.00	6.40	3.32	0.00	71.00	6.40	3.32	0.00
2.00	0.13	0.00	0.00	37.00	6.40	3.32	0.00	72.00	6.40	3.32	0.00
3.00	0.20	0.00	0.00	38.00	6.40	3.32	0.00	73.00	6.40	3.32	0.00
4.00	0.28	0.00	0.00	39.00	6.40	3.32	0.00				
5.00	0.36	0.00	0.00	40.00	6.40	3.32	0.00				
6.00	0.46	0.00	0.00	41.00	6.40	3.32	0.00				
7.00	0.58	0.00	0.00	42.00	6.40	3.32	0.00				
8.00	0.73	0.00	0.00	43.00	6.40	3.32	0.00				
9.00	0.93	0.01	0.01	44.00	6.40	3.32	0.00				
10.00	1.21	0.04	0.03	45.00	6.40	3.32	0.00				
11.00	1.60	0.14	0.07	46.00	6.40	3.32	0.00				
12.00	3.20	0.93	<b>1.10</b>	47.00	6.40	3.32	0.00				
13.00	4.80	2.05	<b>0.20</b>	48.00	6.40	3.32	0.00				
14.00	5.19	2.35	0.13	49.00	6.40	3.32	0.00				
15.00	5.47	2.56	0.10	50.00	6.40	3.32	0.00				
16.00	5.67	2.73	0.07	51.00	6.40	3.32	0.00				
17.00	5.82	2.85	0.06	52.00	6.40	3.32	0.00				
18.00	5.94	2.94	0.04	53.00	6.40	3.32	0.00				
19.00	6.04	3.02	0.04	54.00	6.40	3.32	0.00				
20.00	6.12	3.10	0.03	55.00	6.40	3.32	0.00				
21.00	6.20	3.16	0.03	56.00	6.40	3.32	0.00				
22.00	6.28	3.22	0.03	57.00	6.40	3.32	0.00				
23.00	6.34	3.28	0.03	58.00	6.40	3.32	0.00				
24.00	<b>6.40</b>	<b>3.32</b>	0.02	59.00	6.40	3.32	0.00				
25.00	6.40	3.32	0.00	60.00	6.40	3.32	0.00				
26.00	6.40	3.32	0.00	61.00	6.40	3.32	0.00				
27.00	6.40	3.32	0.00	62.00	6.40	3.32	0.00				
28.00	6.40	3.32	0.00	63.00	6.40	3.32	0.00				
29.00	6.40	3.32	0.00	64.00	6.40	3.32	0.00				
30.00	6.40	3.32	0.00	65.00	6.40	3.32	0.00				
31.00	6.40	3.32	0.00	66.00	6.40	3.32	0.00				
32.00	6.40	3.32	0.00	67.00	6.40	3.32	0.00				
33.00	6.40	3.32	0.00	68.00	6.40	3.32	0.00				
34.00	6.40	3.32	0.00	69.00	6.40	3.32	0.00				
35.00	6.40	3.32	0.00	70.00	6.40	3.32	0.00				

**1817-Basin Repair 2024**

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**Summary for Subcatchment 3Sa: Off-Site East**

Runoff = 9.04 cfs @ 12.12 hrs, Volume= 0.712 af, Depth= 4.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25 Year Rainfall=6.40"

Area (sf)	CN	Description
53,364	74	>75% Grass cover, Good, HSG C
26,882	98	Water Surface, HSG C
<b>*</b> 3,160	96	Gravel Road
83,406	83	Weighted Average
56,524		67.77% Pervious Area
26,882		32.23% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	50	0.0280	0.16		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.00"
0.4	82	0.0316	3.61		<b>Shallow Concentrated Flow, Shallow Conc. Flow</b> Paved Kv= 20.3 fps
3.1	234	0.0317	1.25		<b>Shallow Concentrated Flow, Shallow Conc Flow</b> Short Grass Pasture Kv= 7.0 fps
8.6	366	Total			

**1817-Basin Repair 2024**

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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

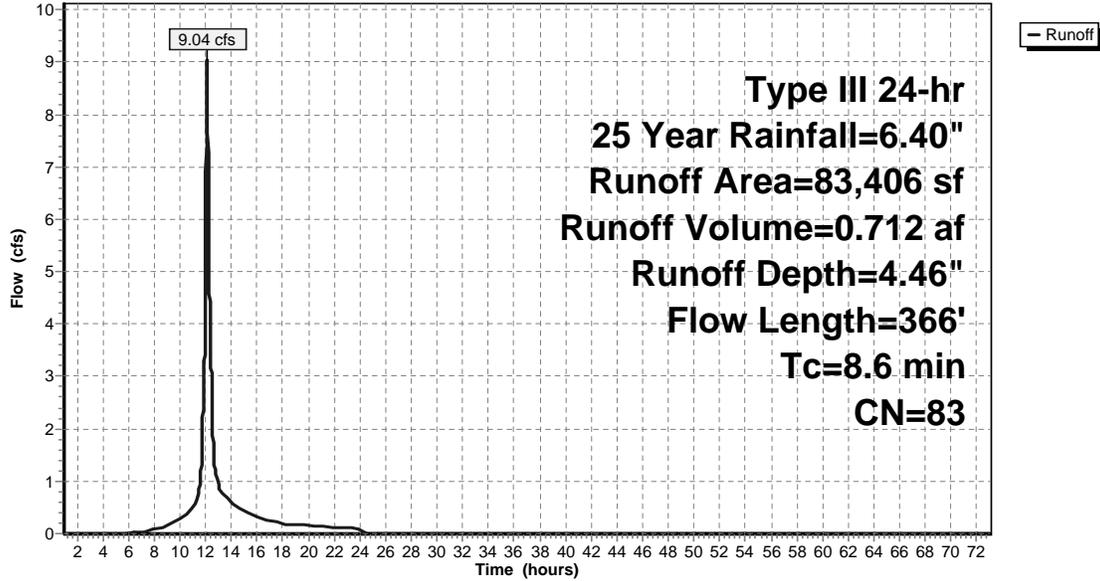
Type III 24-hr 25 Year Rainfall=6.40"

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**Subcatchment 3Sa: Off-Site East**

**Hydrograph**



**1817-Basin Repair 2024**

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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 25 Year Rainfall=6.40"

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**Hydrograph for Subcatchment 3Sa: Off-Site East**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.06	0.00	0.00	36.00	6.40	4.46	0.00	71.00	6.40	4.46	0.00
2.00	0.13	0.00	0.00	37.00	6.40	4.46	0.00	72.00	6.40	4.46	0.00
3.00	0.20	0.00	0.00	38.00	6.40	4.46	0.00	73.00	6.40	4.46	0.00
4.00	0.28	0.00	0.00	39.00	6.40	4.46	0.00				
5.00	0.36	0.00	0.00	40.00	6.40	4.46	0.00				
6.00	0.46	0.00	0.01	41.00	6.40	4.46	0.00				
7.00	0.58	0.01	0.03	42.00	6.40	4.46	0.00				
8.00	0.73	0.04	0.07	43.00	6.40	4.46	0.00				
9.00	0.93	0.11	0.16	44.00	6.40	4.46	0.00				
10.00	1.21	0.22	0.27	45.00	6.40	4.46	0.00				
11.00	1.60	0.44	0.50	46.00	6.40	4.46	0.00				
12.00	3.20	1.61	4.75	47.00	6.40	4.46	0.00				
13.00	4.80	2.99	9.94	48.00	6.40	4.46	0.00				
14.00	5.19	3.35	0.59	49.00	6.40	4.46	0.00				
15.00	5.47	3.60	0.44	50.00	6.40	4.46	0.00				
16.00	5.67	3.79	0.31	51.00	6.40	4.46	0.00				
17.00	5.82	3.93	0.25	52.00	6.40	4.46	0.00				
18.00	5.94	4.03	0.19	53.00	6.40	4.46	0.00				
19.00	6.04	4.13	0.17	54.00	6.40	4.46	0.00				
20.00	6.12	4.21	0.15	55.00	6.40	4.46	0.00				
21.00	6.20	4.28	0.14	56.00	6.40	4.46	0.00				
22.00	6.28	4.35	0.13	57.00	6.40	4.46	0.00				
23.00	6.34	4.41	0.11	58.00	6.40	4.46	0.00				
24.00	6.40	4.46	0.10	59.00	6.40	4.46	0.00				
25.00	6.40	4.46	0.00	60.00	6.40	4.46	0.00				
26.00	6.40	4.46	0.00	61.00	6.40	4.46	0.00				
27.00	6.40	4.46	0.00	62.00	6.40	4.46	0.00				
28.00	6.40	4.46	0.00	63.00	6.40	4.46	0.00				
29.00	6.40	4.46	0.00	64.00	6.40	4.46	0.00				
30.00	6.40	4.46	0.00	65.00	6.40	4.46	0.00				
31.00	6.40	4.46	0.00	66.00	6.40	4.46	0.00				
32.00	6.40	4.46	0.00	67.00	6.40	4.46	0.00				
33.00	6.40	4.46	0.00	68.00	6.40	4.46	0.00				
34.00	6.40	4.46	0.00	69.00	6.40	4.46	0.00				
35.00	6.40	4.46	0.00	70.00	6.40	4.46	0.00				

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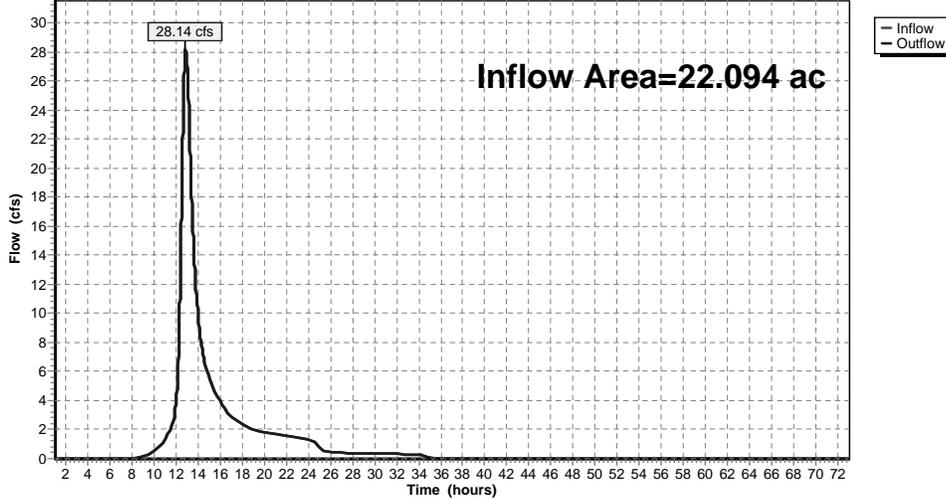
**Summary for Reach DP-1: (new Reach)**

Inflow Area = 22.094 ac, 3.96% Impervious, Inflow Depth = 3.17" for 25 Year event  
 Inflow = 28.14 cfs @ 12.82 hrs, Volume= 5.832 af  
 Outflow = 28.14 cfs @ 12.82 hrs, Volume= 5.832 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-1: (new Reach)**

Hydrograph



**1817-Basin Repair 2024**

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**Hydrograph for Reach DP-1: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.01		0.01	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.00		0.00	42.00	0.00		0.00				
8.00	0.01		0.01	43.00	0.00		0.00				
9.00	0.12		0.12	44.00	0.00		0.00				
10.00	0.53		0.53	45.00	0.00		0.00				
11.00	1.38		1.38	46.00	0.00		0.00				
12.00	<b>4.24</b>		<b>4.24</b>	47.00	0.00		0.00				
13.00	<b>26.70</b>		<b>26.70</b>	48.00	0.00		0.00				
14.00	9.57		9.57	49.00	0.00		0.00				
15.00	5.47		5.47	50.00	0.00		0.00				
16.00	3.90		3.90	51.00	0.00		0.00				
17.00	2.89		2.89	52.00	0.00		0.00				
18.00	2.37		2.37	53.00	0.00		0.00				
19.00	1.97		1.97	54.00	0.00		0.00				
20.00	1.79		1.79	55.00	0.00		0.00				
21.00	1.66		1.66	56.00	0.00		0.00				
22.00	1.55		1.55	57.00	0.00		0.00				
23.00	1.44		1.44	58.00	0.00		0.00				
24.00	1.33		1.33	59.00	0.00		0.00				
25.00	0.74		0.74	60.00	0.00		0.00				
26.00	0.44		0.44	61.00	0.00		0.00				
27.00	0.40		0.40	62.00	0.00		0.00				
28.00	0.38		0.38	63.00	0.00		0.00				
29.00	0.37		0.37	64.00	0.00		0.00				
30.00	0.35		0.35	65.00	0.00		0.00				
31.00	0.34		0.34	66.00	0.00		0.00				
32.00	0.32		0.32	67.00	0.00		0.00				
33.00	0.29		0.29	68.00	0.00		0.00				
34.00	0.25		0.25	69.00	0.00		0.00				
35.00	0.11		0.11	70.00	0.00		0.00				

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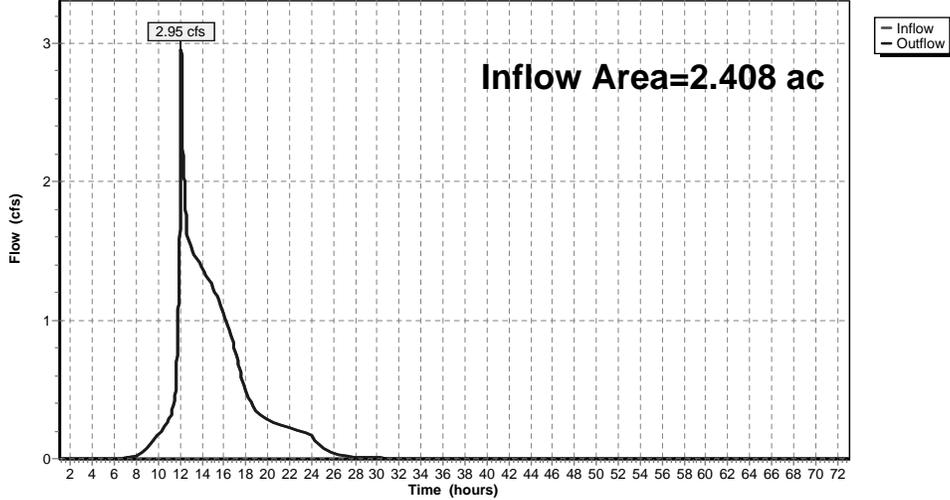
**Summary for Reach DP-3: (new Reach)**

Inflow Area = 2.408 ac, 25.63% Impervious, Inflow Depth = 4.23" for 25 Year event  
 Inflow = 2.95 cfs @ 12.10 hrs, Volume= 0.849 af  
 Outflow = 2.95 cfs @ 12.10 hrs, Volume= 0.849 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-3: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-3: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.00		0.00	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.00		0.00	42.00	0.00		0.00				
8.00	0.02		0.02	43.00	0.00		0.00				
9.00	0.08		0.08	44.00	0.00		0.00				
10.00	0.17		0.17	45.00	0.00		0.00				
11.00	0.29		0.29	46.00	0.00		0.00				
12.00	<b>1.95</b>		<b>1.95</b>	47.00	0.00		0.00				
13.00	<b>1.52</b>		<b>1.52</b>	48.00	0.00		0.00				
14.00	1.37		1.37	49.00	0.00		0.00				
15.00	1.23		1.23	50.00	0.00		0.00				
16.00	1.03		1.03	51.00	0.00		0.00				
17.00	0.79		0.79	52.00	0.00		0.00				
18.00	0.49		0.49	53.00	0.00		0.00				
19.00	0.34		0.34	54.00	0.00		0.00				
20.00	0.28		0.28	55.00	0.00		0.00				
21.00	0.25		0.25	56.00	0.00		0.00				
22.00	0.23		0.23	57.00	0.00		0.00				
23.00	0.20		0.20	58.00	0.00		0.00				
24.00	0.17		0.17	59.00	0.00		0.00				
25.00	0.08		0.08	60.00	0.00		0.00				
26.00	0.04		0.04	61.00	0.00		0.00				
27.00	0.02		0.02	62.00	0.00		0.00				
28.00	0.01		0.01	63.00	0.00		0.00				
29.00	0.01		0.01	64.00	0.00		0.00				
30.00	0.01		0.01	65.00	0.00		0.00				
31.00	0.00		0.00	66.00	0.00		0.00				
32.00	0.00		0.00	67.00	0.00		0.00				
33.00	0.00		0.00	68.00	0.00		0.00				
34.00	0.00		0.00	69.00	0.00		0.00				
35.00	0.00		0.00	70.00	0.00		0.00				

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**Summary for Pond P1A: Pond 1a (Pond Repair)**

Inflow Area = 4.370 ac, 20.04% Impervious, Inflow Depth = 4.04" for 25 Year event  
 Inflow = 16.56 cfs @ 12.17 hrs, Volume= 1.471 af  
 Outflow = 2.57 cfs @ 12.86 hrs, Volume= 1.471 af, Atten= 84%, Lag= 41.1 min  
 Discarded = 0.29 cfs @ 12.86 hrs, Volume= 0.401 af  
 Primary = 0.48 cfs @ 12.86 hrs, Volume= 0.843 af  
 Secondary = 1.80 cfs @ 12.86 hrs, Volume= 0.227 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 78.84' @ 12.86 hrs Surf.Area= 26,159 sf Storage= 31,721 cf

Plug-Flow detention time= 386.6 min calculated for 1.471 af (100% of inflow)  
 Center-of-Mass det. time= 386.5 min ( 1,206.8 - 820.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	75.50'	1,242 cf	<b>Custom Stage Data (Irregular)</b> Listed below 3,106 cf Overall x 40.0% Voids
#2	76.50'	37,823 cf	<b>Custom Stage Data (Irregular)</b> Listed below 39,065 cf Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
75.50	3,106	220.0	0	0	3,106
76.00	3,106	220.0	1,553	1,553	3,216
76.50	3,106	220.0	1,553	3,106	3,326

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.50	3,106	220.0	0	0	3,106
77.00	6,731	331.0	2,402	2,402	7,975
78.00	15,313	639.8	10,732	13,134	31,836
79.20	26,330	782.0	24,689	37,823	47,947

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Device	Routing	Invert	Outlet Devices
#1	Secondary	78.70'	<b>14.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	75.50'	<b>0.270 in/hr Exfiltration over Wetted area</b>
#3	Primary	75.50'	<b>4.0" Round Culvert</b> L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 75.50' / 75.10' S= 0.0100 ' S= 0.0100 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.29 cfs @ 12.86 hrs HW=78.84' (Free Discharge)  
 ↳ **2=Exfiltration** (Exfiltration Controls 0.29 cfs)

**Primary OutFlow** Max=0.48 cfs @ 12.86 hrs HW=78.84' (Free Discharge)  
 ↳ **3=Culvert** (Barrel Controls 0.48 cfs @ 5.47 fps)

**Secondary OutFlow** Max=1.79 cfs @ 12.86 hrs HW=78.84' (Free Discharge)  
 ↳ **1=Broad-Crested Rectangular Weir** (Weir Controls 1.79 cfs @ 0.90 fps)

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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

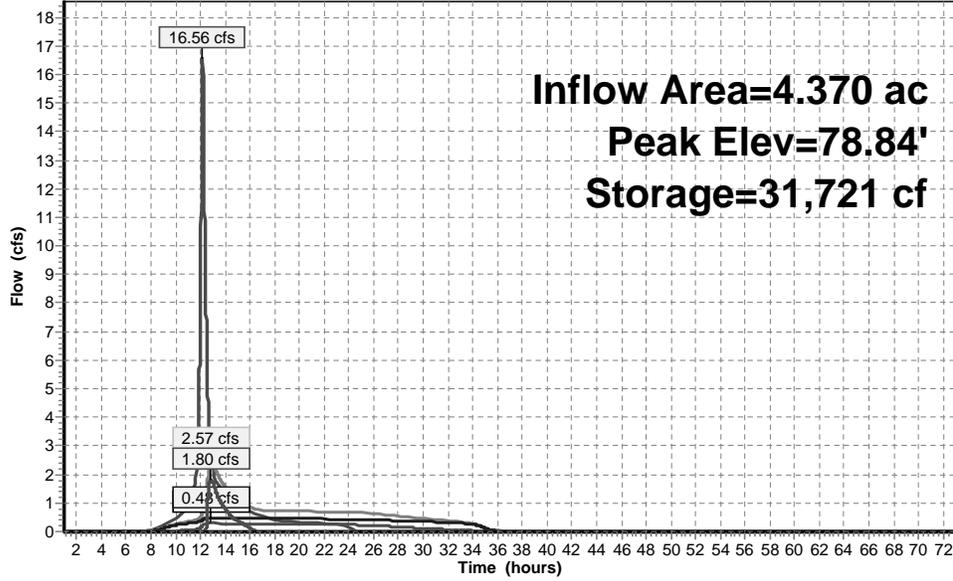
Type III 24-hr 25 Year Rainfall=6.40"

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Pond P1A: Pond 1a (Pond Repair)

Hydrograph



- Inflow
- Outflow
- Discarded
- Primary
- Secondary

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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

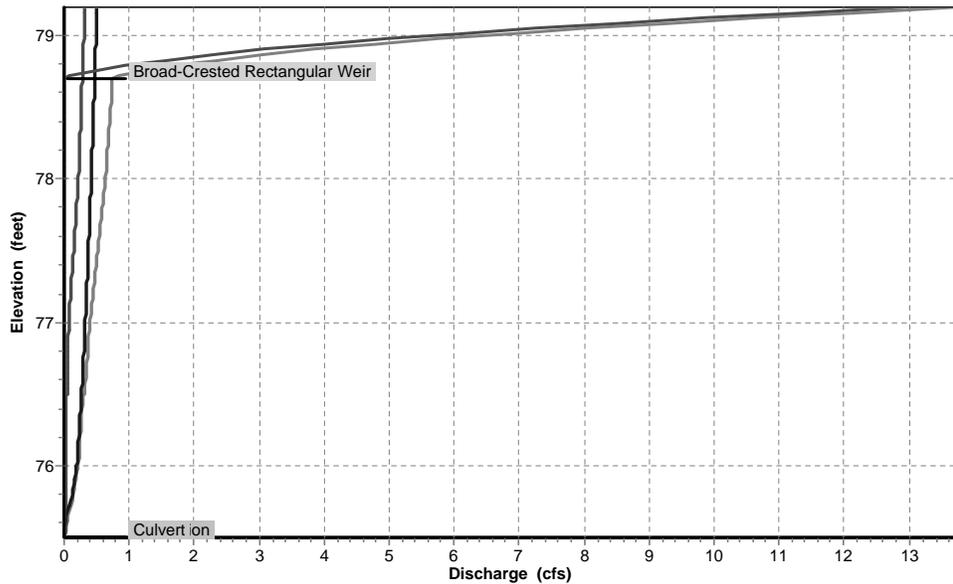
Type III 24-hr 25 Year Rainfall=6.40"

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Pond P1A: Pond 1a (Pond Repair)

Stage-Discharge



- Total
- Discarded
- Primary
- Secondary

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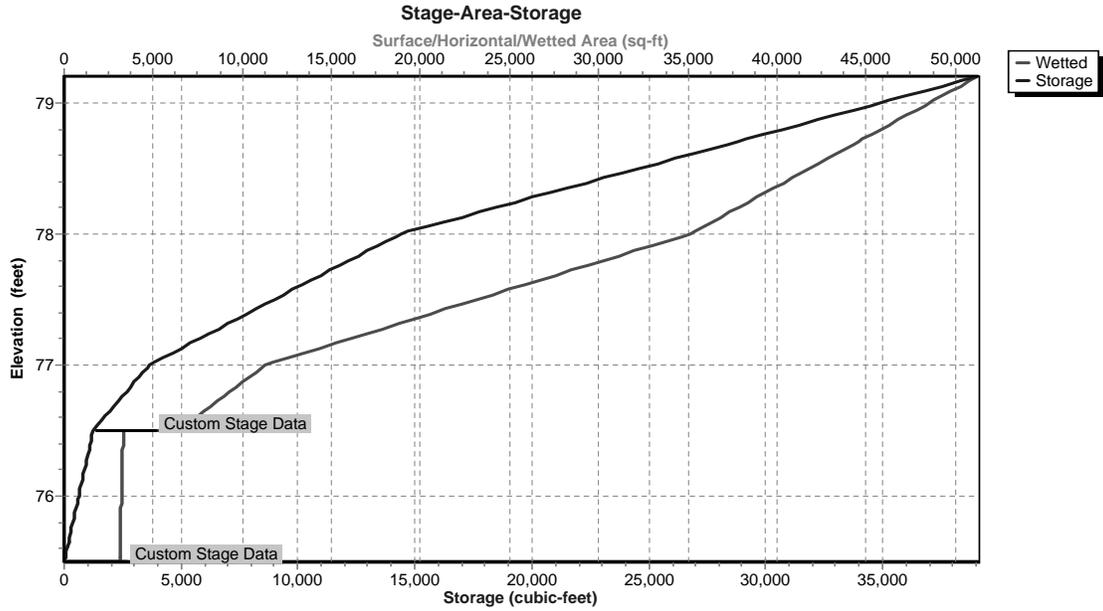
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 25 Year Rainfall=6.40"

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**Pond P1A: Pond 1a (Pond Repair)**



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Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 25 Year Rainfall=6.40"

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**Hydrograph for Pond P1A: Pond 1a (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
1.00	0.00	0	75.50	0.00	0.00	0.00	0.00
6.00	0.00	0	75.50	0.00	0.00	0.00	0.00
11.00	<b>0.90</b>	<b>2,111</b>	<b>76.68</b>	<b>0.34</b>	<b>0.05</b>	<b>0.29</b>	<b>0.00</b>
16.00	<b>0.70</b>	<b>29,234</b>	<b>78.72</b>	<b>0.87</b>	<b>0.28</b>	<b>0.47</b>	<b>0.12</b>
21.00	0.31	23,741	78.46	0.71	0.26	0.45	0.00
26.00	0.00	14,588	78.01	0.64	0.22	0.42	0.00
31.00	0.00	5,089	77.13	0.43	0.09	0.34	0.00
36.00	0.00	108	75.59	0.03	0.02	0.01	0.00
41.00	0.00	0	75.50	0.00	0.00	0.00	0.00
46.00	0.00	0	75.50	0.00	0.00	0.00	0.00
51.00	0.00	0	75.50	0.00	0.00	0.00	0.00
56.00	0.00	0	75.50	0.00	0.00	0.00	0.00
61.00	0.00	0	75.50	0.00	0.00	0.00	0.00
66.00	0.00	0	75.50	0.00	0.00	0.00	0.00
71.00	0.00	0	75.50	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
75.50	0.00	0.00	0.00	0.00	79.00	6.41	0.30	0.49	5.61
75.60	0.04	0.02	0.02	0.00	79.10	9.70	0.31	0.50	8.89
75.70	0.09	0.02	0.07	0.00	79.20	<b>13.72</b>	<b>0.32</b>	<b>0.50</b>	<b>12.89</b>
75.80	0.14	0.02	0.12	0.00					
75.90	0.18	0.02	0.16	0.00					
76.00	0.21	0.02	0.19	0.00					
76.10	0.23	0.02	0.21	0.00					
76.20	0.25	0.02	0.23	0.00					
76.30	0.26	0.02	0.24	0.00					
76.40	0.27	0.02	0.25	0.00					
76.50	0.31	0.04	0.27	0.00					
76.60	0.33	0.05	0.28	0.00					
76.70	0.34	0.05	0.29	0.00					
76.80	0.36	0.06	0.30	0.00					
76.90	0.38	0.06	0.31	0.00					
77.00	0.39	0.07	0.32	0.00					
77.10	0.42	0.09	0.33	0.00					
77.20	0.44	0.10	0.34	0.00					
77.30	0.47	0.12	0.35	0.00					
77.40	0.49	0.13	0.36	0.00					
77.50	0.52	0.15	0.37	0.00					
77.60	0.54	0.16	0.38	0.00					
77.70	0.56	0.18	0.39	0.00					
77.80	0.59	0.19	0.40	0.00					
77.90	0.61	0.20	0.41	0.00					
78.00	0.63	0.22	0.41	0.00					
78.10	0.65	0.23	0.42	0.00					
78.20	0.67	0.24	0.43	0.00					
78.30	0.68	0.24	0.44	0.00					
78.40	0.70	0.25	0.45	0.00					
78.50	0.71	0.26	0.45	0.00					
78.60	0.73	0.27	0.46	0.00					
78.70	0.75	0.28	0.47	0.00					
78.80	1.81	0.29	0.47	1.05					
78.90	3.74	0.30	0.48	2.97					

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**Stage-Area-Storage for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)
75.50	3,106	0	77.25	17,266	6,327	79.00	48,588	34,950
75.55	3,117	62	77.30	18,459	6,864	79.05	49,260	35,979
75.60	3,128	124	77.35	19,652	7,400	79.10	49,931	37,008
75.65	3,139	186	77.40	20,845	7,937	79.15	50,602	38,036
75.70	3,150	248	77.45	22,038	8,473	79.20	<b>51,273</b>	<b>39,065</b>
75.75	3,161	311	77.50	23,231	9,010			
75.80	3,172	373	77.55	24,424	9,547			
75.85	3,183	435	77.60	25,618	10,083			
75.90	3,194	497	77.65	26,811	10,620			
75.95	3,205	559	77.70	28,004	11,156			
76.00	3,216	621	77.75	29,197	11,693			
76.05	3,227	683	77.80	30,390	12,230			
76.10	3,238	745	77.85	31,583	12,766			
76.15	3,249	808	77.90	32,776	13,303			
76.20	3,260	870	77.95	33,969	13,839			
76.25	3,271	932	78.00	35,162	14,376			
76.30	3,282	994	78.05	35,833	15,405			
76.35	3,293	1,056	78.10	36,505	16,434			
76.40	3,304	1,118	78.15	37,176	17,462			
76.45	3,315	1,180	78.20	37,847	18,491			
76.50	6,432	1,242	78.25	38,518	19,520			
76.55	6,919	1,483	78.30	39,190	20,548			
76.60	7,406	1,723	78.35	39,861	21,577			
76.65	7,893	1,963	78.40	40,532	22,606			
76.70	8,380	2,203	78.45	41,204	23,634			
76.75	8,866	2,443	78.50	41,875	24,663			
76.80	9,353	2,683	78.55	42,546	25,692			
76.85	9,840	2,923	78.60	43,218	26,721			
76.90	10,327	3,164	78.65	43,889	27,749			
76.95	10,814	3,404	78.70	44,560	28,778			
77.00	11,301	3,644	78.75	45,232	29,807			
77.05	12,494	4,181	78.80	45,903	30,835			
77.10	13,687	4,717	78.85	46,574	31,864			
77.15	14,880	5,254	78.90	47,246	32,893			
77.20	16,073	5,790	78.95	47,917	33,922			

**1817-Basin Repair 2024**

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**Summary for Pond P3A: Pond 3A (Pond Repair)**

Inflow Area = 1.915 ac, 32.23% Impervious, Inflow Depth = 4.46" for 25 Year event  
 Inflow = 9.04 cfs @ 12.12 hrs, Volume= 0.712 af  
 Outflow = 1.33 cfs @ 12.69 hrs, Volume= 0.712 af, Atten= 85%, Lag= 34.1 min  
 Primary = 0.47 cfs @ 12.69 hrs, Volume= 0.383 af  
 Secondary = 0.86 cfs @ 12.69 hrs, Volume= 0.329 af  
 Tertiary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 77.86' @ 12.69 hrs Surf.Area= 15,649 sf Storage= 13,503 cf  
 Flood Elev= 79.50' Surf.Area= 25,484 sf Storage= 37,166 cf

Plug-Flow detention time= 130.8 min calculated for 0.712 af (100% of inflow)  
 Center-of-Mass det. time= 130.8 min ( 936.9 - 806.2 )

Volume	Invert	Avail.Storage	Storage Description		
#1	76.00'	37,166 cf	<b>Custom Stage Data (Irregular)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.00	2,053	339.0	0	0	2,053
77.00	6,709	559.0	4,158	4,158	17,781
78.00	17,458	791.4	11,663	15,821	42,764
79.00	25,484	883.5	21,345	37,166	55,068

Device	Routing	Invert	Outlet Devices
#1	Primary	76.00'	<b>4.0" Round 6" Culvert 1</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.00' / 75.52' S= 0.0240 1/8" Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Secondary	76.55'	<b>6.0" Round 6" Culvert 2</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.55' / 75.60' S= 0.0475 1/8" Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#3	Tertiary	78.50'	<b>20.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50

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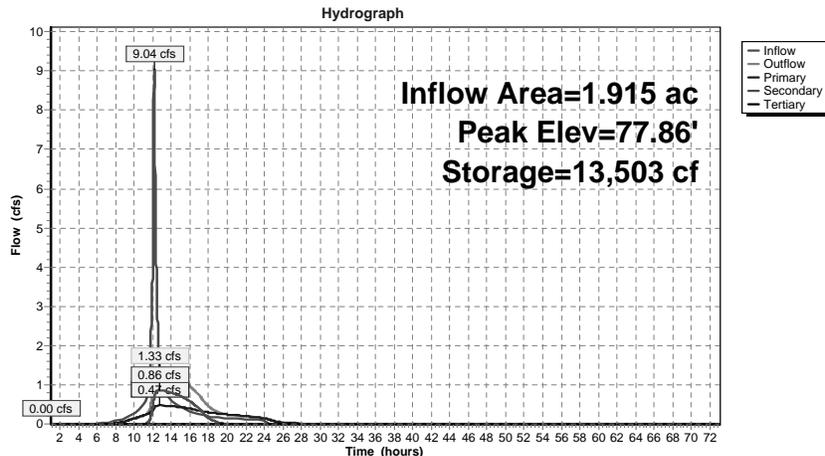
Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76  
 2.83

**Primary OutFlow** Max=0.47 cfs @ 12.69 hrs HW=77.86' (Free Discharge)  
 1=6" Culvert 1 (Barrel Controls 0.47 cfs @ 5.41 fps)

**Secondary OutFlow** Max=0.86 cfs @ 12.69 hrs HW=77.86' (Free Discharge)  
 2=6" Culvert 2 (Inlet Controls 0.86 cfs @ 4.37 fps)

**Tertiary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=76.00' (Free Discharge)  
 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Pond P3A: Pond 3A (Pond Repair)**



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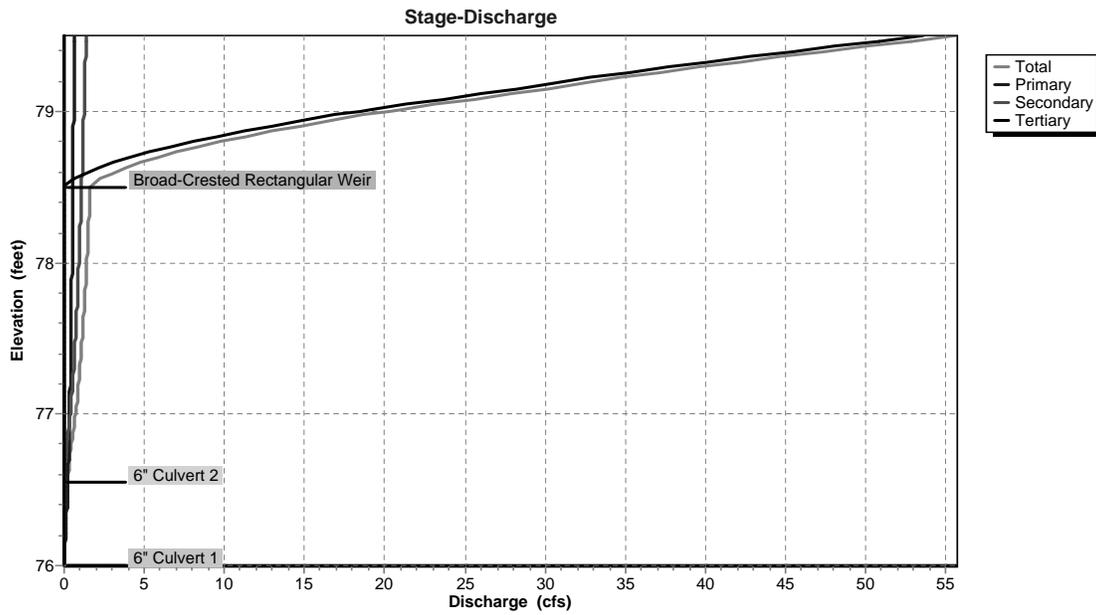
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 25 Year Rainfall=6.40"

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Pond P3A: Pond 3A (Pond Repair)



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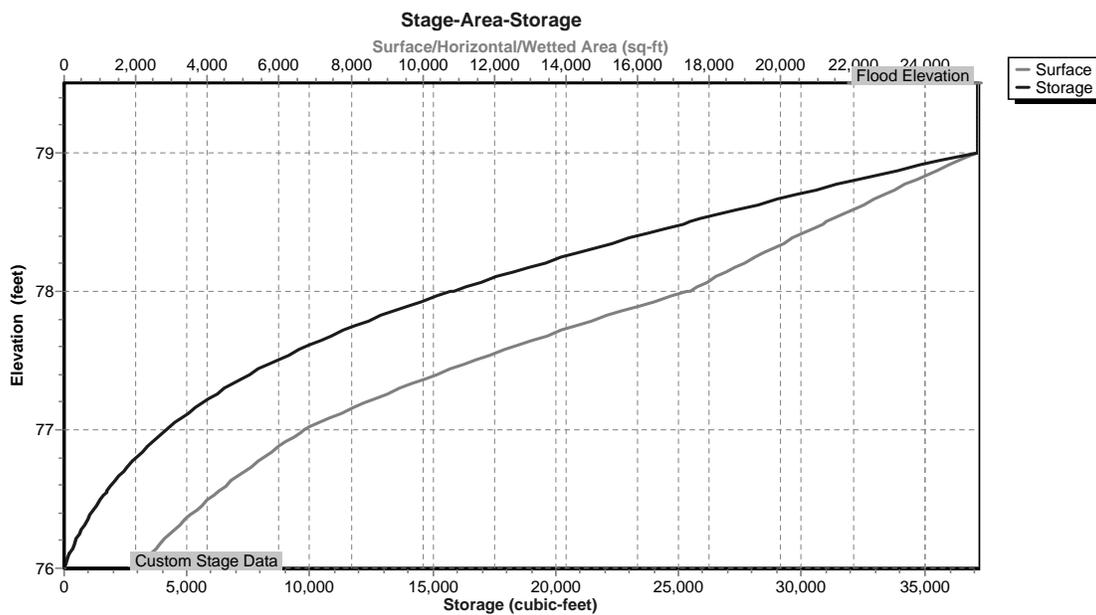
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 25 Year Rainfall=6.40"

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Pond P3A: Pond 3A (Pond Repair)



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**Hydrograph for Pond P3A: Pond 3A (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
1.00	0.00	0	76.00	0.00	0.00	0.00	<b>0.00</b>
6.00	0.01	5	76.00	0.00	0.00	0.00	0.00
11.00	<b>0.50</b>	<b>1,557</b>	<b>76.51</b>	<b>0.22</b>	<b>0.22</b>	<b>0.00</b>	0.00
16.00	<b>0.31</b>	<b>6,329</b>	<b>77.27</b>	<b>0.96</b>	<b>0.39</b>	<b>0.57</b>	0.00
21.00	0.14	1,566	76.52	0.22	0.22	0.00	0.00
26.00	0.00	304	76.13	0.04	0.04	0.00	0.00
31.00	0.00	84	76.04	0.00	0.00	0.00	0.00
36.00	0.00	42	76.02	0.00	0.00	0.00	0.00
41.00	0.00	22	76.01	0.00	0.00	0.00	0.00
46.00	0.00	11	76.01	0.00	0.00	0.00	0.00
51.00	0.00	6	76.00	0.00	0.00	0.00	0.00
56.00	0.00	3	76.00	0.00	0.00	0.00	0.00
61.00	0.00	2	76.00	0.00	0.00	0.00	0.00
66.00	0.00	1	76.00	0.00	0.00	0.00	0.00
71.00	0.00	0	76.00	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
76.00	0.00	0.00	0.00	0.00	79.50	<b>55.61</b>	<b>0.64</b>	<b>1.37</b>	<b>53.60</b>
76.10	0.02	0.02	0.00	0.00					
76.20	0.07	0.07	0.00	0.00					
76.30	0.14	0.14	0.00	0.00					
76.40	0.18	0.18	0.00	0.00					
76.50	0.21	0.21	0.00	0.00					
76.60	0.25	0.24	0.01	0.00					
76.70	0.33	0.27	0.06	0.00					
76.80	0.44	0.30	0.15	0.00					
76.90	0.58	0.32	0.26	0.00					
77.00	0.71	0.34	0.38	0.00					
77.10	0.82	0.36	0.46	0.00					
77.20	0.90	0.38	0.53	0.00					
77.30	0.98	0.39	0.59	0.00					
77.40	1.06	0.41	0.65	0.00					
77.50	1.13	0.43	0.70	0.00					
77.60	1.19	0.44	0.75	0.00					
77.70	1.24	0.45	0.79	0.00					
77.80	1.30	0.46	0.83	0.00					
77.90	1.35	0.48	0.87	0.00					
78.00	1.40	0.49	0.91	0.00					
78.10	1.45	0.50	0.95	0.00					
78.20	1.50	0.51	0.99	0.00					
78.30	1.54	0.52	1.02	0.00					
78.40	1.59	0.53	1.06	0.00					
78.50	1.63	0.54	1.09	0.00					
78.60	3.17	0.55	1.12	1.50					
78.70	5.95	0.56	1.15	4.24					
78.80	9.77	0.57	1.18	8.02					
78.90	14.49	0.58	1.21	12.70					
79.00	20.25	0.59	1.24	18.42					
79.10	26.96	0.60	1.27	25.10					
79.20	33.41	0.61	1.29	31.51					
79.30	40.29	0.62	1.32	38.35					
79.40	47.74	0.63	1.35	45.76					

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**Stage-Area-Storage for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
76.00	2,053	0	77.75	14,298	11,858	79.50	25,484	37,166
76.05	2,222	107	77.80	14,905	12,588			
76.10	2,398	222	77.85	15,524	13,349			
76.15	2,581	347	77.90	16,156	14,141			
76.20	2,770	481	77.95	16,801	14,964			
76.25	2,966	624	78.00	17,458	15,821			
76.30	3,169	777	78.05	17,823	16,703			
76.35	3,378	941	78.10	18,192	17,603			
76.40	3,594	1,115	78.15	18,565	18,522			
76.45	3,817	1,300	78.20	18,942	19,460			
76.50	4,046	1,497	78.25	19,323	20,417			
76.55	4,282	1,705	78.30	19,707	21,392			
76.60	4,525	1,925	78.35	20,095	22,387			
76.65	4,775	2,158	78.40	20,487	23,402			
76.70	5,031	2,403	78.45	20,882	24,436			
76.75	5,294	2,661	78.50	21,282	25,490			
76.80	5,563	2,932	78.55	21,685	26,564			
76.85	5,840	3,217	78.60	22,092	27,659			
76.90	6,123	3,516	78.65	22,503	28,774			
76.95	6,413	3,830	78.70	22,917	29,909			
77.00	6,709	4,158	78.75	23,336	31,065			
77.05	7,127	4,504	78.80	23,758	32,243			
77.10	7,557	4,871	78.85	24,184	33,441			
77.15	8,000	5,259	78.90	24,613	34,661			
77.20	8,455	5,671	78.95	25,047	35,903			
77.25	8,923	6,105	79.00	<b>25,484</b>	<b>37,166</b>			
77.30	9,404	6,563	79.05	25,484	37,166			
77.35	9,897	7,046	79.10	25,484	37,166			
77.40	10,403	7,553	79.15	25,484	37,166			
77.45	10,922	8,086	79.20	25,484	37,166			
77.50	11,453	8,646	79.25	25,484	37,166			
77.55	11,997	9,232	79.30	25,484	37,166			
77.60	12,553	9,846	79.35	25,484	37,166			
77.65	13,122	10,487	79.40	25,484	37,166			
77.70	13,704	11,158	79.45	25,484	37,166			

**1817-Basin Repair 2024**

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Time span=1.00-73.00 hrs, dt=0.01 hrs, 7201 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment 1S: Off-Site Northeast**

Runoff Area=772,071 sf 0.00% Impervious Runoff Depth=4.83"  
 Flow Length=1,645' Tc=61.7 min CN=71 Runoff=39.01 cfs 7.137 af

**Subcatchment 1Sa: Off-Site**

Runoff Area=190,352 sf 20.04% Impervious Runoff Depth=5.78"  
 Flow Length=540' Tc=12.8 min CN=79 Runoff=23.48 cfs 2.104 af

**Subcatchment 3S: Off-Site East**

Runoff Area=21,487 sf 0.00% Impervious Runoff Depth=4.95"  
 Tc=6.0 min CN=72 Runoff=2.86 cfs 0.203 af

**Subcatchment 3Sa: Off-Site East**

Runoff Area=83,406 sf 32.23% Impervious Runoff Depth=6.25"  
 Flow Length=366' Tc=8.6 min CN=83 Runoff=12.49 cfs 0.998 af

**Reach DP-1: (new Reach)**

Inflow=44.76 cfs 8.798 af  
 Outflow=44.76 cfs 8.798 af

**Reach DP-3: (new Reach)**

Inflow=4.07 cfs 1.201 af  
 Outflow=4.07 cfs 1.201 af

**Pond P1A: Pond 1a (Pond Repair)**

Peak Elev=79.12' Storage=37,356 cf Inflow=23.48 cfs 2.104 af  
 Discarded=0.31 cfs 0.443 af Primary=0.50 cfs 0.924 af Secondary=9.53 cfs 0.737 af Outflow=10.34 cfs 2.104 af

**Pond P3A: Pond 3A (Pond Repair)**

Peak Elev=78.22' Storage=19,761 cf Inflow=12.49 cfs 0.998 af  
 Primary=0.51 cfs 0.480 af Secondary=0.99 cfs 0.518 af Tertiary=0.00 cfs 0.000 af Outflow=1.50 cfs 0.998 af

**Total Runoff Area = 24.502 ac Runoff Volume = 10.443 af Average Runoff Depth = 5.11"**  
**93.91% Pervious = 23.009 ac 6.09% Impervious = 1.493 ac**

**1817-Basin Repair 2024**

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**Summary for Subcatchment 1S: Off-Site Northeast**

Runoff = 39.01 cfs @ 12.82 hrs, Volume= 7.137 af, Depth= 4.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100 Year Rainfall=8.29"

Area (sf)	CN	Description
650,962	70	Woods, Good, HSG C
115,309	74	>75% Grass cover, Good, HSG C
* 5,800	96	Gravel Road, HSG C
772,071	71	Weighted Average
772,071		100.00% Pervious Area

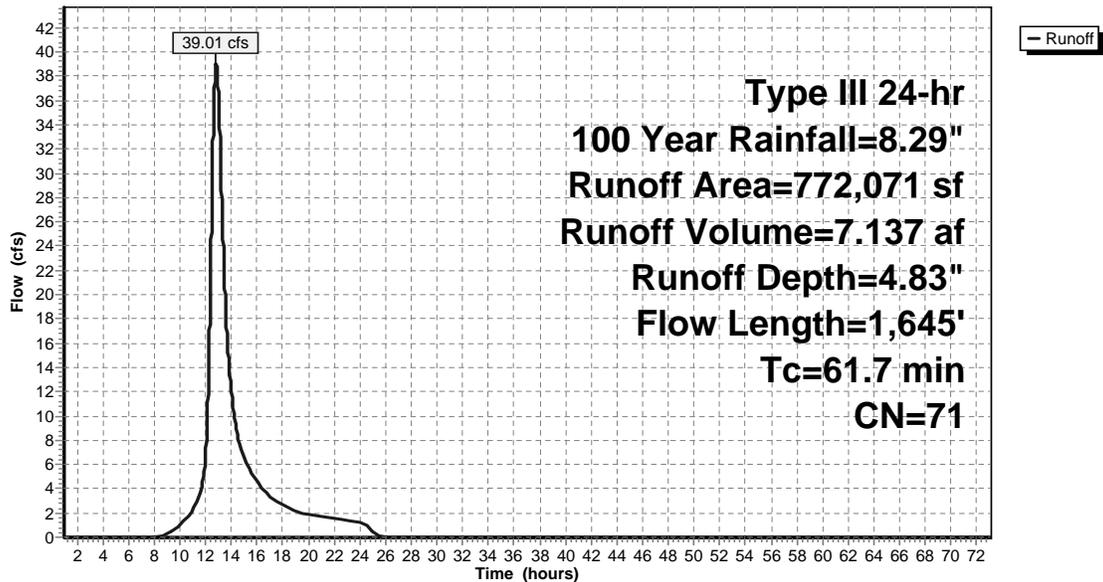
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
32.0	50	0.0080	0.03		<b>Sheet Flow,</b> Woods: Dense underbrush n= 0.800 P2= 3.00"
12.6	628	0.0276	0.83		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
3.3	496	0.0276	2.49		<b>Shallow Concentrated Flow,</b> Grassed Waterway Kv= 15.0 fps
13.8	471	0.0130	0.57		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
61.7	1,645	Total			

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**Subcatchment 1S: Off-Site Northeast**

**Hydrograph**



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**Hydrograph for Subcatchment 1S: Off-Site Northeast**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.08	0.00	0.00	36.00	8.29	4.83	0.00	71.00	8.29	4.83	0.00
2.00	0.17	0.00	0.00	37.00	8.29	4.83	0.00	72.00	8.29	4.83	0.00
3.00	0.25	0.00	0.00	38.00	8.29	4.83	0.00	73.00	8.29	4.83	0.00
4.00	0.36	0.00	0.00	39.00	8.29	4.83	0.00				
5.00	0.47	0.00	0.00	40.00	8.29	4.83	0.00				
6.00	0.60	0.00	0.00	41.00	8.29	4.83	0.00				
7.00	0.75	0.00	0.00	42.00	8.29	4.83	0.00				
8.00	0.95	0.00	0.01	43.00	8.29	4.83	0.00				
9.00	1.21	0.03	0.30	44.00	8.29	4.83	0.00				
10.00	1.57	0.12	1.02	45.00	8.29	4.83	0.00				
11.00	2.07	0.30	2.32	46.00	8.29	4.83	0.00				
12.00	4.14	1.49	<b>6.73</b>	47.00	8.29	4.83	0.00				
13.00	6.22	3.07	<b>36.56</b>	48.00	8.29	4.83	0.00				
14.00	6.72	3.49	11.94	49.00	8.29	4.83	0.00				
15.00	7.08	3.79	6.52	50.00	8.29	4.83	0.00				
16.00	7.34	4.02	4.64	51.00	8.29	4.83	0.00				
17.00	7.54	4.18	3.37	52.00	8.29	4.83	0.00				
18.00	7.69	4.31	2.65	53.00	8.29	4.83	0.00				
19.00	7.82	4.42	2.10	54.00	8.29	4.83	0.00				
20.00	7.93	4.52	1.85	55.00	8.29	4.83	0.00				
21.00	8.04	4.61	1.67	56.00	8.29	4.83	0.00				
22.00	8.13	4.69	1.52	57.00	8.29	4.83	0.00				
23.00	8.21	4.77	1.38	58.00	8.29	4.83	0.00				
24.00	<b>8.29</b>	<b>4.83</b>	1.24	59.00	8.29	4.83	0.00				
25.00	8.29	4.83	0.44	60.00	8.29	4.83	0.00				
26.00	8.29	4.83	0.04	61.00	8.29	4.83	0.00				
27.00	8.29	4.83	0.00	62.00	8.29	4.83	0.00				
28.00	8.29	4.83	0.00	63.00	8.29	4.83	0.00				
29.00	8.29	4.83	0.00	64.00	8.29	4.83	0.00				
30.00	8.29	4.83	0.00	65.00	8.29	4.83	0.00				
31.00	8.29	4.83	0.00	66.00	8.29	4.83	0.00				
32.00	8.29	4.83	0.00	67.00	8.29	4.83	0.00				
33.00	8.29	4.83	0.00	68.00	8.29	4.83	0.00				
34.00	8.29	4.83	0.00	69.00	8.29	4.83	0.00				
35.00	8.29	4.83	0.00	70.00	8.29	4.83	0.00				

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**Summary for Subcatchment 1Sa: Off-Site**

Runoff = 23.48 cfs @ 12.17 hrs, Volume= 2.104 af, Depth= 5.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100 Year Rainfall=8.29"

Area (sf)	CN	Description
152,204	74	>75% Grass cover, Good, HSG C
* 9,937	98	Gravel Road, HSG C
27,571	98	Water Surface, HSG C
* 640	98	Equipment Pad, HSG C
190,352	79	Weighted Average
152,204		79.96% Pervious Area
38,148		20.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	50	0.0380	0.19		<b>Sheet Flow,</b> Grass: Short n=0.150 P2= 3.00"
8.3	490	0.0196	0.98		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
12.8	540	Total			

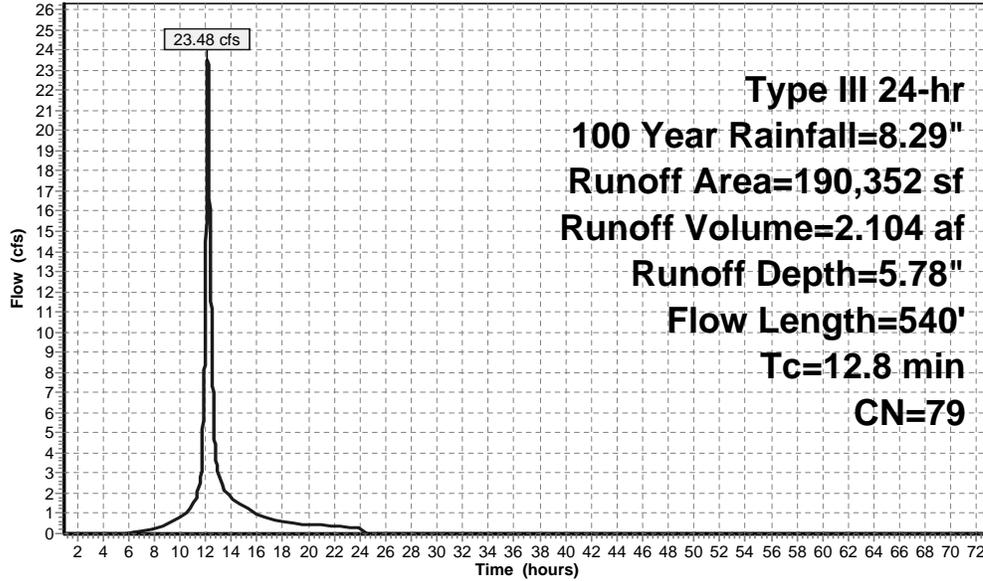
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Subcatchment 1Sa: Off-Site

Hydrograph



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Hydrograph for Subcatchment 1Sa: Off-Site

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.08	0.00	0.00	36.00	8.29	5.78	0.00	71.00	8.29	5.78	0.00
2.00	0.17	0.00	0.00	37.00	8.29	5.78	0.00	72.00	8.29	5.78	0.00
3.00	0.25	0.00	0.00	38.00	8.29	5.78	0.00	73.00	8.29	5.78	0.00
4.00	0.36	0.00	0.00	39.00	8.29	5.78	0.00				
5.00	0.47	0.00	0.00	40.00	8.29	5.78	0.00				
6.00	0.60	0.00	0.02	41.00	8.29	5.78	0.00				
7.00	0.75	0.02	0.09	42.00	8.29	5.78	0.00				
8.00	0.95	0.06	0.21	43.00	8.29	5.78	0.00				
9.00	1.21	0.14	0.44	44.00	8.29	5.78	0.00				
10.00	1.57	0.29	0.78	45.00	8.29	5.78	0.00				
11.00	2.07	0.57	1.44	46.00	8.29	5.78	0.00				
12.00	4.14	2.08	11.04	47.00	8.29	5.78	0.00				
13.00	6.22	3.87	3.00	48.00	8.29	5.78	0.00				
14.00	6.72	4.33	1.78	49.00	8.29	5.78	0.00				
15.00	7.08	4.66	1.33	50.00	8.29	5.78	0.00				
16.00	7.34	4.90	0.95	51.00	8.29	5.78	0.00				
17.00	7.54	5.08	0.74	52.00	8.29	5.78	0.00				
18.00	7.69	5.22	0.57	53.00	8.29	5.78	0.00				
19.00	7.82	5.34	0.50	54.00	8.29	5.78	0.00				
20.00	7.93	5.45	0.45	55.00	8.29	5.78	0.00				
21.00	8.04	5.54	0.41	56.00	8.29	5.78	0.00				
22.00	8.13	5.63	0.37	57.00	8.29	5.78	0.00				
23.00	8.21	5.71	0.34	58.00	8.29	5.78	0.00				
24.00	8.29	5.78	0.30	59.00	8.29	5.78	0.00				
25.00	8.29	5.78	0.00	60.00	8.29	5.78	0.00				
26.00	8.29	5.78	0.00	61.00	8.29	5.78	0.00				
27.00	8.29	5.78	0.00	62.00	8.29	5.78	0.00				
28.00	8.29	5.78	0.00	63.00	8.29	5.78	0.00				
29.00	8.29	5.78	0.00	64.00	8.29	5.78	0.00				
30.00	8.29	5.78	0.00	65.00	8.29	5.78	0.00				
31.00	8.29	5.78	0.00	66.00	8.29	5.78	0.00				
32.00	8.29	5.78	0.00	67.00	8.29	5.78	0.00				
33.00	8.29	5.78	0.00	68.00	8.29	5.78	0.00				
34.00	8.29	5.78	0.00	69.00	8.29	5.78	0.00				
35.00	8.29	5.78	0.00	70.00	8.29	5.78	0.00				

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**Summary for Subcatchment 3S: Off-Site East**

Runoff = 2.86 cfs @ 12.09 hrs, Volume= 0.203 af, Depth= 4.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100 Year Rainfall=8.29"

Area (sf)	CN	Description
11,216	70	Woods, Good, HSG C
10,271	74	>75% Grass cover, Good, HSG C
21,487	72	Weighted Average
21,487		100.00% Pervious Area

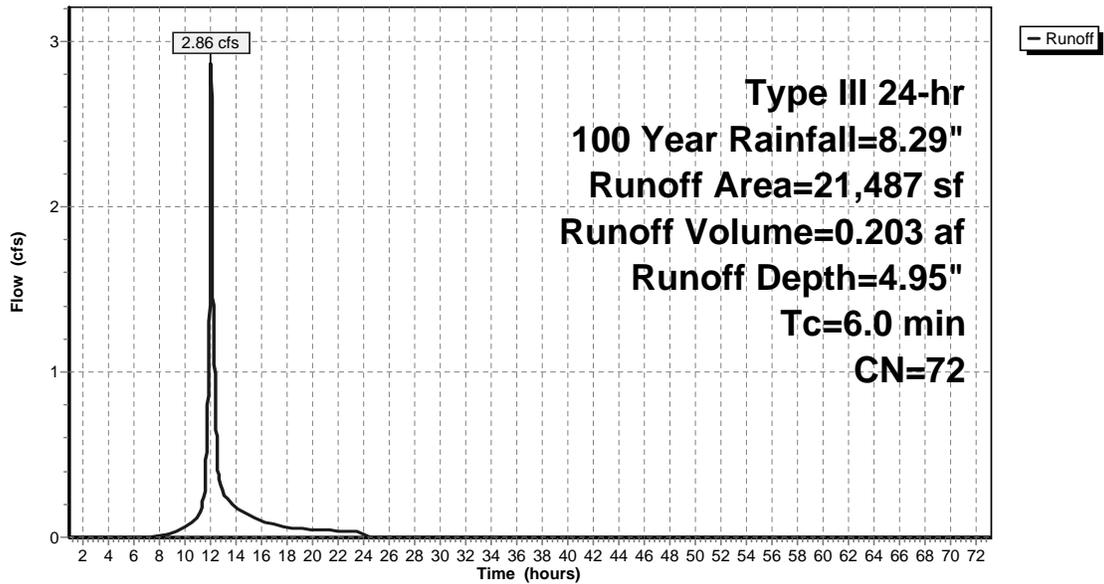
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Direct Entry

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**Subcatchment 3S: Off-Site East**

**Hydrograph**



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**Hydrograph for Subcatchment 3S: Off-Site East**

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.08	0.00	0.00	36.00	8.29	4.95	0.00	71.00	8.29	4.95	0.00
2.00	0.17	0.00	0.00	37.00	8.29	4.95	0.00	72.00	8.29	4.95	0.00
3.00	0.25	0.00	0.00	38.00	8.29	4.95	0.00	73.00	8.29	4.95	0.00
4.00	0.36	0.00	0.00	39.00	8.29	4.95	0.00				
5.00	0.47	0.00	0.00	40.00	8.29	4.95	0.00				
6.00	0.60	0.00	0.00	41.00	8.29	4.95	0.00				
7.00	0.75	0.00	0.00	42.00	8.29	4.95	0.00				
8.00	0.95	0.01	0.01	43.00	8.29	4.95	0.00				
9.00	1.21	0.04	0.03	44.00	8.29	4.95	0.00				
10.00	1.57	0.13	0.06	45.00	8.29	4.95	0.00				
11.00	2.07	0.32	0.12	46.00	8.29	4.95	0.00				
12.00	4.14	1.56	1.67	47.00	8.29	4.95	0.00				
13.00	6.22	3.17	0.28	48.00	8.29	4.95	0.00				
14.00	6.72	3.59	0.18	49.00	8.29	4.95	0.00				
15.00	7.08	3.90	0.14	50.00	8.29	4.95	0.00				
16.00	7.34	4.12	0.10	51.00	8.29	4.95	0.00				
17.00	7.54	4.29	0.08	52.00	8.29	4.95	0.00				
18.00	7.69	4.43	0.06	53.00	8.29	4.95	0.00				
19.00	7.82	4.54	0.05	54.00	8.29	4.95	0.00				
20.00	7.93	4.64	0.05	55.00	8.29	4.95	0.00				
21.00	8.04	4.73	0.04	56.00	8.29	4.95	0.00				
22.00	8.13	4.81	0.04	57.00	8.29	4.95	0.00				
23.00	8.21	4.88	0.04	58.00	8.29	4.95	0.00				
24.00	8.29	4.95	0.03	59.00	8.29	4.95	0.00				
25.00	8.29	4.95	0.00	60.00	8.29	4.95	0.00				
26.00	8.29	4.95	0.00	61.00	8.29	4.95	0.00				
27.00	8.29	4.95	0.00	62.00	8.29	4.95	0.00				
28.00	8.29	4.95	0.00	63.00	8.29	4.95	0.00				
29.00	8.29	4.95	0.00	64.00	8.29	4.95	0.00				
30.00	8.29	4.95	0.00	65.00	8.29	4.95	0.00				
31.00	8.29	4.95	0.00	66.00	8.29	4.95	0.00				
32.00	8.29	4.95	0.00	67.00	8.29	4.95	0.00				
33.00	8.29	4.95	0.00	68.00	8.29	4.95	0.00				
34.00	8.29	4.95	0.00	69.00	8.29	4.95	0.00				
35.00	8.29	4.95	0.00	70.00	8.29	4.95	0.00				

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**Summary for Subcatchment 3Sa: Off-Site East**

Runoff = 12.49 cfs @ 12.12 hrs, Volume= 0.998 af, Depth= 6.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100 Year Rainfall=8.29"

Area (sf)	CN	Description
53,364	74	>75% Grass cover, Good, HSG C
26,882	98	Water Surface, HSG C
* 3,160	96	Gravel Road
83,406	83	Weighted Average
56,524		67.77% Pervious Area
26,882		32.23% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	50	0.0280	0.16		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.00"
0.4	82	0.0316	3.61		<b>Shallow Concentrated Flow, Shallow Conc. Flow</b> Paved Kv= 20.3 fps
3.1	234	0.0317	1.25		<b>Shallow Concentrated Flow, Shallow Conc Flow</b> Short Grass Pasture Kv= 7.0 fps
8.6	366	Total			

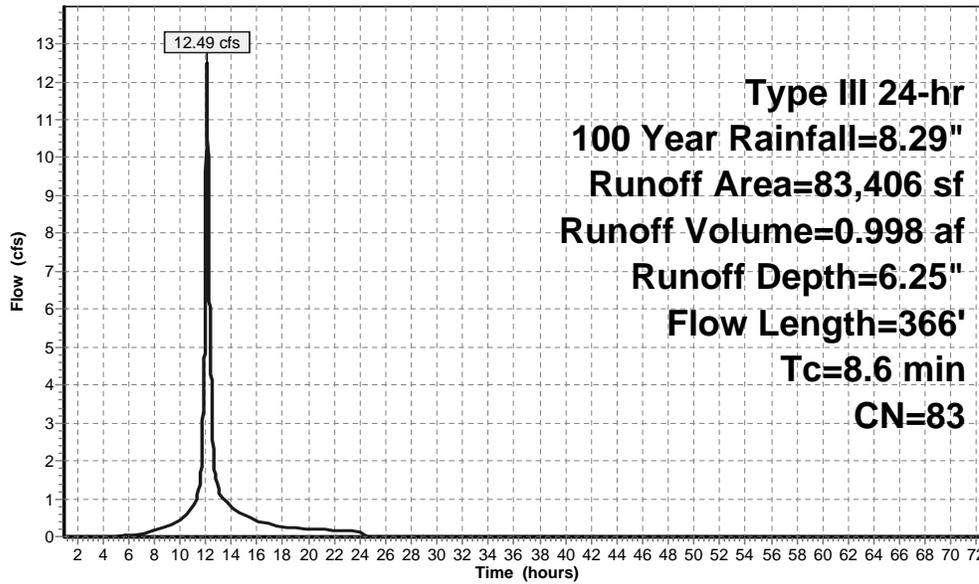
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Subcatchment 3Sa: Off-Site East

Hydrograph



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Hydrograph for Subcatchment 3Sa: Off-Site East

Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)	Time (hours)	Precip. (inches)	Excess (inches)	Runoff (cfs)
1.00	0.08	0.00	0.00	36.00	8.29	6.25	0.00	71.00	8.29	6.25	0.00
2.00	0.17	0.00	0.00	37.00	8.29	6.25	0.00	72.00	8.29	6.25	0.00
3.00	0.25	0.00	0.00	38.00	8.29	6.25	0.00	73.00	8.29	6.25	0.00
4.00	0.36	0.00	0.00	39.00	8.29	6.25	0.00				
5.00	0.47	0.00	0.01	40.00	8.29	6.25	0.00				
6.00	0.60	0.02	0.04	41.00	8.29	6.25	0.00				
7.00	0.75	0.05	0.08	42.00	8.29	6.25	0.00				
8.00	0.95	0.11	0.15	43.00	8.29	6.25	0.00				
9.00	1.21	0.22	0.27	44.00	8.29	6.25	0.00				
10.00	1.57	0.42	0.44	45.00	8.29	6.25	0.00				
11.00	2.07	0.75	0.76	46.00	8.29	6.25	0.00				
12.00	4.14	2.41	<b>6.67</b>	47.00	8.29	6.25	0.00				
13.00	6.22	4.29	<b>1.27</b>	48.00	8.29	6.25	0.00				
14.00	6.72	4.77	0.78	49.00	8.29	6.25	0.00				
15.00	7.08	5.10	0.59	50.00	8.29	6.25	0.00				
16.00	7.34	5.35	0.42	51.00	8.29	6.25	0.00				
17.00	7.54	5.54	0.33	52.00	8.29	6.25	0.00				
18.00	7.69	5.68	0.25	53.00	8.29	6.25	0.00				
19.00	7.82	5.81	0.22	54.00	8.29	6.25	0.00				
20.00	7.93	5.91	0.20	55.00	8.29	6.25	0.00				
21.00	8.04	6.01	0.18	56.00	8.29	6.25	0.00				
22.00	8.13	6.10	0.17	57.00	8.29	6.25	0.00				
23.00	8.21	6.18	0.15	58.00	8.29	6.25	0.00				
24.00	<b>8.29</b>	<b>6.25</b>	0.13	59.00	8.29	6.25	0.00				
25.00	8.29	6.25	0.00	60.00	8.29	6.25	0.00				
26.00	8.29	6.25	0.00	61.00	8.29	6.25	0.00				
27.00	8.29	6.25	0.00	62.00	8.29	6.25	0.00				
28.00	8.29	6.25	0.00	63.00	8.29	6.25	0.00				
29.00	8.29	6.25	0.00	64.00	8.29	6.25	0.00				
30.00	8.29	6.25	0.00	65.00	8.29	6.25	0.00				
31.00	8.29	6.25	0.00	66.00	8.29	6.25	0.00				
32.00	8.29	6.25	0.00	67.00	8.29	6.25	0.00				
33.00	8.29	6.25	0.00	68.00	8.29	6.25	0.00				
34.00	8.29	6.25	0.00	69.00	8.29	6.25	0.00				
35.00	8.29	6.25	0.00	70.00	8.29	6.25	0.00				

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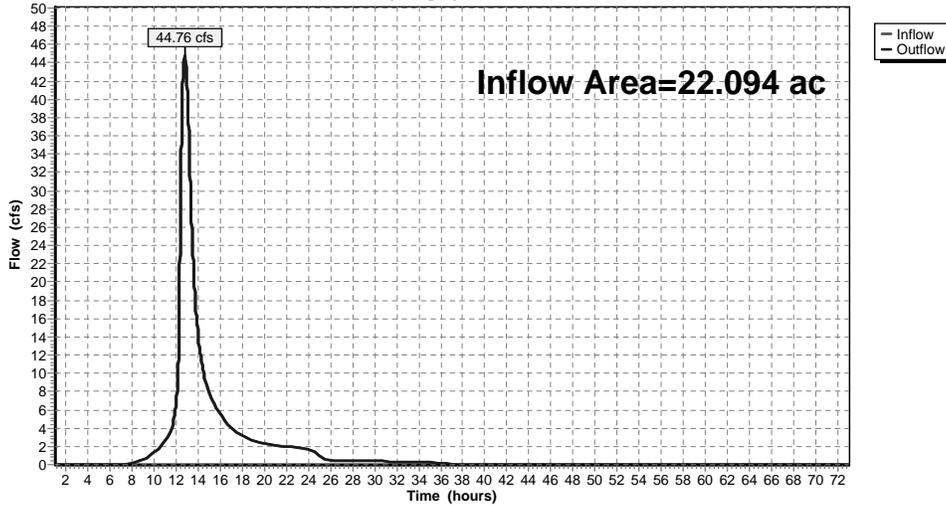
**Summary for Reach DP-1: (new Reach)**

Inflow Area = 22.094 ac, 3.96% Impervious, Inflow Depth = 4.78" for 100 Year event  
 Inflow = 44.76 cfs @ 12.75 hrs, Volume= 8.798 af  
 Outflow = 44.76 cfs @ 12.75 hrs, Volume= 8.798 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-1: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-1: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.16		0.16	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.02		0.02	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.02		0.02	42.00	0.00		0.00				
8.00	0.13		0.13	43.00	0.00		0.00				
9.00	0.52		0.52	44.00	0.00		0.00				
10.00	1.30		1.30	45.00	0.00		0.00				
11.00	2.65		2.65	46.00	0.00		0.00				
12.00	<b>7.15</b>		<b>7.15</b>	47.00	0.00		0.00				
13.00	<b>40.69</b>		<b>40.69</b>	48.00	0.00		0.00				
14.00	13.74		13.74	49.00	0.00		0.00				
15.00	7.74		7.74	50.00	0.00		0.00				
16.00	5.49		5.49	51.00	0.00		0.00				
17.00	3.96		3.96	52.00	0.00		0.00				
18.00	3.11		3.11	53.00	0.00		0.00				
19.00	2.57		2.57	54.00	0.00		0.00				
20.00	2.31		2.31	55.00	0.00		0.00				
21.00	2.13		2.13	56.00	0.00		0.00				
22.00	1.98		1.98	57.00	0.00		0.00				
23.00	1.83		1.83	58.00	0.00		0.00				
24.00	1.68		1.68	59.00	0.00		0.00				
25.00	0.87		0.87	60.00	0.00		0.00				
26.00	0.46		0.46	61.00	0.00		0.00				
27.00	0.42		0.42	62.00	0.00		0.00				
28.00	0.40		0.40	63.00	0.00		0.00				
29.00	0.39		0.39	64.00	0.00		0.00				
30.00	0.37		0.37	65.00	0.00		0.00				
31.00	0.36		0.36	66.00	0.00		0.00				
32.00	0.34		0.34	67.00	0.00		0.00				
33.00	0.33		0.33	68.00	0.00		0.00				
34.00	0.30		0.30	69.00	0.00		0.00				
35.00	0.27		0.27	70.00	0.00		0.00				

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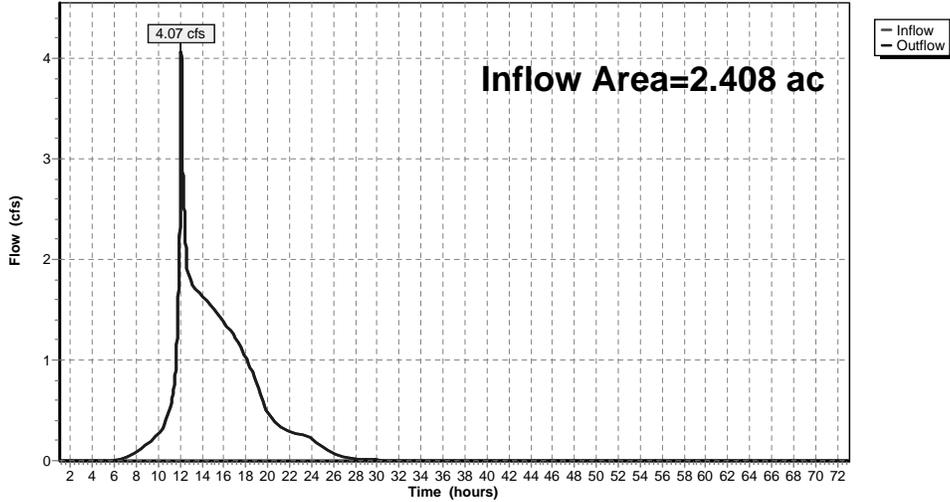
**Summary for Reach DP-3: (new Reach)**

Inflow Area = 2.408 ac, 25.63% Impervious, Inflow Depth = 5.99" for 100 Year event  
 Inflow = 4.07 cfs @ 12.09 hrs, Volume= 1.201 af  
 Outflow = 4.07 cfs @ 12.09 hrs, Volume= 1.201 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs

**Reach DP-3: (new Reach)**

Hydrograph



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**Hydrograph for Reach DP-3: (new Reach)**

Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)	Time (hours)	Inflow (cfs)	Elevation (feet)	Outflow (cfs)
1.00	0.00		0.00	36.00	0.00		0.00	71.00	0.00		0.00
2.00	0.00		0.00	37.00	0.00		0.00	72.00	0.00		0.00
3.00	0.00		0.00	38.00	0.00		0.00	73.00	0.00		0.00
4.00	0.00		0.00	39.00	0.00		0.00				
5.00	0.00		0.00	40.00	0.00		0.00				
6.00	0.00		0.00	41.00	0.00		0.00				
7.00	0.03		0.03	42.00	0.00		0.00				
8.00	0.08		0.08	43.00	0.00		0.00				
9.00	0.17		0.17	44.00	0.00		0.00				
10.00	0.27		0.27	45.00	0.00		0.00				
11.00	0.49		0.49	46.00	0.00		0.00				
12.00	<b>2.74</b>		<b>2.74</b>	47.00	0.00		0.00				
13.00	<b>1.78</b>		<b>1.78</b>	48.00	0.00		0.00				
14.00	1.63		1.63	49.00	0.00		0.00				
15.00	1.52		1.52	50.00	0.00		0.00				
16.00	1.38		1.38	51.00	0.00		0.00				
17.00	1.23		1.23	52.00	0.00		0.00				
18.00	1.02		1.02	53.00	0.00		0.00				
19.00	0.76		0.76	54.00	0.00		0.00				
20.00	0.48		0.48	55.00	0.00		0.00				
21.00	0.35		0.35	56.00	0.00		0.00				
22.00	0.29		0.29	57.00	0.00		0.00				
23.00	0.26		0.26	58.00	0.00		0.00				
24.00	0.24		0.24	59.00	0.00		0.00				
25.00	0.14		0.14	60.00	0.00		0.00				
26.00	0.07		0.07	61.00	0.00		0.00				
27.00	0.03		0.03	62.00	0.00		0.00				
28.00	0.02		0.02	63.00	0.00		0.00				
29.00	0.01		0.01	64.00	0.00		0.00				
30.00	0.01		0.01	65.00	0.00		0.00				
31.00	0.00		0.00	66.00	0.00		0.00				
32.00	0.00		0.00	67.00	0.00		0.00				
33.00	0.00		0.00	68.00	0.00		0.00				
34.00	0.00		0.00	69.00	0.00		0.00				
35.00	0.00		0.00	70.00	0.00		0.00				

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**Summary for Pond P1A: Pond 1a (Pond Repair)**

Inflow Area = 4.370 ac, 20.04% Impervious, Inflow Depth = 5.78" for 100 Year event  
 Inflow = 23.48 cfs @ 12.17 hrs, Volume= 2.104 af  
 Outflow = 10.34 cfs @ 12.48 hrs, Volume= 2.104 af, Atten= 56%, Lag= 18.3 min  
 Discarded = 0.31 cfs @ 12.48 hrs, Volume= 0.443 af  
 Primary = 0.50 cfs @ 12.48 hrs, Volume= 0.924 af  
 Secondary = 9.53 cfs @ 12.48 hrs, Volume= 0.737 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 79.12' @ 12.48 hrs Surf.Area= 28,674 sf Storage= 37,356 cf

Plug-Flow detention time= 306.3 min calculated for 2.104 af (100% of inflow)  
 Center-of-Mass det. time= 306.4 min ( 1,116.6 - 810.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	75.50'	1,242 cf	<b>Custom Stage Data (Irregular)</b> Listed below 3,106 cf Overall x 40.0% Voids
#2	76.50'	37,823 cf	<b>Custom Stage Data (Irregular)</b> Listed below 39,065 cf Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
75.50	3,106	220.0	0	0	3,106
76.00	3,106	220.0	1,553	1,553	3,216
76.50	3,106	220.0	1,553	3,106	3,326

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.50	3,106	220.0	0	0	3,106
77.00	6,731	331.0	2,402	2,402	7,975
78.00	15,313	639.8	10,732	13,134	31,836
79.20	26,330	782.0	24,689	37,823	47,947

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Device	Routing	Invert	Outlet Devices
#1	Secondary	78.70'	<b>14.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83
#2	Discarded	75.50'	<b>0.270 in/hr Exfiltration over Wetted area</b>
#3	Primary	75.50'	<b>4.0" Round Culvert</b> L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 75.50' / 75.10' S= 0.0100 ' S= 0.0100 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf

**Discarded OutFlow** Max=0.31 cfs @ 12.48 hrs HW=79.12' (Free Discharge)  
 ↳ **2=Exfiltration** (Exfiltration Controls 0.31 cfs)

**Primary OutFlow** Max=0.50 cfs @ 12.48 hrs HW=79.12' (Free Discharge)  
 ↳ **3=Culvert** (Barrel Controls 0.50 cfs @ 5.69 fps)

**Secondary OutFlow** Max=9.52 cfs @ 12.48 hrs HW=79.12' (Free Discharge)  
 ↳ **1=Broad-Crested Rectangular Weir** (Weir Controls 9.52 cfs @ 1.63 fps)

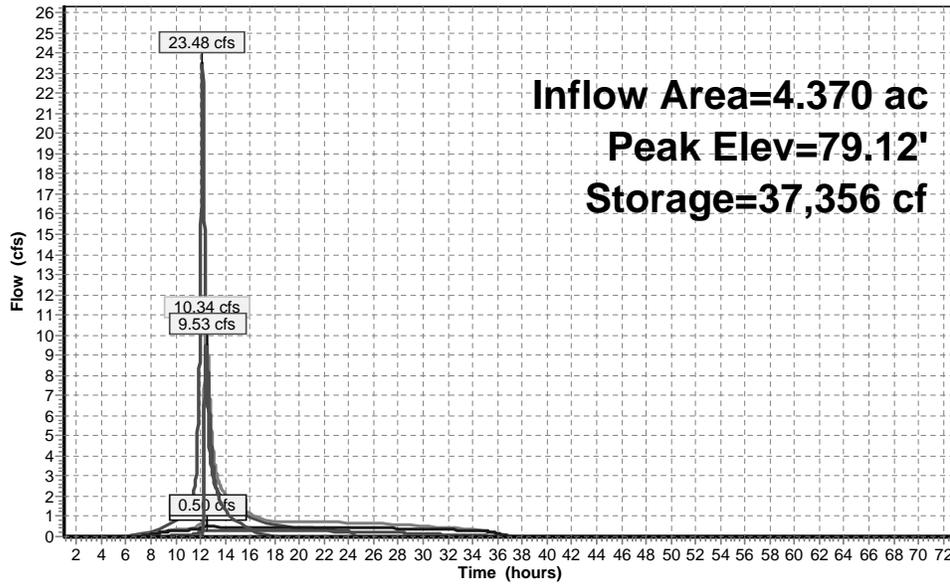
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Pond P1A: Pond 1a (Pond Repair)

Hydrograph



- Inflow
- Outflow
- Discarded
- Primary
- Secondary

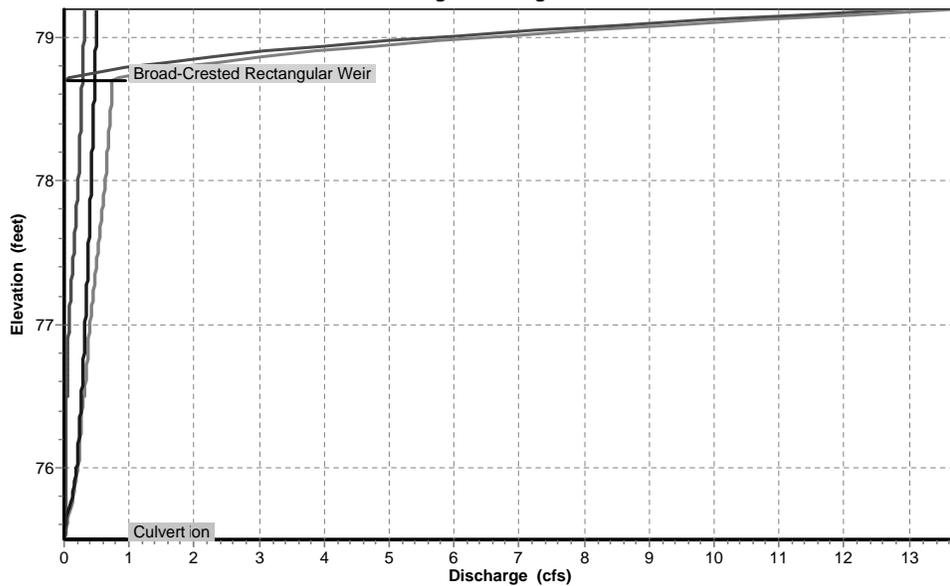
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Pond P1A: Pond 1a (Pond Repair)

Stage-Discharge

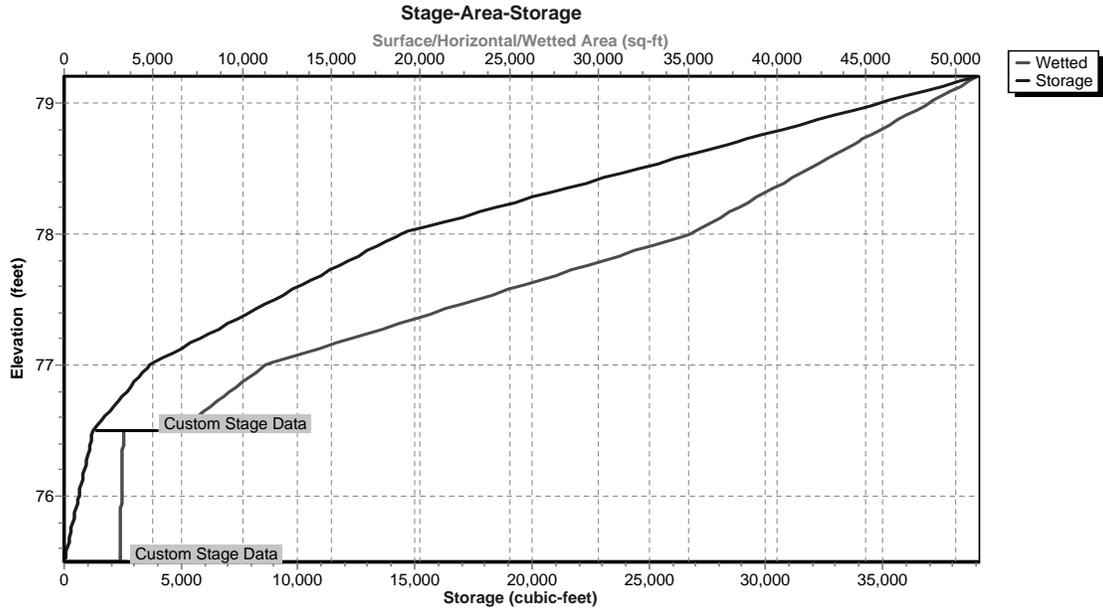


- Total
- Discarded
- Primary
- Secondary

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**Pond P1A: Pond 1a (Pond Repair)**



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**Hydrograph for Pond P1A: Pond 1a (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
1.00	0.00	0	75.50	0.00	0.00	0.00	0.00
6.00	0.02	8	75.51	0.00	0.00	0.00	0.00
11.00	<b>1.44</b>	<b>4,470</b>	<b>77.08</b>	<b>0.41</b>	<b>0.08</b>	<b>0.33</b>	<b>0.00</b>
16.00	<b>0.95</b>	<b>29,795</b>	<b>78.75</b>	<b>1.13</b>	<b>0.28</b>	<b>0.47</b>	<b>0.38</b>
21.00	0.41	25,955	78.56	0.72	0.27	0.46	0.00
26.00	0.00	17,448	78.15	0.66	0.23	0.43	0.00
31.00	0.00	7,081	77.32	0.47	0.12	0.36	0.00
36.00	0.00	480	75.89	0.18	0.02	0.16	0.00
41.00	0.00	0	75.50	0.00	0.00	0.00	0.00
46.00	0.00	0	75.50	0.00	0.00	0.00	0.00
51.00	0.00	0	75.50	0.00	0.00	0.00	0.00
56.00	0.00	0	75.50	0.00	0.00	0.00	0.00
61.00	0.00	0	75.50	0.00	0.00	0.00	0.00
66.00	0.00	0	75.50	0.00	0.00	0.00	0.00
71.00	0.00	0	75.50	0.00	0.00	0.00	0.00

**1817-Basin Repair 2024**

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**Stage-Discharge for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Secondary (cfs)
75.50	0.00	0.00	0.00	0.00	79.00	6.41	0.30	0.49	5.61
75.60	0.04	0.02	0.02	0.00	79.10	9.70	0.31	0.50	8.89
75.70	0.09	0.02	0.07	0.00	79.20	<b>13.72</b>	<b>0.32</b>	<b>0.50</b>	<b>12.89</b>
75.80	0.14	0.02	0.12	0.00					
75.90	0.18	0.02	0.16	0.00					
76.00	0.21	0.02	0.19	0.00					
76.10	0.23	0.02	0.21	0.00					
76.20	0.25	0.02	0.23	0.00					
76.30	0.26	0.02	0.24	0.00					
76.40	0.27	0.02	0.25	0.00					
76.50	0.31	0.04	0.27	0.00					
76.60	0.33	0.05	0.28	0.00					
76.70	0.34	0.05	0.29	0.00					
76.80	0.36	0.06	0.30	0.00					
76.90	0.38	0.06	0.31	0.00					
77.00	0.39	0.07	0.32	0.00					
77.10	0.42	0.09	0.33	0.00					
77.20	0.44	0.10	0.34	0.00					
77.30	0.47	0.12	0.35	0.00					
77.40	0.49	0.13	0.36	0.00					
77.50	0.52	0.15	0.37	0.00					
77.60	0.54	0.16	0.38	0.00					
77.70	0.56	0.18	0.39	0.00					
77.80	0.59	0.19	0.40	0.00					
77.90	0.61	0.20	0.41	0.00					
78.00	0.63	0.22	0.41	0.00					
78.10	0.65	0.23	0.42	0.00					
78.20	0.67	0.24	0.43	0.00					
78.30	0.68	0.24	0.44	0.00					
78.40	0.70	0.25	0.45	0.00					
78.50	0.71	0.26	0.45	0.00					
78.60	0.73	0.27	0.46	0.00					
78.70	0.75	0.28	0.47	0.00					
78.80	1.81	0.29	0.47	1.05					
78.90	3.74	0.30	0.48	2.97					

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**Stage-Area-Storage for Pond P1A: Pond 1a (Pond Repair)**

Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Wetted (sq-ft)	Storage (cubic-feet)
75.50	3,106	0	77.25	17,266	6,327	79.00	48,588	34,950
75.55	3,117	62	77.30	18,459	6,864	79.05	49,260	35,979
75.60	3,128	124	77.35	19,652	7,400	79.10	49,931	37,008
75.65	3,139	186	77.40	20,845	7,937	79.15	50,602	38,036
75.70	3,150	248	77.45	22,038	8,473	79.20	<b>51,273</b>	<b>39,065</b>
75.75	3,161	311	77.50	23,231	9,010			
75.80	3,172	373	77.55	24,424	9,547			
75.85	3,183	435	77.60	25,618	10,083			
75.90	3,194	497	77.65	26,811	10,620			
75.95	3,205	559	77.70	28,004	11,156			
76.00	3,216	621	77.75	29,197	11,693			
76.05	3,227	683	77.80	30,390	12,230			
76.10	3,238	745	77.85	31,583	12,766			
76.15	3,249	808	77.90	32,776	13,303			
76.20	3,260	870	77.95	33,969	13,839			
76.25	3,271	932	78.00	35,162	14,376			
76.30	3,282	994	78.05	35,833	15,405			
76.35	3,293	1,056	78.10	36,505	16,434			
76.40	3,304	1,118	78.15	37,176	17,462			
76.45	3,315	1,180	78.20	37,847	18,491			
76.50	6,432	1,242	78.25	38,518	19,520			
76.55	6,919	1,483	78.30	39,190	20,548			
76.60	7,406	1,723	78.35	39,861	21,577			
76.65	7,893	1,963	78.40	40,532	22,606			
76.70	8,380	2,203	78.45	41,204	23,634			
76.75	8,866	2,443	78.50	41,875	24,663			
76.80	9,353	2,683	78.55	42,546	25,692			
76.85	9,840	2,923	78.60	43,218	26,721			
76.90	10,327	3,164	78.65	43,889	27,749			
76.95	10,814	3,404	78.70	44,560	28,778			
77.00	11,301	3,644	78.75	45,232	29,807			
77.05	12,494	4,181	78.80	45,903	30,835			
77.10	13,687	4,717	78.85	46,574	31,864			
77.15	14,880	5,254	78.90	47,246	32,893			
77.20	16,073	5,790	78.95	47,917	33,922			

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**Summary for Pond P3A: Pond 3A (Pond Repair)**

Inflow Area = 1.915 ac, 32.23% Impervious, Inflow Depth = 6.25" for 100 Year event  
 Inflow = 12.49 cfs @ 12.12 hrs, Volume= 0.998 af  
 Outflow = 1.50 cfs @ 12.83 hrs, Volume= 0.998 af, Atten= 88%, Lag= 42.7 min  
 Primary = 0.51 cfs @ 12.83 hrs, Volume= 0.480 af  
 Secondary = 0.99 cfs @ 12.83 hrs, Volume= 0.518 af  
 Tertiary = 0.00 cfs @ 1.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 1.00-73.00 hrs, dt= 0.01 hrs  
 Peak Elev= 78.22' @ 12.83 hrs Surf.Area= 19,062 sf Storage= 19,761 cf  
 Flood Elev= 79.50' Surf.Area= 25,484 sf Storage= 37,166 cf

Plug-Flow detention time= 155.6 min calculated for 0.998 af (100% of inflow)  
 Center-of-Mass det. time= 155.5 min ( 952.3 - 796.8 )

Volume	Invert	Avail.Storage	Storage Description		
#1	76.00'	37,166 cf	<b>Custom Stage Data (Irregular)</b> Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
76.00	2,053	339.0	0	0	2,053
77.00	6,709	559.0	4,158	4,158	17,781
78.00	17,458	791.4	11,663	15,821	42,764
79.00	25,484	883.5	21,345	37,166	55,068

Device	Routing	Invert	Outlet Devices
#1	Primary	76.00'	<b>4.0" Round 6" Culvert 1</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.00' / 75.52' S= 0.0240 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Secondary	76.55'	<b>6.0" Round 6" Culvert 2</b> L= 20.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 76.55' / 75.60' S= 0.0475 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#3	Tertiary	78.50'	<b>20.0' long x 6.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50

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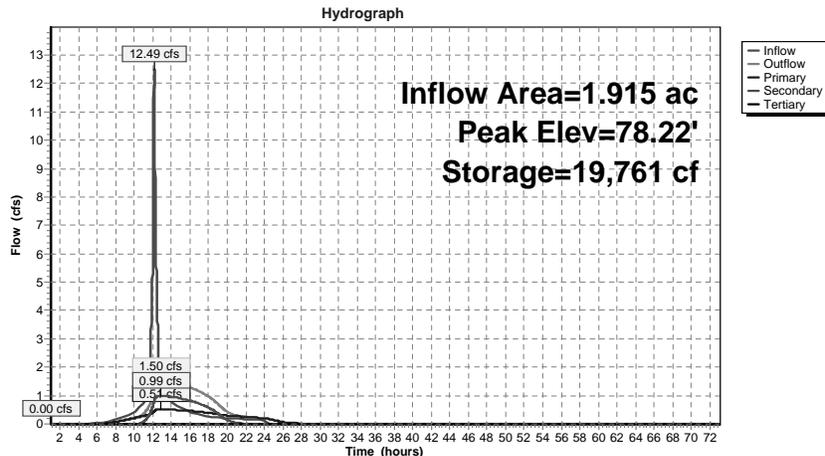
Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76  
 2.83

**Primary OutFlow** Max=0.51 cfs @ 12.83 hrs HW=78.22' (Free Discharge)  
 1=6" Culvert 1 (Barrel Controls 0.51 cfs @ 5.87 fps)

**Secondary OutFlow** Max=0.99 cfs @ 12.83 hrs HW=78.22' (Free Discharge)  
 2=6" Culvert 2 (Inlet Controls 0.99 cfs @ 5.06 fps)

**Tertiary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=76.00' (Free Discharge)  
 3=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Pond P3A: Pond 3A (Pond Repair)**



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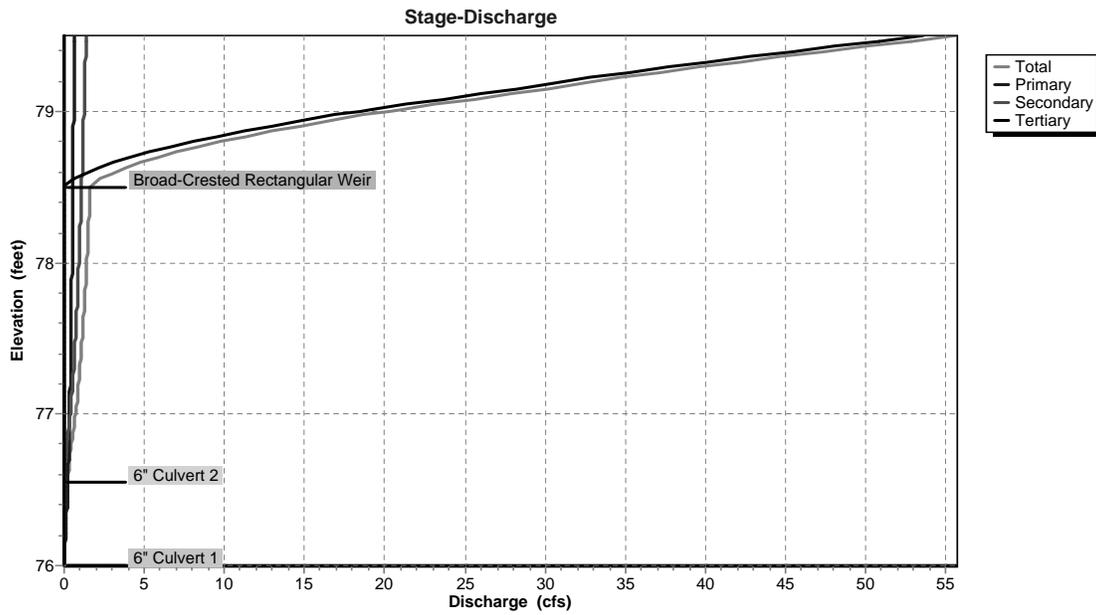
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 100 Year Rainfall=8.29"

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Pond P3A: Pond 3A (Pond Repair)



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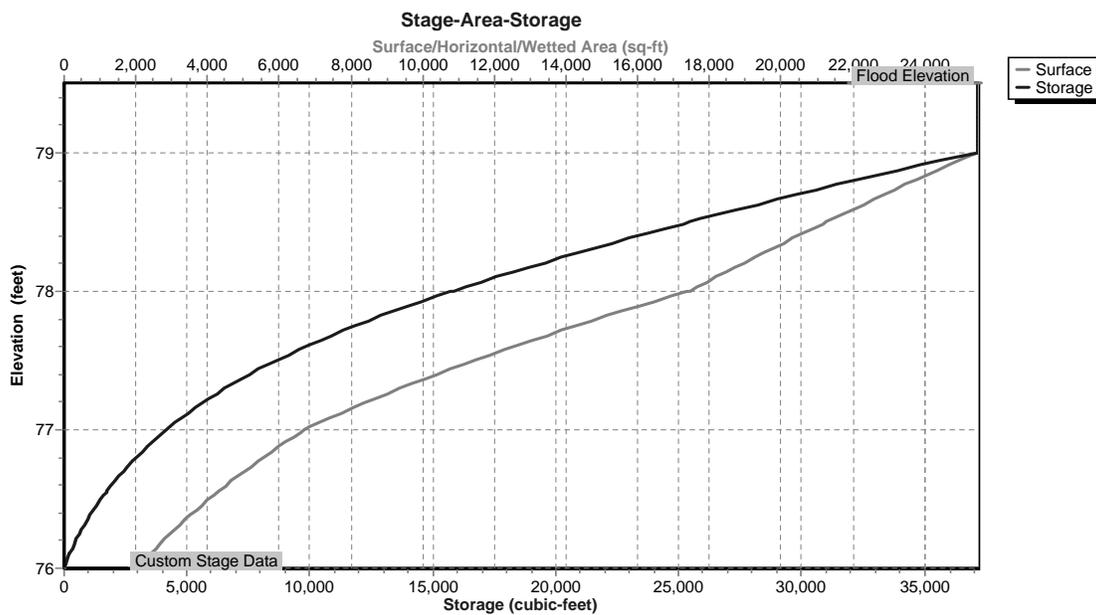
Proposed Basin Repair Analysis for 2-, 10-, 25-, 100-Year Storms

Type III 24-hr 100 Year Rainfall=8.29"

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Pond P3A: Pond 3A (Pond Repair)



**1817-Basin Repair 2024**

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**Hydrograph for Pond P3A: Pond 3A (Pond Repair)**

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Outflow (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
1.00	0.00	0	76.00	0.00	0.00	0.00	0.00
6.00	0.04	85	76.04	0.00	0.00	0.00	0.00
11.00	0.76	2,604	76.74	0.37	0.28	0.09	0.00
16.00	0.42	12,171	77.77	1.28	0.46	0.82	0.00
21.00	0.18	2,287	76.68	0.31	0.26	0.04	0.00
26.00	0.00	447	76.19	0.07	0.07	0.00	0.00
31.00	0.00	96	76.04	0.00	0.00	0.00	0.00
36.00	0.00	47	76.02	0.00	0.00	0.00	0.00
41.00	0.00	24	76.01	0.00	0.00	0.00	0.00
46.00	0.00	12	76.01	0.00	0.00	0.00	0.00
51.00	0.00	6	76.00	0.00	0.00	0.00	0.00
56.00	0.00	3	76.00	0.00	0.00	0.00	0.00
61.00	0.00	2	76.00	0.00	0.00	0.00	0.00
66.00	0.00	1	76.00	0.00	0.00	0.00	0.00
71.00	0.00	0	76.00	0.00	0.00	0.00	0.00

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**Stage-Discharge for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Tertiary (cfs)
76.00	0.00	0.00	0.00	0.00
76.10	0.02	0.02	0.00	0.00
76.20	0.07	0.07	0.00	0.00
76.30	0.14	0.14	0.00	0.00
76.40	0.18	0.18	0.00	0.00
76.50	0.21	0.21	0.00	0.00
76.60	0.25	0.24	0.01	0.00
76.70	0.33	0.27	0.06	0.00
76.80	0.44	0.30	0.15	0.00
76.90	0.58	0.32	0.26	0.00
77.00	0.71	0.34	0.38	0.00
77.10	0.82	0.36	0.46	0.00
77.20	0.90	0.38	0.53	0.00
77.30	0.98	0.39	0.59	0.00
77.40	1.06	0.41	0.65	0.00
77.50	1.13	0.43	0.70	0.00
77.60	1.19	0.44	0.75	0.00
77.70	1.24	0.45	0.79	0.00
77.80	1.30	0.46	0.83	0.00
77.90	1.35	0.48	0.87	0.00
78.00	1.40	0.49	0.91	0.00
78.10	1.45	0.50	0.95	0.00
78.20	1.50	0.51	0.99	0.00
78.30	1.54	0.52	1.02	0.00
78.40	1.59	0.53	1.06	0.00
78.50	1.63	0.54	1.09	0.00
78.60	3.17	0.55	1.12	1.50
78.70	5.95	0.56	1.15	4.24
78.80	9.77	0.57	1.18	8.02
78.90	14.49	0.58	1.21	12.70
79.00	20.25	0.59	1.24	18.42
79.10	26.96	0.60	1.27	25.10
79.20	33.41	0.61	1.29	31.51
79.30	40.29	0.62	1.32	38.35
79.40	47.74	0.63	1.35	45.76

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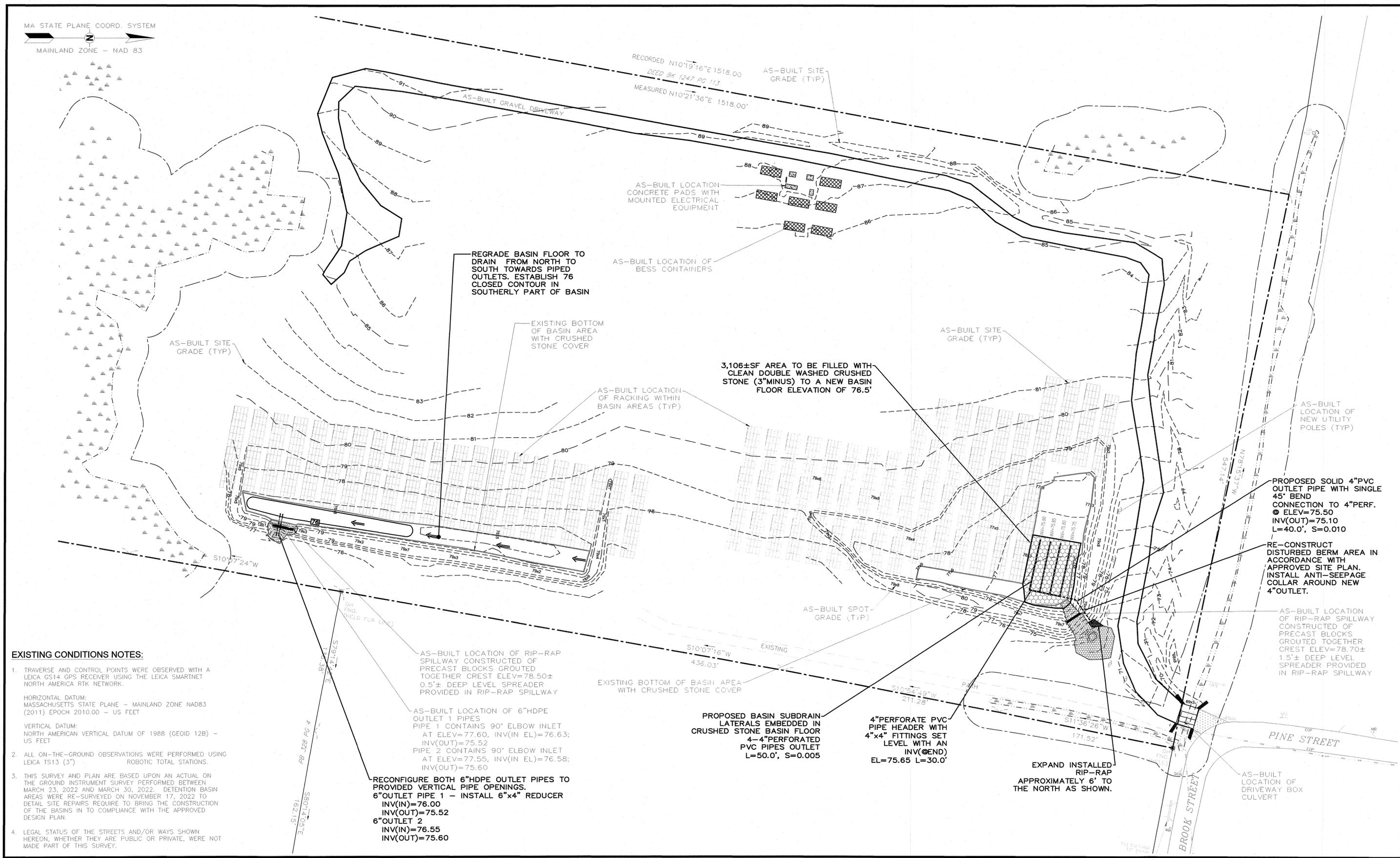
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**Stage-Area-Storage for Pond P3A: Pond 3A (Pond Repair)**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
76.00	2,053	0	77.75	14,298	11,858	79.50	25,484	37,166
76.05	2,222	107	77.80	14,905	12,588			
76.10	2,398	222	77.85	15,524	13,349			
76.15	2,581	347	77.90	16,156	14,141			
76.20	2,770	481	77.95	16,801	14,964			
76.25	2,966	624	78.00	17,458	15,821			
76.30	3,169	777	78.05	17,823	16,703			
76.35	3,378	941	78.10	18,192	17,603			
76.40	3,594	1,115	78.15	18,565	18,522			
76.45	3,817	1,300	78.20	18,942	19,460			
76.50	4,046	1,497	78.25	19,323	20,417			
76.55	4,282	1,705	78.30	19,707	21,392			
76.60	4,525	1,925	78.35	20,095	22,387			
76.65	4,775	2,158	78.40	20,487	23,402			
76.70	5,031	2,403	78.45	20,882	24,436			
76.75	5,294	2,661	78.50	21,282	25,490			
76.80	5,563	2,932	78.55	21,685	26,564			
76.85	5,840	3,217	78.60	22,092	27,659			
76.90	6,123	3,516	78.65	22,503	28,774			
76.95	6,413	3,830	78.70	22,917	29,909			
77.00	6,709	4,158	78.75	23,336	31,065			
77.05	7,127	4,504	78.80	23,758	32,243			
77.10	7,557	4,871	78.85	24,184	33,441			
77.15	8,000	5,259	78.90	24,613	34,661			
77.20	8,455	5,671	78.95	25,047	35,903			
77.25	8,923	6,105	79.00	<b>25,484</b>	<b>37,166</b>			
77.30	9,404	6,563	79.05	25,484	37,166			
77.35	9,897	7,046	79.10	25,484	37,166			
77.40	10,403	7,553	79.15	25,484	37,166			
77.45	10,922	8,086	79.20	25,484	37,166			
77.50	11,453	8,646	79.25	25,484	37,166			
77.55	11,997	9,232	79.30	25,484	37,166			
77.60	12,553	9,846	79.35	25,484	37,166			
77.65	13,122	10,487	79.40	25,484	37,166			
77.70	13,704	11,158	79.45	25,484	37,166			



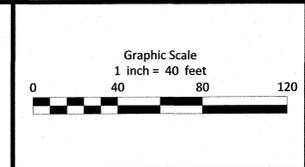


**EXISTING CONDITIONS NOTES:**

1. TRAVERSE AND CONTROL POINTS WERE OBSERVED WITH A LEICA GS14 GPS RECEIVER USING THE LEICA SMARTNET NORTH AMERICA RTK NETWORK.  
HORIZONTAL DATUM:  
MASSACHUSETTS STATE PLANE - MAINLAND ZONE NAD83 (2011) EPOCH 2010.00 - US FEET  
VERTICAL DATUM:  
NORTH AMERICAN VERTICAL DATUM OF 1988 (GEOID 12B) - US FEET
2. ALL ON-THE-GROUND OBSERVATIONS WERE PERFORMED USING LEICA TS13 (3") ROBOTIC TOTAL STATIONS.
3. THIS SURVEY AND PLAN ARE BASED UPON AN ACTUAL ON THE GROUND INSTRUMENT SURVEY PERFORMED BETWEEN MARCH 23, 2022 AND MARCH 30, 2022. DETENTION BASIN AREAS WERE RE-SURVEYED ON NOVEMBER 17, 2022 TO DETAIL SITE REPAIRS REQUIRE TO BRING THE CONSTRUCTION OF THE BASINS IN TO COMPLIANCE WITH THE APPROVED DESIGN PLAN.
4. LEGAL STATUS OF THE STREETS AND/OR WAYS SHOWN HEREON, WHETHER THEY ARE PUBLIC OR PRIVATE, WERE NOT MADE PART OF THIS SURVEY.

REV #	DATE	DESCRIPTION
0	4/15/24	ISSUED FOR REVIEW

REVISIONS:



PREPARED BY:

CIVIL ENGINEERING / LAND SURVEYING  
249 SOUTH STREET, UNIT 1, PLAINVILLE, MA 02762  
Tel. 508 - 995-2221  
website: www.levelsg.com

PROJECT:

893 BROOK STREET  
PARCEL ID: 016.0-0028-0000.0  
DIGHTON, MASSACHUSETTS

TITLE:

**BASINS 1 & 3 REPAIR  
BROOK STREET SOLAR**

PREPARED FOR:

GHTJA03, LLC  
1209 ORANGE STREET  
WILMINGTON, DE 19801

DATE:

APRIL 15, 2024

1 OF 1  
SHEET NO. 1